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Aerotherm TR-76-13

AEROTHERM GRAPHITE SURFACE KINETICS COMPUTER PROGRAM (GASKET2)
USER'S MANUAL

Acurex Corporation/Aerotherm Division
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December 1976



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Air Force Rocket Propulsion Laboratory
Director of Science and Technology
Air Force Systems Command
Edwards AFB, California 93523

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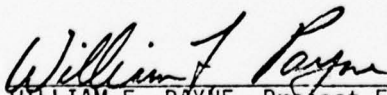
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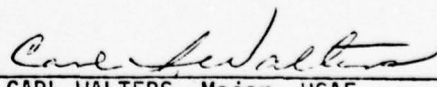
FOREWORD

This report was submitted by Acurex Corporation/ Aerotherm Division, 485 Clyde Avenue, Mountain View, CA 94042 under contract F04611-74-C-0023, Job Order No. 305909HUJ with the Air Force Rocket Propulsion Laboratory, Edwards AFB, California 93523.

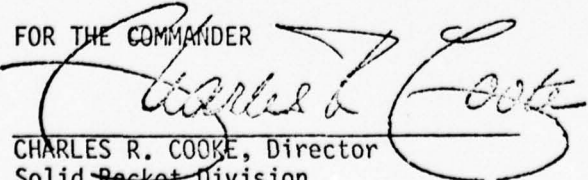
Contract work was performed in the period 1 May 1974 to 31 July 1976 and was documented in this final report and in a second final report (AFRPL-TR-76-71) which is classified CONFIDENTIAL. In addition to the final reports and other written documentation, a 2-day seminar was conducted by Aerotherm at its Mountain View facility to present contract results to the rocket motor community in a timely fashion. The Aerotherm work was managed by Mr. Roger J. Bedard, Manager, Propulsion Systems, and the Air Force Technical Monitor was Mr. William F. Payne.

This report has been reviewed by the Information Office/DOZ and is releasable to the National Technical Information Service (NTIS). At NTIS it will be available to the general public, including foreign nations. This report is unclassified and suitable for general public release.


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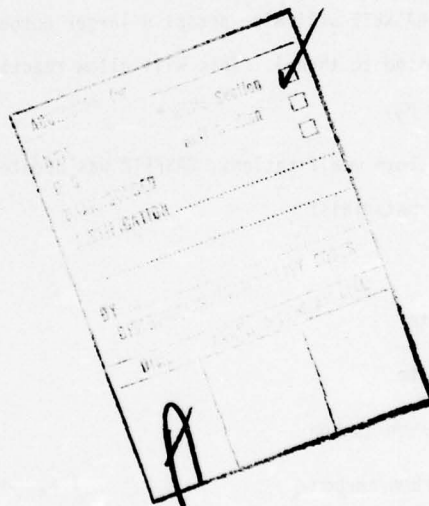
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temperatures below 5500°R. GASKET2 also accepts an increased number of surface kinetics - controlled reactions.

In addition to the modifications, surface kinetics for ATJ and G-90 bulk graphites, 15% silicon carbide modified pyrolytic graphite and Pyrocarb 901 and Carbitex 700 carbon/carbon materials were added to GASKET2. Also, improved surface kinetics for C plane pyrolytic graphite were included. ↑

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SUMMARY

Recent studies at Aerotherm have shown that the accuracy and versatility of the GASKET code can be improved by some minor code modifications. These modifications were identified and incorporated into the GASKET code. The modified code, entitled GASKET2, includes a generalized computational scheme for combined equilibrium-nonequilibrium systems, sublimation kinetics, and an expanded thermochemistry data bank including the Duff-Bauer hydrocarbon species. With these modifications, GASKET2 predicts higher ablation rates than GASKET at surface temperatures above 5500°R. These rates reach the asymptotic diffusion controlled value at the high temperature limit. At surface temperatures below 5500°R, however, both codes predict results with insignificant discrepancies. In addition to the improved predictions, GASKET2 will also accept a larger number of surface kinetically controlled reactions than GASKET (limited to three). This will allow reactants other than the three currently used; namely, H_2O , CO_2 and H_2 .

In addition to the above modifications, GASKET2 was updated to include the surface kinetics of the following graphitic materials:

- 15% SiC/PG
- ATJ bulk graphite
- G-90 bulk graphite
- Pyrocarb 901 carbon/carbon
- Carbitex 700 carbon/carbon
- C plane pyrolytic graphite (improved kinetics)

Kinetic reaction rates for these materials were obtained from arc plasma generator and rocket motor data.

This report was prepared in two parts. The first part describes the code modifications and updates to GASKET. The differences between GASKET and GASKET2 are illustrated in terms of computational scheme and surface ablation rate predictions. Also, a brief description of the GASKET2 output

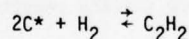
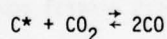
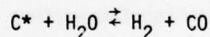
is included, so that users can use this code more effectively. The second part of the report contains an updated user's manual, a partial listing of GASKET2 which shows the locations where FORTRAN changes were made to GASKET, and three sample problems. Finally, it should be noted that this report serves only as an addendum to the earlier published GASKET reports.

SECTION 1
CODE MODIFICATIONS AND UPDATES

The Graphite Surface Kinetics (GASKET) computer code, developed under USAF Contract F04611-69-C-0081, was designed to calculate graphite surface thermochemical ablation rates as a result of exposure to propellant gases. The mathematical model, employed by GASKET, accounts for such thermophysical phenomena as:

- Diffusion of the reactive species from the boundary layer edge to the gaseous region adjacent to the carbon surface
- Adsorption of the reactive species to an active site on the carbon surface
- Formation of reaction products at the carbon surface
- Desorption of reaction products from the carbon surface
- Diffusion of reaction products into the boundary layer

Among all possible heterogeneous reactions occurring at the surface, only the following three were considered to be important at the temperature range and environments of interest:



Also under the same contract, the surface kinetics of the following materials were correlated:

- A-b plane pyrolytic graphite
- C plane pyrolytic graphite
- Bulk graphite

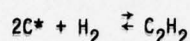
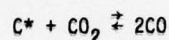
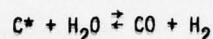
These correlations were then implemented into GASKET.

GASKET has been used extensively in rocket motor applications. The surface temperature range for this type of application is normally between 3000°R and 6000°R. For these applications, GASKET predicts satisfactory results.

Recently, the trend of rocket nozzle design has been altered somewhat. Instead of burning the conventional propellant and fabricating rocket nozzles with pyrolytic graphite, higher enthalpy propellants and graphitic materials such as carbon/carbon composite and bulk graphite are used. The introduction of these new elements into the rocket technology necessitated the assessment of the prediction ability of GASKET in a temperature range exceeding 6000°R and the correlation of the ablation kinetics of these graphitic materials. Under USAF Contract F04611-74-C-0023, GASKET was modified to handle the high temperature calculations, and was updated to contain the surface kinetics of the graphitic materials that were correlated under the same contract.

1.1 GENERAL EQUILIBRIUM-NONEQUILIBRIUM COMPUTATIONAL SCHEME

As mentioned previously, the thermochemical ablation of graphite materials as a result of exposure to propellant gases is assumed to be controlled by the following heterogeneous reactions:



This kinetic model appears to be a viable assumption in the temperature range between 3000°R and 6000°R as satisfactory predictions have been obtained. However, as surface temperature exceeds 6000°R, other surface activities may become significant, e.g., sublimation. Due to the intrinsic weakness of the computational scheme used in GASKET, the inclusion of more than three surface reactions may encounter difficulties (see Reference 1 for detailed discussion). Since more surface reactions are required to be considered in high temperature predictions, it is necessary that such an intrinsic weakness be removed by using a more general computational scheme.

GASKET was modified to accommodate more surface reactions. This capability was made possible by allowing reactants and products to be base as well as nonbase species (see Reference 2). Through internal bookkeeping, the net generation rate for each base species is calculated without the complication of introducing a fictitious base species (as was done in the previous version of GASKET).

A comparison of the computational procedures for the two versions of GASKET is demonstrated schematically in Figure 1. A (H, O) composition edge-gas reaction with a carbon surface was taken as an illustrative example. As can be seen, a fictitious base species (in this case, CO₂) was created in order to accommodate the three kinetically controlled reactions in the previous version of GASKET.

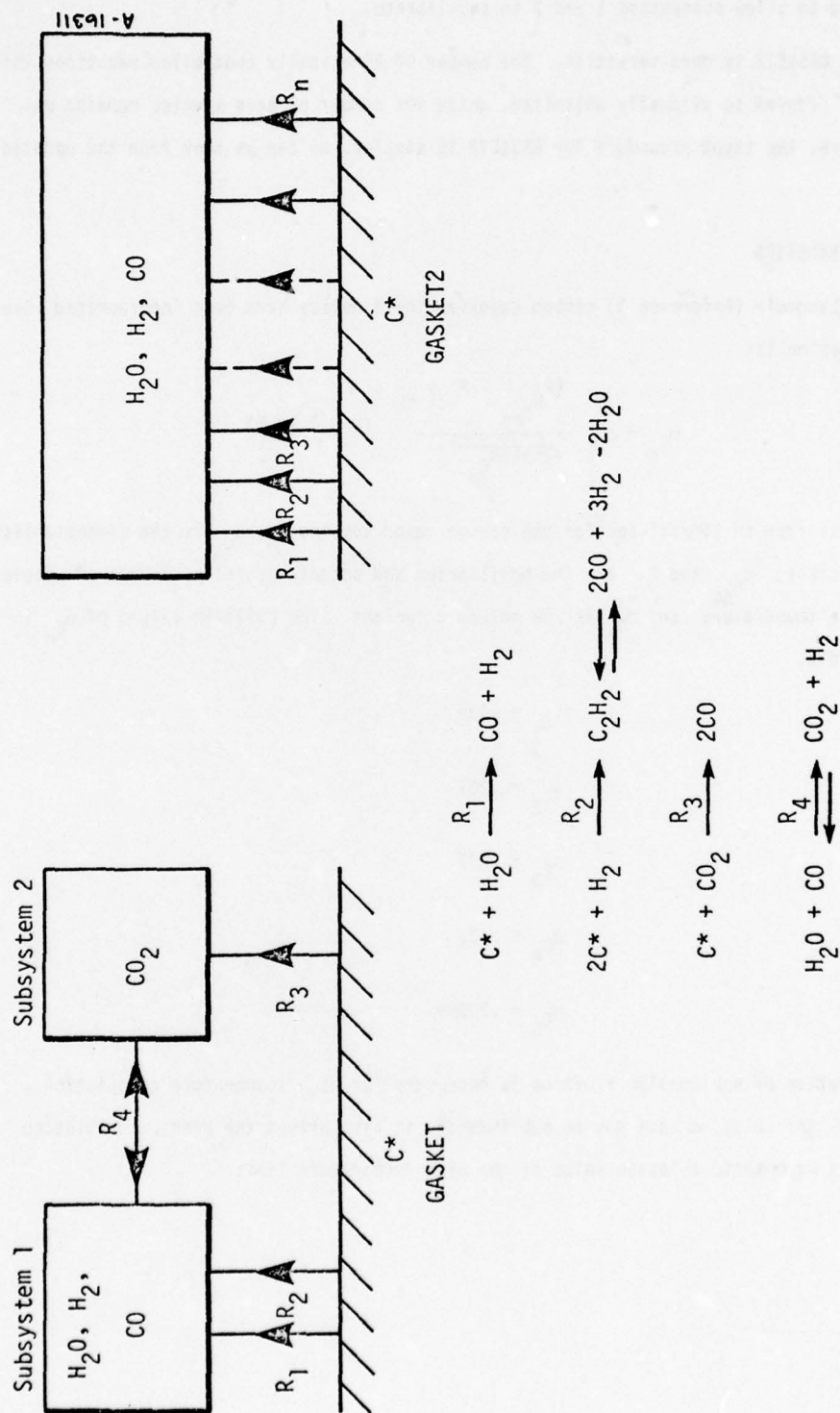


Figure 1. Comparison of computational schemes between the previous and modified versions of GASKET.

If more kinetically controlled reactions are required more fictitious base species should be created accordingly. In addition, since gas phase species are in equilibrium, an artificial infinite rate reaction is required to allow subsystems 1 and 2 to equilibrate.

In contrast, GASKET2 is more versatile. The number of kinetically controlled reactions that can be input to the program is virtually unlimited, while the number of base species remains unchanged. Furthermore, the input procedure for GASKET2 is simpler, as can be seen from the updated input instructions.

1.2 SUBLIMATION KINETICS

The Knudsen-Langmuir (Reference 3) carbon vaporization kinetics have been incorporated into GASKET2. The expression is:

$$m_{C_n} = \alpha_{C_n} \frac{(P_{C_{n,eq}} - P_{C_n})}{\sqrt{2\pi RT/M_{C_n}}} \quad (n = 1 \text{ to } 5)$$

where m_{C_n} is the mass flux in lbm/ft²-sec for the carbon vapor species C_n , α_{C_n} is the dimensionless vaporization coefficient, $P_{C_{n,eq}}$ and P_{C_n} are the equilibrium and actual partial pressures of species C_n , T is the surface temperature, and M_{C_n} is the molecular weight. The built-in values of α_{C_n} in GASKET2 are as follows:

$$\alpha_{C_1} = .125$$

$$\alpha_{C_2} = .261$$

$$\alpha_{C_3} = .012$$

$$\alpha_{C_4} = .130$$

$$\alpha_{C_5} = .00096$$

The incorporation of sublimation kinetics is necessary for high temperature calculations. It not only predicts the ablation rate due to sublimation, it also drives the predicted ablation rates to the correct asymptotic ablation value at the high temperature limit.

1.3 THERMOCHEMICAL EQUILIBRIUM DATA

The determination of a thermodynamic state of a chemical reacting system requires the input of thermochemical equilibrium data describing the formation of each species. In a particular temperature and pressure range of interest, some species can be neglected without affecting the accuracy of the calculation significantly. However, it does not guarantee the same accuracy can be maintained when the range has been surpassed. Therefore, a screening study was initiated to evaluate the built-in thermochemical equilibrium data in GASKET for high temperature calculations.

The results of the evaluation show that the Duff-Bauer hydrocarbon species, formed favorably at temperatures above 6000°R but not below, should be included in the built-in data bank. With the inclusion of the Duff-Bauer hydrocarbon species, GASKET2 predicts higher ablation rates at or above 5500°R. The reason for the increase in the predicted ablation rate is due to a significant increase in the formation of C_3H at temperatures above 5500°R. Carbon molecules which ablate to the gas phase through surface reactions are quickly reacted to form C_3H . Therefore, a larger carbon sink exists in the gas phase with C_3H species than the one without. Furthermore, the existence of C_3H species can alter the reactive species concentration at the carbon surface, and hence the ablation rates.

1.4 COMPARISONS OF GASKET AND GASKET2 PREDICTIONS

A sample problem was run to compare the predictions from GASKET and GASKET2. The selected problem considers the thermochemical ablation at the exit cone location of the rocket nozzle when exposed to PEG/FEFO propellant. The surface material was assumed to be bulk graphite. The comparison of the two solutions in terms of B' versus T_w is shown in Figure 2. Also shown in this figure is the surface equilibrium solution which serves as the baseline solution. As can be seen, both GASKET and GASKET2 solutions predicted B' values below the surface equilibrium value at surface temperatures below 5500°R. This indicates that the surface reactions are kinetically controlled. Also, note that both solutions agree with each other with less than 10 percent discrepancy. As the surface temperature exceeds 5500°R, the B' predicted by GASKET2 gradually approaches the surface equilibrium value, whereas the GASKET B' is still markedly below and has no trend of approaching the surface equilibrium B' .

From the results of this comparison, the following conclusions can be drawn:

- Both GASKET and GASKET2 predict similar results at or below 5500°R
- At the upper temperature limit, GASKET2 has the correct asymptotic functional behavior

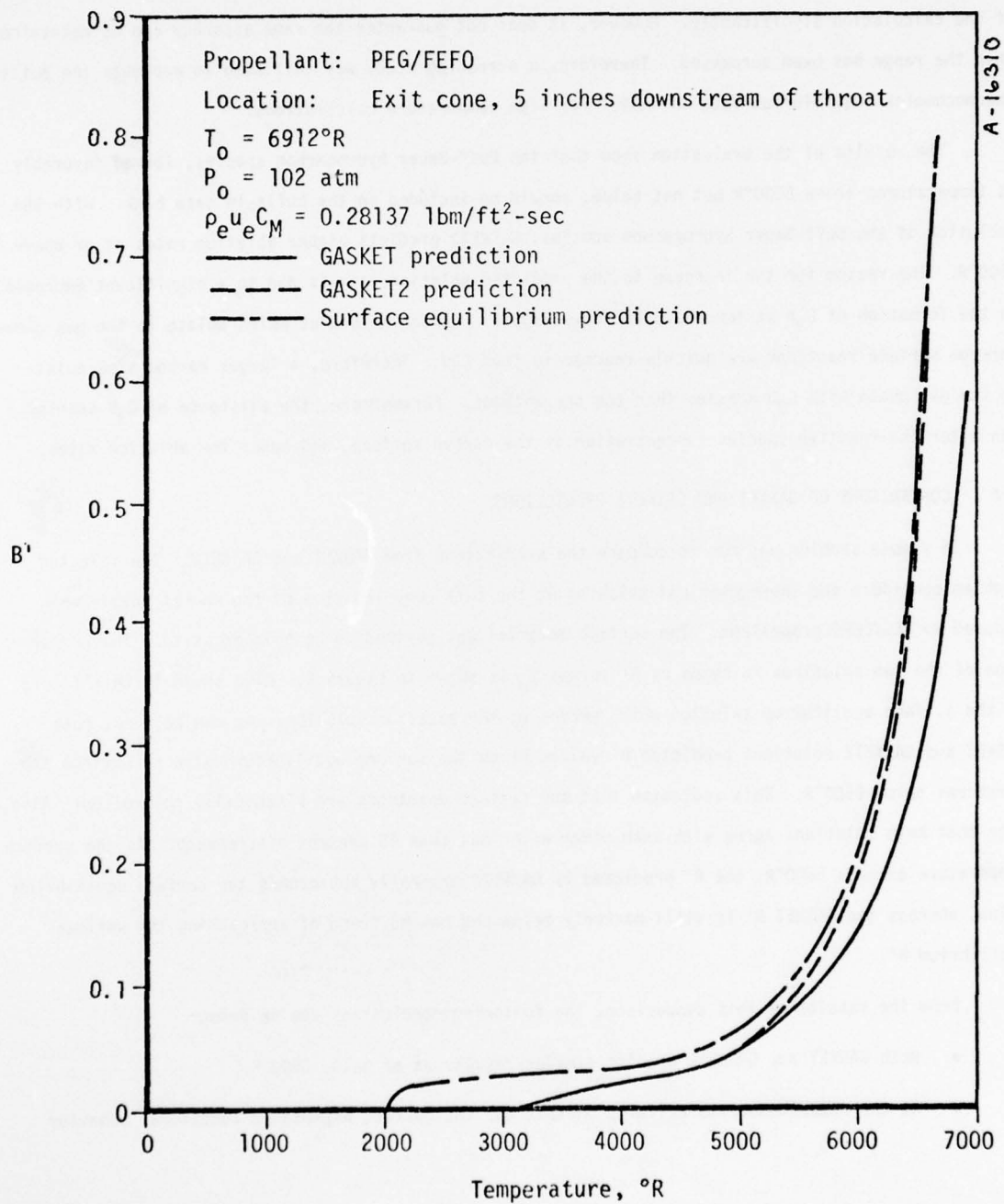


Figure 2. Comparison of GASKET and GASKET2 predictions.

1.5 DESCRIPTION OF GASKET2 OUTPUT ON TRANSPORT PROPERTIES AND SURFACE KINETICS INFORMATION

There are concerns by the users of whether GASKET2 computes transport properties based on both gas and condensed phase species, or on gas phase species alone. It is the purpose of this section to clarify that these properties are computed based on gas phase species only. The reason for neglecting condensed species is due to the common belief within the rocket community that condensed species have a small influence on boundary layer events.* For those users who also use ACE (Aerotherm Chemical Equilibrium code) to perform their inviscid flow field calculations, it should be noted that those transport properties are calculated including both gas and condensed phase species. Therefore, the user should evaluate the implications if those transport properties are being used.

For those users who are interested in obtaining information on how each individual heterogeneous reaction contributes to the total ablation rate, this information is also contained in the GASKET2 output. As an illustration, part of the GASKET2 output was extracted and presented in Figures 3 and 4. Figure 3 shows the printout of the built-in or input surface kinetic constants for each surface reaction. Note that the preexponential factor is normalized by the mass transfer coefficient ($\rho_e u_e C_M$). Shown at the bottom of Figure 4 for each surface reaction are the ablation rate and the ratio of the forward rate and the backward rate indicating how close the reaction is to being in equilibrium. By summing the net rates of all the surface reactions according to the following equation, the sum should be equal to B' .

$$B' = MW_{C*} \sum_{i=1}^N v_{C*i} [\text{Net Rate}]_i$$

N is the total number of surface reactions, and v_{C*i} is the stoichmetric coefficient of carbon for reaction i which can be obtained from the printout for surface kinetics information (see Figure 3).

*This is probably a valid assumption for regions near the nozzle throat; however, the noscap and exit cone regions must be evaluated more carefully.

TRANSFER COEFFICIENT RHOF*UE*CM= .94900+00

KINETIC

REACTION--- 1

1.00H2O +1.00C* -->1.00CO +1.00H2

INHIBITION TERMS

252.67H2O

541A.31CO2

.05CO

.00H2

POISONING TERMS

PRE-EXPONENT FACTOR .726+06 ACTIVATION ENERGY .102+06 T EXPONENT .433+00 8 8 0

8

REACTION--- 8

5.00C* -->1.00CS

PRE-EXPONENT FACTOR .101-02 ACTIVATION ENERGY .000 T EXPONENT -.500+00 99 8 0

Figure 3. Typical GASKET2 output.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
 MASS TRANSFER COEFFICIENT ROUCM = .94900+00
 RHO V WALL/RHOE UE CM = .13546+00 BPRIME = .13546+00

STATE ADJACENT TO THE SURFACE
 TEMP = 6119.9999 DEG R = 3400.0000 DEG K PRESS = 31.47837 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LBM	.90329+03	.00000	.90329+03
ENTROPY - BTU/LBM DEG R	.28345+01	.00000	.00000
DENSITY - LBM/FT3	.15112+00		.15112+00
MOLECULAR WEIGHT	21.4580	.0000	21.4580

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM)	
1= .65142-03 2= .13623-02 3= .44967-02 4= .37470-04 5= .71843-04	
6= .28152-04 7= .13733-05 8= .21875-07	

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES

1= .14303+01 2= .14383+01 3= .20688+01 4= .14383+01 5= .20698+01
6= .29756+01 7= .42798+01 8= .61557+01

Figure 4. Typical GASKET2 output.

SECTION 2

INPUT INSTRUCTION MANUAL

2.1 GASKET2 INPUT

This section defines the format and significance of each field of the input data card deck for the modified Aerotherm Graphite Surface Kinetics (GASKET2) program. In the most general case, the input consists of eight card sets. These are:

1. CONTROL CARD
2. FROZEN-EDGE TEMPERATURE ARRAY
3. SURFACE TEMPERATURE ARRAY
4. ELEMENTAL COMPOSITION
5. DIFFUSION FACTOR DATA
6. SPECIES THERMOCHEMICAL EQUILIBRIUM DATA
7. OBLIQUE OR NORMAL SHOCK DATA
8. REACTION RATE DATA

Card Set 1 is a control card which contains a 10-element array, KRK(I). This array controls most of the program options and tells the program what to expect from the remaining card sets. Few problems require all card sets since, in most cases, the user will wish to utilize the data built into the GASKET program to replace card sets 2, 3, 5, 6, and 8. The card sets are described in detail in this section.

CARD SET 1 - CONTROL CARD (2 Cards)

CARD 1

FIELD 1 (Columns 1-10, Format 10I1) the variable array KRK(10) which is used to control the various program options.

COLUMN 1 -- EDGE THERMODYNAMIC STATE

0 Input
 1 Static state behind shock, upstream conditions input
 (card set 7)
 2 Same as 1, except stagnation state behind shock
 3 Isentropic expansion from input chamber conditions
 4 Static state behind shock, upstream conditions calculated
 via isentropic expansion from input chamber conditions
 (card set 7)
 5 Same as 4, except stagnation state behind shock

COLUMN 2 -- STATE OPTION (pertains to Z, cols. 11-20 of this card)

0 Assigned temperature
 2 Assigned enthalpy
 3 Assigned entropy

COLUMN 3 -- SPECIES THERMOCHEMICAL DATA

0 9 Use built-in thermochemistry data
 0 Use built-in diffusion factor data
 12 Read from cards new thermochemistry data, and if provided,
 diffusion factor data
 2 Print out thermochemistry data for allowable species
 9 Update diffusion factor data

COLUMN 4 -- CARBON SURFACE SPECIFICATION

1 Layer-oriented PG
 2 Edge-oriented PG
 3 General Bulk Graphite
 4 G-90 Bulk Graphite
 5 ATJ Bulk Graphite
 6 Carbitex 700 Carbon/Carbon
 7 PC-901 Carbon/Carbon
 8 SiC/PG

COLUMN 5 -- FROZEN -- EDGE TEMPERATURE ARRAY

0 Bypass this calculation
 1 Use built-in temperature array
 2 Read the temperature array from cards (card set 2)

COLUMN 6 -- SURFACE TEMPERATURE ARRAY

0 Bypass this calculation
 1 Use built-in temperature array
 2 Read the temperature array from cards (card set 3)

NOTE: When $KRK(6) \geq 1$, GASKET2 automatically provides two
 equilibrium surface calculations, for 500°K and 1000°K,
 with the restriction of zero ablation; this is done
 in order to provide tables for CMA and/or ASTHMA
 which facilitate smooth interpolation.

COLUMN 7 -- KINETIC CONSTANTS

0 Use built-in Arrhenius/Langmuir model
 1 3 Read from cards the pre-exponential factor, B'_i (lb mole
 reaction/ft²sec), activation energy, E_m (cal/gm mole), and
 temperature exponent, ϕ_m for both reaction and sublimation
 kinetics
 23 Read from cards the partial pressure multiplicative factors,
 ψ_{jm} and F_{jm} (atm⁻¹) for reaction kinetics only

COLUMN 8 -- EDGE GAS ELEMENTAL COMPOSITION

- 1 e.g. does not contain H or O (Kinetically inert surface)
- 2 e.g. does not contain H (reaction 2. only)
- 3 e.g. does not contain O (reaction 3. only)
- 4 e.g. contains both H and O (reactions 1., 2., and 3.)

COLUMN 9 -- PUNCHED CARD OUTPUT

- 0 No punched card output
- 1 3 Punch a card appropriate to CMA input for each convergent frozen edge or surface solution
- 23 Punch a card appropriate to ASTHMA input for each convergent frozen edge or surface solution

COLUMN 10 -- DIAGNOSTIC OUTPUT CONTROL

- 0 No diagnostic output
- 1 Output a single line of diagnostic information per iteration
- j (Where j is a digit greater than one) output full diagnostic information for 5(j-1) iterations and output a single line of diagnostic information for subsequent iterations.

FIELD 2 (Columns 11-20, Format F10.5) Thermodynamic State Variable, Z

- 1) a) If $KRK(2) = 0$, Z is assigned to temperature, °K
- b) If $KRK(2) = 2$, Z is assigned to enthalpy, cal/gm
- c) If $KRK(2) = 3$, Z is assigned to entropy, cal/gm°K
- 2) a) If $KRK(1) = 0$, Z pertains to the edge state
- b) If $KRK(1) = 1$ or 2, Z pertains to the thermodynamic state upstream of a shock wave
- c) If $KRK(1) > 3$, Z pertains to the chamber thermodynamic state
 - i) If $PC = 0$, Z pertains to the actual chamber state
 - ii) If $PC \neq 0$, Z pertains to the ideal chamber state (see PC, Cols. 41-50 of this card)

FIELD 3 (Columns 21-30, Format F10.5) Pressure, PR atm

- 1) If $KRK(1) = 0$, PR pertains to the edge thermodynamic state
- 2) If $KRK(1) \neq 0$, PR pertains to the actual chamber thermodynamic state or to the thermodynamic state upstream of a shock wave

FIELD 4 (Columns 31-40, Format F10.5) Edge or Shock Upstream Thermodynamic State, ZE

- 1) If $KRK(1) \leq 2$, this field is ignored
- 2) a) If $ZE > 0$, it is assigned as the pressure, atm, at either the edge ($KRK(1) = 3$), or the upstream side of a shock wave ($KRK(1) = 4$ or 5)
- b) If $ZE < 0$, it is assigned as the Mach number at either the edge ($KRK(1) = 3$) or the upstream side of a shock wave ($KRK(1) = 4$ or 5)

FIELD 5 (Columns 41-50, Format F10.5) Ideal Chamber Pressure, PC atm

FIELD 6 (Columns 51-60, Format F10.5) Mass Transfer Coefficient, ROUCM lbm/ft²sec

FIELD 7 (Columns 61-70, Format F10.5) Diffusion Coefficient Exponent for Unequal Diffusion Coefficient Model, GAMER

- 1) If GAMER = 0.0, it is automatically set to 2/3 (this value is appropriate for most calculations)
- 2) If GAMER = 10⁻⁵, the diffusion model reduces to equal diffusion coefficients

FIELD 8 (Columns 71-80, Format 2A4,A4) Job Title, TILE (3)

CARD 2 If $KRK(4) \neq 8$, skip this card

FIELD 1 (Columns 1-10, Format F10.0) Mass fraction of SiC in SiC/PG

CARD SET 2 — FROZEN-EDGE TEMPERATURE ARRAY TFA(I) (number of cards = no. of temperatures + 1)

- 1) If KRK(5) = 0 or 1, skip this card set
- 2) If KRK(5) = 2, read in an array of no more than eight temperatures, TFA(I) °K

CARD(S) 1,2,... (Columns 1-10, Format F10.5) one temperature per card

FINAL CARD blank

NOTE: The TFA(I) array built into GASKET2 contains temperatures from 500 to 4000°K in 500°K increments

CARD SET 3 — SURFACE TEMPERATURE ARRAY TSA(I) (number of cards = no. of temperatures + 1)

- 1) If KRK(6) = 0 or 1, skip this card set
- 2) If KRK(6) = 2, read in an array of no more than fifteen temperatures, TSA(I) °K

CARD(S) 1,2,... (Columns 1-10, Format F10.5) one temperature per card

FINAL CARD blank

NOTE: The TSA(I) array built into GASKET2 contains temperatures from 1200 to 4000°K in 2000°K increments. Also, whenever KRK(6) \geq 1 two surface equilibrium, zero-ablation calculations are performed for surface temperatures of 500 and 1000°K.

CARD SET 4 — ELEMENTAL COMPOSITION (number of cards = no. of elements +1)

CARD 1 (Columns 1-3, Format I3) the number of elements in the system

CARD 2,3,4 . . . (one card for each element)

FIELD 1 (Columns 1-3, Format I3) the atomic number of the element

FIELD 2 (Columns 4-15, Format 3A4) the name of the element (for output identification only)

FIELD 3 (Columns 16-25, Format F10.5) the atomic weight of the element

FIELD 4 (Columns 26-35, Format F10.5) the relative amount of the element in the edge gas (this is the same as the relative amount of the element in the chamber or at the upstream side of a shock wave, since elements are conserved)

- 1) Positive values are in relative gram-atomic-weights (or moles)
- 2) Negative values are in relative masses

FIELD 5 (Columns 46-55, Format F10.5) the relative amount of the element in the surface material (the present version of GASKET2 allows the surface to be comprised of carbon only; hence, the quantity 1.0 must be entered in this field for the element carbon)

CARD SET 5 — DIFFUSION FACTOR DATA (number of cards = 1/4 x (7 + no. of data items, e.g., diffusion factors, reference molecular weight, diffusion exponent)

- 1) If KRK(3) = 0, this card set must be skipped
- 2) If KRK(3) = 1,2,3, or 4, this card set may be skipped
- 3) If KRK(3) = 9, this card set must not be skipped

CARD 1 (Columns 1-3, Format I3) the total number of data items (e.g., diffusion factors, reference molecular weight, diffusion exponent) to be entered

Diffusion factors may be specified for any or all species individually and/or diffusion factors may be calculated via

$$\text{Diffusion Factor} = \left(\frac{\text{Molec.Wt.}}{\text{REFM}} \right)^{\text{FFA}}$$

where REFM and FFA may be specified here. For species for which diffusion factors are not specified individually, diffusion factors will be calculated via the above correlation, and if REFM and FFA are not specified, diffusion factors will be calculated from the above with REFM = 23.4 and FFA = 0.431.

CARD(S) 2,3, . . .

FIELDS 1,3,5,7 (Columns 1-8, 21-28, 41-48, 61-68, each Format 2A4)

The "name" of the species for which data is to be provided, exactly as it appears in columns 73-80 of the first card of the 3 thermochemical data cards (card set 6) for that species. To specify values of REFM or FFA in the next field, enter the alpha characters "REFM" or "FFA" respectively here.

FIELDS 2,4,6,8 (Columns 9-20, 29-40, 49-60, 69-80, each Format E12.4)

- 1) If the name of a chemical species was entered in the preceding field, this number is presumed to be a diffusion factor.
- 2) If the name REFM or FFA was entered in the preceding field, enter the desired values of REFM or FFA respectively in this field.

The diffusion factors introduced into the solution in this manner replace either the values set automatically (see card 1 above) if the species thermochemical data are read from cards or tape, or the values built into the GASKET2 program (see Volume II).

NOTE: If KRK(3) = 9 and KRK(1) = 1,2,4 or 5, this card set must follow the OBLIQUE OR NORMAL SHOCK DATA card set; if KRK(3) = 1,2,3, or 4 this card set, if used, precedes the SPECIES THERMOCHEMICAL EQUILIBRIUM DATA card set.

CARD SET 6 - SPECIES THERMOCHEMICAL EQUILIBRIUM DATA (number of cards = 1 + 3 x no. of species)

- 1) If KRK(3) = 0 or 9, skip this card set
- 2) If KRK(3) = 1,2,3, or 4, read in this card set; there are three of these cards for each molecular, atomic, or condensed species; the end of this card set is signaled by a blank card

CARDS 1,4,7 . . . Describe the elemental composition of the species and establish its name designation

FIELDS 1,3,5, . . . , 13 (one for each element in the species)
(Columns 1-3, 7-9, 13-15, . . . , 37-39, each format F3.0)

The number of atoms (of atomic number given in the following field) in a molecule of this species

(If field 1 is zero, this card is presumed to represent the end of card set 6)

FIELDS 2,4,6,. . . , 14. (one for each element in the species)
(Columns 4-6, 10-12, 16-18,. . . , 40-42, each format I3)

The atomic numbers of the elements in the molecule (the number of atoms of which was given in the previous field)

(If field 2 is zero, this card is presumed to be the first card of card set 5)

FIELD 15 (Columns 42-72, Format 7A4A2) the source and date of the thermochemical data for this specie. Used for output only

FIELD 16 (Columns 73-80, Format 2A4) the name designation of this species (e.g., AL2O3). This variable is used for output and as a means of identifying data entered in card set 5

CARDS 2,5,8. . . Lower temperature range thermochemical data

FIELDS 1,2,3,4,5 and 6 (Columns 1-54, Format 6E9.6) Input the 5 constants (F1,F2, F3,F4,F5,F6) appropriate to the lower temperature range of the thermodynamic data for this species. These constants are defined as follows, where T is in °K:

F1 = the heat of formation of the species at 298°K from the JANNAF base state (elements in most natural form at 298°K) in cal/mole

F2 = the enthalpy change of the species from 298°K to 3000°K in cal/mole

F3,F4 and F5 are defined by a curve fit to the heat capacity at constant pressure of the form:

$$C_p = F3 + F4 T + \frac{F5}{T^2} \text{ in cal/mole } ^\circ\text{K}$$

F6 = the entropy of the species at 3000°K in cal/mole °K

FIELD 7 (Columns 61-66, Format F6.0) the upper limit of the lower temperature range in °K

FIELD 8 (Column 67, Format I1) the phase specification:

- 1 signifies gaseous species
- 2 signifies solid species
- 3 signifies liquid species

The only phase combination allowed in one three card set is solid-liquid in which case a 2 and 3 would appear in fields 8 of cards 2 and 3, respectively.

CARDS 3,6,9. . . Upper temperature range thermochemical data

These cards are the same as cards 2,5,8. . . except use constants for the upper temperature range and field 7 is ignored

LAST CARD OF CARD SET 6 MUST BE BLANK

The end of the species thermochemical data is signified by a blank card. Hence, the last card of card set 6 must be a blank card.

NOTE: If this data is read in on cards, the atomic number of C* must be 106, rather than the actual value of 6. Finally, all condensed phase species (except C*) must follow the gas phase species.

CARD SET 7 — OBLIQUE OR NORMAL SHOCK DATA (1 card)

- 1) If $KRK(1) = 0$ or 3, skip this card set
 - 2) If $KRK(1) = 1, 2, 4$, or 5, this card set must be read in
- FIELD 1 (Column 1, Format I1) Input the variable KVH which determines how the velocity ahead of the shock, the static enthalpy ahead of the shock, and the total enthalpy are calculated (since total enthalpy = static enthalpy + $1/2$ velocity²)
- If $KVH = 1$, velocity is calculated from specified total and static enthalpy
- If $KVH = 2$, total enthalpy is calculated from specified static enthalpy and velocity
- If $KVH = 3$, static enthalpy is calculated from specified total enthalpy and velocity
- FIELD 2 (Columns 2-10, Format F9.4) The velocity variable, UR (this field is ignored if $KVH = 1$)
- If $UR \neq -9999$, then UR is assigned to SVL , the velocity upstream of the shock in ft/sec
- If $UR = -9999$, the velocity calculated in the prior solution is assigned to SVL
- FIELD 3 (Columns 11-20, Format F10.4) The total enthalpy variable, HTR (this field is ignored if $KVH = 2$)
- If $HTR \neq 0$, then HTR is assigned to HCH , the total enthalpy of the system in BTU/lbm
- If $HTR = 0$, HCH is unchanged
- FIELD 4 (Columns 21-30, Format F10.4) the static enthalpy variable, HSR (This field is ignored if $KVH = 3$)
- If $HSR \neq -9999$, then HSR is assigned to $SH1$, the static enthalpy upstream of the shock in BTU/lbm
- If $HSR = -9999$, the static enthalpy calculated in the prior solution is assigned to $SH1$
- FIELD 5 (Columns 41-50, Format F10.4) the shock angle (0.0 for a normal shock) in degrees

CARD SET 8 — REACTION RATE DATA (number of cards = $3 \times MT - 10$ at maximum)

- 1) If $KRK(7) = 0$, skip this card set
- 2) If $KRK(7) = 1$ or 3, the first subset of this card set must be read in
- 3) If $KRK(7) = 2$ or 3, the second subset of this card set must be read in

First Subset: MT cards

CARDS 1, 2, . . . , MT

- FIELD 1 (Columns 1-10, Format E10.4), $FKF(M)$ the preexponential factor for the Mth reaction, lb mole/ft²sec atm
- FIELD 2 (Columns 11-20, Format E10.4), $EAK(M)$, the activation energy for the Mth forward reaction, cal/gm mole
- FIELD 3 (Columns 21-30, Format E10.4), $EXK(M)$, the temperature exponent for the Mth reaction

Second Subset: 2 x MT -10 cards

CARDS MT + 1, MT + 3, MT + 5; . . . 3 x MT -13, 3 x MT -11;

FIELDS 1-6 (Columns 1-10 x 6, Format 8F10.6, inhibiting specie partial pressure coefficient, PSI (J,M), J = 1, 6 atm⁻¹)

CARDS MT + 2, MT + 4; MT + 6, 7, . . . 3 x MT - 12, 3 x MT -10

FIELDS 1-6 (Columns 1-10 x 6, Format 8F10.6, inhibiting specie partial pressure coefficient FKK(J,M), J = 1, 6, atm⁻¹)

NOTE: MT = no. of reactions

1) IF KRK(8) = 1, MT = 0, kinetics ignored

2) If KRK(8) = 2, MT = 1 + 5 sublimation kinetics reactions

M = 1 $C^* + CO_2 \rightleftharpoons 2CO$

J = 1 CO_2

J = 2 CO

3) If KRK(8) = 3, MT = 1 + 5 sublimation kinetics reactions

M = 1 $2C^* + H_2 \rightleftharpoons C_2H_2$

J = 1 H_2

4) If KRK(8) = 4, MT = 3 + 5 sublimation kinetics reactions

M = 1 $C^* + H_2O \rightleftharpoons CO + H_2$

M = 2 $C^* + CO_2 \rightleftharpoons 2CO$

M = 3 $2C^* + H_2 \rightleftharpoons C_2H_2$

J = 1 H_2O

J = 2 CO_2

J = 3 CO

J = 4 H_2

J = 5 CLH

J = 6 FH

TO TERMINATE A JOB

KRK(1) = 8 on final card

MULTIPLE JOBS

1) Several jobs may be loaded back to back, with a control card signifying the start of each new job:

CONTROL CARD #1

:

ELEMENTAL COMPOSITION #1

:

additional data as required for job #1

:

CONTROL CARD #2

:

ELEMENTAL COMPOSITION #2

:

additional data as required for job #2

:

KRK(1) = 8

- 2) If jobs following the first job have the same elemental composition as the first job, Card Set #4 (ELEMENTAL COMPOSITION) may be replaced by a single blank card for all jobs after the first:

CONTROL CARD #1

:

ELEMENTAL COMPOSITION #1

:

additional data as required for job #1

:

CONTROL CARD #2

:

blank card

:

additional data as required for job #2

:

KRK(1) = 8

2.2 NEW FORTRAN VARIABLE NAMES USED IN GASKET2

This section describes the names and definitions of the newly introduced FORTRAN variables resulting from the computer code modification. Since this is an addendum to Reference 1, similar format and abbreviations are adopted here.

LIST OF NEW FORTRAN VARIABLES APPEARING IN COMMON STATEMENTS, GASKET2

<u>Variable Name</u>	<u>Description</u>	<u>Routine(s) in Which Variable is Utilized</u>
CPER	Mass fraction of carbon in SiC/PG	KN,IM
FKKS(M)	Same definition as FFX(M)	T,KT
INP(M)	Chemical reaction index (8 = oxidation, 99 = sublimation)	T,KT
NMP(N,M)	Index used to locate the reactants in the thermochemical equilibrium data	T,KT
NMR(N,M)	Index used to locate the products in the thermochemical equilibrium data	T,KT
NPF(N,M)	Index used to locate the poisoning species in the thermochemical equilibrium data	T,KT
NPP(N,M)	Index used to locate the inhibiting species in the thermochemical equilibrium data	T,KT
PERCT	Mass fraction of SiC in SiC/PG	KN,IM
SIPER	Mass fraction of Si in SiC/PG	KN,IM

LIST OF NEW FORTRAN VARIABLES APPEARING IN SUBROUTINE KINET, GASKET2

<u>Variable Name</u>	<u>Description</u>
DBDP	Locally defined variable
VLNI	$(-H/RT + S/R)$ of reactant
VLNII	$(-H/RT + S/R)$ of product
VNNMR	Local variable for $VNU(I,J)$ of reactants
VNNMP	Local variable for $VNU(I,J)$ of products
VNNPP	Local variable for $VNU(I,J)$ of inhibiting species
VNNPF	Local variable for $VNU(I,J)$ of poisoning species
XX(M)	Saved value of preexponential constant

LIST OF NEW FORTRAN VARIABLES APPEARING IN SUBROUTINE THERM GASKET2

Variable Name	
FKKD(I,J,K)	Built-in values for poisoning species
FNAM(I,IZ)	Temporary variable for the chemical symbol of the species involved in the chemical reaction ($IZ < 4$ reactants, $5 < IZ < 8$ products, $9 < IZ < 16$ inhibiting species, $17 < IZ < 24$ poisoning species)
FSS(I)	Sublimation constants built-in value
IIZ	Index to define total number of species involved in the chemical reactions
INHB(I)	First four alphanumeric characters for the chemical symbol of the inhibiting species
IRX	Flag indicating type of surface reaction (1 = reactions involved H ₂ O species, 2 = reaction involved O species only, 3 = reaction involved H species only)
MS	Total number of sublimation kinetic reactions
POIS(I,J)	First four alphanumeric characters for the chemical symbol of the poisoning species
PRSP(I,J)	First four alphanumeric characters for the chemical symbol of products
PSID(I,J,K)	Built-in values for inhibiting coefficients
RXSP(I,J)	First four alphanumeric characters for the chemical symbol of reactants
RUCM	Same as ROUCM
SUBC	Locally defined variable

2.3 LISTING OF THE MODIFIED SUBROUTINES

The listing of the following subroutines are given in this section:

- IMELM
- INPUT
- KINET
- OUTPUT
- THERM
- KININ
- ZIPIN
- AFMAT
- ALPST
- BELCH
- CRECT
- GASKET
- MAT 1
- MAT 2
- MAT 3
- PROPS
- SCALE

The modifications made to the subroutines are shown in the right hand side column. The notation "***-n" means that n lines of FORTRAN statements have been deleted preceeding the line where "***-n" appeared. "*COR" indicates the location where new FORTRAN statements are inserted.

[illegible]


```

112.
113.
114.
115.
116.
117.
118.
119.
120.
121.
122.
123.

120  TOL(L)=TG(L,L)*DM(I,K)*TK(K,L)
125  RETURN
130  WRITE (ROUT,150)
135  STOP
140  C
145  FORMAT (13,3A4,4F10.5)
150  FORMAT (54HRELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS
      1 /4XGHA1,NO.3X7HELEMT4X9HATC1C 4TSX21HCOF GAS
      213.3X3A4,4F10.5,2F13.7))
150  FORMAT (////40X,31HPROGRAM LIMITED TO 10 ELEMENTS )
      END
124  IMEL0124
125  IMEL0125
126  IMEL0126
127  IMEL0127
128  IMEL0128
129  IMEL0129
130  IMEL0130
131  IMEL0131
132  IMEL0132
133  IMEL0133
134  IMEL0134
135  IMEL0135

```

1.	SUBROUTINE INPUT	TEMP0001
2.	CONFORM/ACF1/ACF2/ACF3/ACF4/ACF5/ACF6/ACF7/ACF8/ACF9/ACF10/ACF11/ACF12/ACF13/ACF14/ACF15/ACF16/ACF17/ACF18/ACF19/ACF20/ACF21/ACF22/ACF23/ACF24/ACF25/ACF26/ACF27/ACF28/ACF29/ACF30/ACF31/ACF32/ACF33/ACF34/ACF35/ACF36/ACF37/ACF38/ACF39/ACF40/ACF41/ACF42/ACF43/ACF44/ACF45/ACF46/ACF47/ACF48/ACF49/ACF50/ACF51/ACF52/ACF53/ACF54/ACF55/ACF56/ACF57/ACF58/ACF59/ACF60/ACF61/ACF62/ACF63/ACF64/ACF65/ACF66/ACF67/ACF68/ACF69/ACF70/ACF71/ACF72/ACF73/ACF74/ACF75/ACF76/ACF77/ACF78/ACF79/ACF80/ACF81/ACF82/ACF83/ACF84/ACF85/ACF86/ACF87/ACF88/ACF89/ACF90/ACF91/ACF92/ACF93/ACF94/ACF95/ACF96/ACF97/ACF98/ACF99/ACF100/ACF101/ACF102/ACF103/ACF104/ACF105/ACF106/ACF107/ACF108/ACF109/ACF110/ACF111/ACF112/ACF113/ACF114/ACF115/ACF116/ACF117/ACF118/ACF119/ACF120/ACF121/ACF122/ACF123/ACF124/ACF125/ACF126/ACF127/ACF128/ACF129/ACF130/ACF131/ACF132/ACF133/ACF134/ACF135/ACF136/ACF137/ACF138/ACF139/ACF140/ACF141/ACF142/ACF143/ACF144/ACF145/ACF146/ACF147/ACF148/ACF149/ACF150/ACF151/ACF152/ACF153/ACF154/ACF155/ACF156/ACF157/ACF158/ACF159/ACF160/ACF161/ACF162/ACF163/ACF164/ACF165/ACF166/ACF167/ACF168/ACF169/ACF170/ACF171/ACF172/ACF173/ACF174/ACF175/ACF176/ACF177/ACF178/ACF179/ACF180/ACF181/ACF182/ACF183/ACF184/ACF185/ACF186/ACF187/ACF188/ACF189/ACF190/ACF191/ACF192/ACF193/ACF194/ACF195/ACF196/ACF197/ACF198/ACF199/ACF200/ACF201/ACF202/ACF203/ACF204/ACF205/ACF206/ACF207/ACF208/ACF209/ACF210/ACF211/ACF212/ACF213/ACF214/ACF215/ACF216/ACF217/ACF218/ACF219/ACF220/ACF221/ACF222/ACF223/ACF224/ACF225/ACF226/ACF227/ACF228/ACF229/ACF230/ACF231/ACF232/ACF233/ACF234/ACF235/ACF236/ACF237/ACF238/ACF239/ACF240/ACF241/ACF242/ACF243/ACF244/ACF245/ACF246/ACF247/ACF248/ACF249/ACF250/ACF251/ACF252/ACF253/ACF254/ACF255/ACF256/ACF257/ACF258/ACF259/ACF260/ACF261/ACF262/ACF263/ACF264/ACF265/ACF266/ACF267/ACF268/ACF269/ACF270/ACF271/ACF272/ACF273/ACF274/ACF275/ACF276/ACF277/ACF278/ACF279/ACF280/ACF281/ACF282/ACF283/ACF284/ACF285/ACF286/ACF287/ACF288/ACF289/ACF290/ACF291/ACF292/ACF293/ACF294/ACF295/ACF296/ACF297/ACF298/ACF299/ACF300/ACF301/ACF302/ACF303/ACF304/ACF305/ACF306/ACF307/ACF308/ACF309/ACF310/ACF311/ACF312/ACF313/ACF314/ACF315/ACF316/ACF317/ACF318/ACF319/ACF320/ACF321/ACF322/ACF323/ACF324/ACF325/ACF326/ACF327/ACF328/ACF329/ACF330/ACF331/ACF332/ACF333/ACF334/ACF335/ACF336/ACF337/ACF338/ACF339/ACF340/ACF341/ACF342/ACF343/ACF344/ACF345/ACF346/ACF347/ACF348/ACF349/ACF350/ACF351/ACF352/ACF353/ACF354/ACF355/ACF356/ACF357/ACF358/ACF359/ACF360/ACF361/ACF362/ACF363/ACF364/ACF365/ACF366/ACF367/ACF368/ACF369/ACF370/ACF371/ACF372/ACF373/ACF374/ACF375/ACF376/ACF377/ACF378/ACF379/ACF380/ACF381/ACF382/ACF383/ACF384/ACF385/ACF386/ACF387/ACF388/ACF389/ACF390/ACF391/ACF392/ACF393/ACF394/ACF395/ACF396/ACF397/ACF398/ACF399/ACF400/ACF401/ACF402/ACF403/ACF404/ACF405/ACF406/ACF407/ACF408/ACF409/ACF410/ACF411/ACF412/ACF413/ACF414/ACF415/ACF416/ACF417/ACF418/ACF419/ACF420/ACF421/ACF422/ACF423/ACF424/ACF425/ACF426/ACF427/ACF428/ACF429/ACF430/ACF431/ACF432/ACF433/ACF434/ACF435/ACF436/ACF437/ACF438/ACF439/ACF440/ACF441/ACF442/ACF443/ACF444/ACF445/ACF446/ACF447/ACF448/ACF449/ACF450/ACF451/ACF452/ACF453/ACF454/ACF455/ACF456/ACF457/ACF458/ACF459/ACF460/ACF461/ACF462/ACF463/ACF464/ACF465/ACF466/ACF467/ACF468/ACF469/ACF470/ACF471/ACF472/ACF473/ACF474/ACF475/ACF476/ACF477/ACF478/ACF479/ACF480/ACF481/ACF482/ACF483/ACF484/ACF485/ACF486/ACF487/ACF488/ACF489/ACF490/ACF491/ACF492/ACF493/ACF494/ACF495/ACF496/ACF497/ACF498/ACF499/ACF500/ACF501/ACF502/ACF503/ACF504/ACF505/ACF506/ACF507/ACF508/ACF509/ACF510/ACF511/ACF512/ACF513/ACF514/ACF515/ACF516/ACF517/ACF518/ACF519/ACF520/ACF521/ACF522/ACF523/ACF524/ACF525/ACF526/ACF527/ACF528/ACF529/ACF530/ACF531/ACF532/ACF533/ACF534/ACF535/ACF536/ACF537/ACF538/ACF539/ACF540/ACF541/ACF542/ACF543/ACF544/ACF545/ACF546/ACF547/ACF548/ACF549/ACF550/ACF551/ACF552/ACF553/ACF554/ACF555/ACF556/ACF557/ACF558/ACF559/ACF560/ACF561/ACF562/ACF563/ACF564/ACF565/ACF566/ACF567/ACF568/ACF569/ACF570/ACF571/ACF572/ACF573/ACF574/ACF575/ACF576/ACF577/ACF578/ACF579/ACF580/ACF581/ACF582/ACF583/ACF584/ACF585/ACF586/ACF587/ACF588/ACF589/ACF590/ACF591/ACF592/ACF593/ACF594/ACF595/ACF596/ACF597/ACF598/ACF599/ACF600/ACF601/ACF602/ACF603/ACF604/ACF605/ACF606/ACF607/ACF608/ACF609/ACF610/ACF611/ACF612/ACF613/ACF614/ACF615/ACF616/ACF617/ACF618/ACF619/ACF620/ACF621/ACF622/ACF623/ACF624/ACF625/ACF626/ACF627/ACF628/ACF629/ACF630/ACF631/ACF632/ACF633/ACF634/ACF635/ACF636/ACF637/ACF638/ACF639/ACF640/ACF641/ACF642/ACF643/ACF644/ACF645/ACF646/ACF647/ACF648/ACF649/ACF650/ACF651/ACF652/ACF653/ACF654/ACF655/ACF656/ACF657/ACF658/ACF659/ACF660/ACF661/ACF662/ACF663/ACF664/ACF665/ACF666/ACF667/ACF668/ACF669/ACF670/ACF671/ACF672/ACF673/ACF674/ACF675/ACF676/ACF677/ACF678/ACF679/ACF680/ACF681/ACF682/ACF683/ACF684/ACF685/ACF686/ACF687/ACF688/ACF689/ACF690/ACF6	

[illegible]

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[illegible]

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35

454.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4454	*COR
455.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4455	*COR
456.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4456	*COR
457.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4457	*COR
458.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4458	*COR
459.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4459	*COR
460.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4460	*COR
461.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4461	*COR
462.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4462	*COR
463.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4463	*COR
464.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/63	44H	INPU4464	*COR
465.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/63	44H	INPU4465	*COR
466.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/64	44H	INPU4466	*COR
467.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/65	44H	INPU4467	*COR
468.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/65	44H	INPU4468	*COR
469.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/63	44H	INPU4469	*COR
470.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4470	*COR
471.	DATA (SOFCY(T)1=55,746)								
472.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/63	44H	INPU4472	*COR
473.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4473	*COR
474.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4474	*COR
475.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/67	44H	INPU4475	*COR
476.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4476	*COR
477.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/65	44H	INPU4477	*COR
478.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4478	*COR
479.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4479	*COR
480.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4480	*COR
481.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/62	44H	INPU4481	*COR
482.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4482	*COR
483.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4483	*COR
484.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4484	*COR
485.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4485	*COR
486.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/64	44H	INPU4486	*COR
487.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4487	*COR
488.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4488	*COR
489.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/63	44H	INPU4489	*COR
490.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4490	*COR
491.	DATA (SOFCY(T)1=73,846)								
492.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4492	*COR
493.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4493	*COR
494.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4494	*COR
495.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4495	*COR
496.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4496	*COR
497.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/67	44H	INPU4497	*COR
498.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4498	*COR
499.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4499	*COR
500.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/66	44H	INPU4500	*COR
501.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4501	*COR
502.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4502	*COR
503.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/69	44H	INPU4503	*COR
504.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/70	44H	INPU4504	*COR
505.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/70	44H	INPU4505	*COR
506.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4506	*COR
507.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4507	*COR
508.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/68	44H	INPU4508	*COR
509.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4509	*COR
510.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/61	44H	INPU4510	*COR

[illegible]

568.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/65	4H	4H	INPU568	*COR
569.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/67	4H	4H	INPU569	*COR
570.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/66	4H	4H	INPU570	*COR
571.	DATA (SRCV(1),1E1345,1496)/							*COR
572.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU572	*COR
573.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/70	4H	4H	INPU573	*COR
574.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/66	4H	4H	INPU574	*COR
575.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/66	4H	4H	INPU575	*COR
576.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU576	*COR
577.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/60	4H	4H	INPU577	*COR
578.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/64	4H	4H	INPU578	*COR
579.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU579	*COR
580.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/60	4H	4H	INPU580	*COR
581.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/62	4H	4H	INPU581	*COR
582.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/66	4H	4H	INPU582	*COR
583.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/60	4H	4H	INPU583	*COR
584.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/62	4H	4H	INPU584	*COR
585.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	4H	INPU585	*COR
586.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/61	4H	4H	INPU586	*COR
587.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/63	4H	4H	INPU587	*COR
588.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/64	4H	4H	INPU588	*COR
589.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	4H	INPU589	*COR
590.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	4H	INPU590	*COR
591.	DATA (SRCV(1),1E1497,1648)/							*COR
592.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	4H	INPU592	*COR
593.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/64	4H	4H	INPU593	*COR
594.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	4H	INPU594	*COR
595.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/62	4H	4H	INPU595	*COR
596.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/67	4H	4H	INPU596	*COR
597.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/67	4H	4H	INPU597	*COR
598.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/61	4H	4H	INPU598	*COR
599.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	4H	INPU599	*COR
600.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	4H	INPU600	*COR
601.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	4H	INPU601	*COR
602.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	4H	INPU602	*COR
603.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU603	*COR
604.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/66	4H	4H	INPU604	*COR
605.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU605	*COR
606.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU606	*COR
607.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	4H	INPU607	*COR
608.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU608	*COR
609.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/65	4H	4H	INPU609	*COR
610.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	4H	INPU610	*COR
611.	DATA (SRCV(1),1E1649,1800)/							*COR
612.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/63	4H	4H	INPU612	*COR
613.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/65	4H	4H	INPU613	*COR
614.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	4H	INPU614	*COR
615.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/62	4H	4H	INPU615	*COR
616.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU616	*COR
617.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	4H	INPU617	*COR
618.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	4H	INPU618	*COR
619.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	4H	INPU619	*COR
620.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/65	4H	4H	INPU620	*COR
621.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/63	4H	4H	INPU621	*COR
622.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/63	4H	4H	INPU622	*COR
623.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/60	4H	4H	INPU623	*COR
624.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/63	4H	4H	INPU624	*COR

625.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU625	*COR
626.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU626	*COR
627.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU627	*COR
628.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/63	4H	INPU628	*COR
629.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/63	4H	INPU629	*COR
630.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU630	*COR
631.	DATA (SORCY(1),1=1901,1952)/						
632.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/67	4H	INPU632	*COR
633.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU633	*COR
634.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU634	*COR
635.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU635	*COR
636.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU636	*COR
637.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU637	*COR
638.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU638	*COR
639.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU639	*COR
640.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU640	*COR
641.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU641	*COR
642.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU642	*COR
643.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU643	*COR
644.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/66	4H	INPU644	*COR
645.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/66	4H	INPU645	*COR
646.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU646	*COR
647.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU647	*COR
648.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU648	*COR
649.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU649	*COR
650.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU650	*COR
651.	DATA (SORCY(1),1=1953,2104)/						
652.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/70	4H	INPU652	*COR
653.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU653	*COR
654.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU654	*COR
655.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU655	*COR
656.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU656	*COR
657.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU657	*COR
658.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/66	4H	INPU658	*COR
659.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU659	*COR
660.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU660	*COR
661.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU661	*COR
662.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU662	*COR
663.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU663	*COR
664.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/67	4H	INPU664	*COR
665.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/67	4H	INPU665	*COR
666.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/67	4H	INPU666	*COR
667.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU667	*COR
668.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU668	*COR
669.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU669	*COR
670.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU670	*COR
671.	DATA (SORCY(1),1=2105,2216)/						
672.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU672	*COR
673.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU673	*COR
674.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU674	*COR
675.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU675	*COR
676.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU676	*COR
677.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/60	4H	INPU677	*COR
678.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/60	4H	INPU678	*COR
679.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/61	4H	INPU679	*COR
680.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/61	4H	INPU680	*COR
681.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/70	4H	INPU681	*COR

682.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/70	4H	*COR
683.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/70	4H	*COR
684.	*2HCO,4HJAT	*HHR	2P,4H1H-12,4H2	12,4H/61	4H	*COR
685.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
686.	DATA (SQRX(I),I=2217,2328)/					
687.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
688.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
689.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
690.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
691.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
692.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
693.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
694.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
695.	*2HJU,4HJEF	*4HJAE,4H	6/6,4H1	4H	4H	*COR
696.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/63	4H	*COR
697.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
698.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
699.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/65	4H	*COR
700.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
701.	DATA (SQRX(I),I=2329,2480)/					
702.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/60	4H	*COR
703.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/65	4H	*COR
704.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/62	4H	*COR
705.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/64	4H	*COR
706.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/66	4H	*COR
707.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/70	4H	*COR
708.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
709.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/61	4H	*COR
710.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/62	4H	*COR
711.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/67	4H	*COR
712.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/65	4H	*COR
713.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/66	4H	*COR
714.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/62	4H	*COR
715.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/66	4H	*COR
716.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
717.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	*COR
718.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
719.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
720.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
721.	DATA (SQRX(I),I=2481,2632)/					
722.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
723.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	*COR
724.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/61	4H	*COR
725.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/63	4H	*COR
726.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/63	4H	*COR
727.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
728.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/62	4H	*COR
729.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/69	4H	*COR
730.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/66	4H	*COR
731.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
732.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
733.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
734.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
735.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	*COR
736.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
737.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
738.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/64	4H	*COR

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1195. * 2.4146E+1, 2.3695E+1, 2.2074E+1, 3.5026E+1, 1.2408E+1, 1.1942E+1, INPU1169
1196. * 4.0773E+1, 4.0808E+1, 4.1234E+1, 4.4455E+1, 1.1280E+1, 1.0388E+1, INPU1170
1197. * 6.8219E+0, 6.7984E+0, 3.0774E+1, 3.3646E+1, 3.2724E+1, 4.3491E+1, INPU1171
1198. * 3.3567E+1, 4.0269E+1, 2.5809E+0, 7.5808E+0, 2.8773E+1, 3.4622E+1, INPU1172
1199. * 5.6046E+0, 7.5001E+0, -1.7944E+0, 2.9604E+1, 2.3000E+1, 3.2520E+1, INPU1173
1200. * 4.2931E+0, 7.9250E+0, 1.0222E+1, 1.6000E+1, 1.8114E+1, 2.2002E+1, INPU1174
1201. * 3.2065E+1, 3.2001E+1, 1.7521E+1, 1.0053E+1, 1.5340E+1, INPU1175
1202. * 9.5257E+0, 2.0740E+1, 1.7445E+1, 2.4000E+1, 1.7404E+1, 2.0511E+1, INPU1176
1203. * 5.4604E+0, 6.5000E+0, 1.8374E+1, 3.4558E+1, 2.2462E+1, 2.9020E+1, INPU1177
1204. * 1.1016E+1, 1.3845E+1, 3.0894E+1, 4.0000E+1, 3.5032E+1, 3.9538E+1, INPU1178
1205. * 4.7458E+1, 1.0114E+2, 6.1414E+1, 7.6250E+1, 1.1045E+2, 1.1088E+2, INPU1179
1206. * 3.7206E+1, 6.0372E+1, 7.0681E+0, 4.4321E+1, 3.2377E+1, 3.3346E+1, INPU1180
1207. * 2.2149E+1, 5.5500E+1, 1.2060E+2, 1.1204E+2, 7.0971E+1, 6.6165E+1, INPU1181
1208. * 3.7941E+1, 6.4517E+1, 8.4657E+1, 1.7419E+2, 3.7210E+2, 1.4900E+1, INPU1182
1209. * 1.3631E+1, 2.3636E+1, 2.6043E+1, 4.2291E+1, 5.9686E+1, 6.7238E+1, INPU1183
1210. * 2.9515E+1, 2.7617E+1, 2.8410E+1, 2.7439E+1, 5.1062E+1, 6.0000E+1, INPU1184
1211. DATA (BOX(1),I=1,108)/
1212. * 7.3366E-4, 2.0963E-4, 9.3467E-4, 3.6202E-4, 1.8325E-3, 2.3113E-4, INPU1186
1213. * 4.4145E-4, 4.6597E-5, 2.4001E-4, 2.1613E-4, 2.1387E-3, 4.5148E-4, INPU1187
1214. * 7.1091E-4, 1.3281E-4, 2.0861E-4, 1.3413E-4, 7.5355E-5, 7.6670E-5, INPU1189
1215. * 7.5222E-4, 4.4717E-4, 1.0863E-3, 2.3058E-4, 7.0445E-4, 5.8077E-5, INPU1189
1216. * 9.4415E-4, 7.7518E-5, 3.0453E-5, 2.7501E-4, 1.2781E-4, 1.0929E-4,
1217. * 1.5268E-4, 6.7172E-6, 2.5615E-5, 2.8001E-5, 6.5923E-5, 6.2719E-6, INPU1192
1218. * 4.1685E-5, 3.8524E-6, 8.0914E-6, 9.4384E-7, 4.0810E-5, 3.6685E-6, INPU1193
1219. * 1.9832E-5, 1.5300E-6, 1.1616E-4, 9.8950E-5, 6.4798E-5, 6.2062E-6, INPU1194
1220. * 5.8266E-5, 5.5773E-6, 9.6150E-5, 8.8091E-6, 3.8821E-4, 1.7961E-4, INPU1195
1221. * 3.4415E-4, 3.0878E-4, 9.7846E-4, 6.8802E-4, 1.3162E-4, 9.4657E-5, INPU1196
1222. * 1.6050E-3, -2.3623E-4, 3.4088E-5, 3.2931E-6, 6.7860E-5, 6.3272E-6, INPU1197
1223. * 1.9485E-4, 1.7666E-4, 1.0877E-5, 1.0434E-4, 1.2265E-4, 9.6225E-5, INPU1198
1224. * 1.3827E-4, 1.2620E-5, 2.8693E-4, 2.5576E-5, 3.0983E-4, 2.5995E-5, INPU1199
1225. * 6.5913E-5, 6.1657E-6, 1.8822E-4, 1.7170E-5, 1.0708E-4, 1.0014E-5, INPU1200
1226. * 2.1969E-4, 8.6130E-5, 3.7019E-4, 3.1900E-5, 2.3841E-4, 2.1384E-5, INPU1201
1227. * 3.8529E-4, 3.4161E-5, 5.4728E-4, 1.7700E-4, 7.8441E-4, 6.2918E-5, INPU1202
1228. * 1.3535E-3, 1.0251E-4, 1.0922E-3, 8.3036E-5, 1.4850E-3, 1.1442E-4, INPU1203
1229. * 2.2724E-3, 1.7133E-4, 2.6030E-3, 1.9311E-4, 3.7280E-4, 1.3944E-4, INPU1204
1230. DATA (BOX(1),I=109,222)/
1231. * 3.6453E-4, 2.9024E-4, 1.6625E-4, 1.0010E-4, 1.4660E-4, 1.6391E-5, INPU1206
1232. * 7.6907E-4, 2.9316E-4, 7.0071E-4, 5.7198E-5, 0.7299E-4, 7.1736E-5, INPU1207
1233. * 5.2082E-4, 4.8174E-5, 6.8102E-4, 8.7245E-5, 2.9162E-3, 2.1768E-4, INPU1208
1234. * 5.1844E-3, 3.9393E-4, 5.7402E-3, 4.6456E-4, 8.5585E-3, 6.9335E-4, INPU1209
1235. * 6.5025E-4, 1.6525E-3, 5.4078E-4, 4.9508E-4, 1.2468E-4, 2.0527E-4, INPU1210
1236. * 1.2237E-4, 1.1101E-5, 7.4204E-5, 6.6708E-6, 1.8597E-4, 8.7495E-5, INPU1211
1237. * 1.9885E-4, 1.7524E-5, 5.8003E-4, 1.7303E-4, 9.8146E-4, 7.2205E-5, INPU1212
1238. * 8.8052E-4, 7.3480E-5, 1.7328E-3, 1.7202E-4, 2.3777E-4, 8.3268E-5, INPU1213
1239. * 4.5384E-4, 4.1206E-6, 3.1763E-4, 2.8757E-5, 9.2717E-4, 8.2272E-5, INPU1214
1240. * 7.5243E-4, 6.8660E-5, 9.5619E-4, 2.5661E-4, 1.1273E-3, 1.0265E-4, INPU1215
1241. * 1.8477E-4, 2.8724E-4, 4.0880E-4, 3.6643E-5, 3.0731E-4, 2.7982E-5, INPU1216
1242. * 7.2948E-4, 3.0807E-4, 3.3204E-4, 2.1001E-5, 1.3028E-4, 1.2769E-5, INPU1217
1243. * 7.1462E-4, 6.5675E-6, 2.0691E-4, 1.8755E-4, 5.1259E-4, 4.0900E-5, INPU1218
1244. * 2.1250E-4, 6.4005E-4, 5.0949E-4, 4.3546E-5, 3.0722E-4, 2.7627E-5, INPU1219
1245. * 4.1370E-4, 3.7228E-5, 1.2231E-3, 1.4108E-4, 1.0262E-3, 8.0162E-5, INPU1220
1246. * 9.7387E-4, 7.5660E-5, 8.9112E-4, 6.8070E-5, 1.1768E-3, 9.1902E-5, INPU1221
1247. * 1.1804E-3, 9.3656E-5, 1.2157E-3, 8.7004E-5, 1.3106E-3, 9.7479E-5, INPU1222
1248. * 8.9487E-4, 1.6437E-4, 1.4627E-4, 1.0672E-4, 1.8070E-3, 1.3783E-4, INPU1223
1249. * 1.6948E-3, 1.2012E-4, 1.4300E-3, 1.4010E-4, 1.7955E-3, 1.3899E-4, INPU1224
1250. DATA (BOX(1),I=223,336)/
1251. * 2.2465E-3, 1.6416E-4, 2.4725E-3, 1.6643E-4, 7.2006E-3, 2.5752E-3, INPU1226

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DATA (PFX(1),I=557,562)/
* 5.0A3F-4, 2.464F-4, 9.592F-4, 3.647F-4, 7.660F-4, 4.5624F-4,
* 5.2A66F-4, 5.771F-4, 9.5056F-4, 7.332F-4, 5.7434F-4, 4.0251F-4,
* 7.3A92F-4, 4.5640F-4,
* 0.0000F+0, 0.0000F+0,
* 4.6546F-4, -1.1031F-4, 9.7467F-4, 1.2402F-4, 0.7132F-4, 4.1360F-4/INPUT244
DATA (PFX(1),I=563,690)/
* 2.4245F-4, 2.4465F-4, 2.4549F-4, 9.2427F-4, 4.1041F-4, 1.2406F-4, INPUT244
* 4.6160F-4, -2.7460F-4, 1.6211F-4, 1.0457F-4, 4.3324F-4, -4.7945F-4, INPUT247
* 8.1342F-4, 1.6317F-4, 2.9332F-4, -1.6090F-4, -1.0744F-4, 1.1715F-4, INPUT248
* 6.7773F-4, 6.7655F-4, 7.2447F-4, 4.1934F-4, 3.0361F-4, INPUT249
* -3.4000F-4, -5.5234F-4, 3.1212F-4, 2.4790F-4, 7.0302F-4, 5.6028F-4, INPUT291
* 5.3363F-4, 2.1469F-4, 5.6164F-4, 1.1441F-4, 2.2394F-4, 1.6019F-4, INPUT291
* 7.8947F-4, -1.2806F-4, 3.7012F-4, 1.4524F-4, 5.3457F-4, 4.2766F-4, INPUT292
* 2.2470F-4, -1.2664F-4, 1.5556F-4, -3.3230F-4, 2.1540F-4, 4.8056F-4, INPUT294
* 2.5913F-4, -1.2664F-4, 5.0024F-4, -2.2434F-4, 4.2970F-4, 2.7940F-4, INPUT294
* 1.0640F-4, -6.0534F-4, 3.5049F-4, 3.6321F-4, 2.9909F-4, -2.2319F-4, INPUT295
* 9.1830F-4, 2.7540F-4, 1.1681F-4, -3.5856F-4, 3.2700F-4, 2.6077F-4, INPUT296
* 7.9007F-4, 2.7075F-4, 6.3162F-4, 3.3419F-4, 7.9272F-4, 6.4265F-4, INPUT297
* 2.6444F-4, 7.5265F-4, 1.6795F-4, 1.6077F-4, 1.4481F-4, 1.4015F-4, INPUT299
* 2.0141F-4, 4.5364F-4, 3.6115F-4, -4.8666F-4, 3.6519F-4, 3.0395F-4, INPUT299
* 3.5052F-4, 1.8624F-4, 7.2511F-4, 9.6566F-4, 3.1135F-4, 4.6023F-4, INPUT300
* 1.7105F-4, -4.8290F-4, 4.1024F-4, -1.8685F-4, 1.2609F-4, -6.0536F-4, INPUT301
* 9.3034F-4, -1.6243F-4, 1.4124F-4, 3.1587F-4, 1.1499F-4, 3.1862F-4, INPUT301
* -4.0594F-4, 9.8653F-4, 8.0419F-4, 1.1652F-4, 7.4406F-4, 1.0431F-4/INPUT303
DATA (PFX(1),I=1,108)/
* 7.5454F+5, -2.3397F+4, 6.1192F+4, -1.4686F+6, -3.0537F+5, -4.8199F+6, INPUT305
* -2.6202F+5, -1.5517F+5, -5.5646F+5, 1.3133F+6, -9.0355F+5, -3.8598F+6, INPUT306
* -1.3620F+5, -9.6431F+5, 2.0080F+4, -2.4202F+4, 2.2087F+9, -7.8207F+6, INPUT307
* 1.8767F+5, 2.4237F+5, -4.4592F+5, -2.7025F+6, -1.1239F+6, -9.2315F+5, INPUT308
* -1.2537F+6, -1.2764F+6, 2.3393F+4, 4.2753F+6, -1.5010F+5, -1.2884F+5,
* 5.5425F+4, 7.4690F+6, -2.5515F+5, -2.2401F+5, -4.8925F+5, -4.0093F+5, INPUT311
* 3.3255F+5, -2.7931F+5, -1.5681F+5, -1.4502F+5, -3.8557F+5, -3.3371F+5, INPUT312
* -2.8367F+5, -2.5430F+5, -1.6192F+5, -2.5325F+5, -4.9024F+5, -3.3371F+5, INPUT312
* 3.6152F+5, -2.7584F+5, -5.9316F+5, -4.7044F+5, -3.0152F+3, -1.7169F+5, INPUT314
* 9.2207F+5, -6.1044F+5, -8.1720F+5, -2.1306F+6, -1.9755F+5, -1.4604F+5, INPUT315
* 4.9078F+4, 5.8440F+5, -6.1080F+5, -5.5656F+5, -3.7134F+5, -2.8505F+5, INPUT316
* 9.4781F+5, -7.0767F+5, 3.9783F+3, 1.5432F+6, -1.7425F+5, -1.3641F+5, INPUT317
* 5.0053F+5, -3.4550F+5, -0.9623F+5, -6.2244F+5, -5.2422F+5, -9.2955F+5, INPUT318
* 3.6464F+5, -2.8292F+5, -7.2949F+5, -5.5544F+5, -6.0255F+5, -6.5705F+5, INPUT319
* 2.8742F+5, -3.3772F+5, -2.4804F+5, -2.44572F+5, -5.8394F+5, -1.5799F+5, INPUT320
* 1.0456F+6, -7.0136F+5, -2.4299F+5, -3.6193F+5, -7.9721F+5, -7.8006F+5, INPUT321
* -1.0900F+6, -2.7675F+6, -7.5323F+5, -1.3506F+6, -1.5903F+6, -2.3962F+6, INPUT322
* -1.2396F+6, -2.4809F+6, -2.0028F+6, -5.0075F+6, -2.6400F+5, -2.1633F+6/INPUT323
DATA (PFX(1),I=109,222)/
* -2.4444F+4, 2.7500F+4, -2.2066F+5, -1.5702F+5, -9.7323F+5, -8.1497F+5, INPUT325
* 3.7939F+4, -4.3404F+6, -9.0272F+5, -7.5324F+5, -1.2447F+5, -1.0443F+6, INPUT327
* -2.4061F+6, -1.7075F+6, -2.9596F+6, -2.0141F+6, -3.7641F+5, -7.8884F+6, INPUT327
* 5.1242F+6, -9.3543F+6, -7.4612F+6, -7.2422F+6, -1.2339F+7, -1.2056F+7, INPUT329
* 2.3222F+4, 1.4011F+7, -6.9566F+5, -4.7298F+5, -1.7104F+5, 1.5106F+6, INPUT329
* 3.9923F+5, -2.7519F+5, -3.2309F+5, -2.3590F+5, -2.6939F+5, -1.5799F+5, INPUT330
* 4.4.9720F+5, -3.3772F+5, -2.4804F+5, -2.44572F+5, -5.8394F+5, -1.5799F+5, INPUT330
* -1.1207F+6, -7.8756F+5, -1.2869F+6, -3.4952F+5, -2.9400F+5, -1.6583F+5, INPUT332
* 4.5954F+5, -4.0189F+5, -1.0619F+6, -7.1104F+5, -2.3217F+6, -1.4800F+6, INPUT333
* -2.9253F+6, -2.0856F+6, -3.7585F+6, -2.6669F+6, -6.6626F+6, -3.3910F+6, INPUT334
* -1.6167F+5, 2.0250F+6, -9.3453F+5, -7.0009F+5, -1.2554F+6, -9.1340F+5, INPUT335
* -4.8370F+4, -5.1415F+5, -7.5237F+5, -5.7552F+5, -8.5223F+5, -6.7942F+5, INPUT336

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53

1440. * 1.4045E+2, 1.4045E+2, 1.9019E+2, 1.9019E+2, 1.0396E+2, 3.1670E+2, 3.1635E+2, INPUT447
 1441. * 4.040E+1, 4.040E+1, 6.1650E+1, 6.1650E+1, 9.2640E+1, 7.1911E+1, 7.1906E+1, INPUT448
 1442. * 9.2640E+1, 9.2640E+1, 9.2640E+1, 9.2640E+1, 9.2640E+1, 6.9403E+1, 6.9403E+1, INPUT449
 1443. * 6.9403E+1, 6.9403E+1, 6.9403E+1, 6.9403E+1, 6.9403E+1, 7.8525E+1, 7.8525E+1, INPUT450
 1444. * 7.8525E+1, 7.8525E+1, 7.8525E+1, 7.8525E+1, 7.8525E+1, 6.6146E+1, 6.6146E+1, INPUT451
 1445. * 6.6146E+1, 6.6146E+1, 6.6146E+1, 6.6146E+1, 6.6146E+1, 1.2472E+2, 1.2472E+2, INPUT452
 1446. * 1.2472E+2, 1.2472E+2, 1.2472E+2, 1.2472E+2, 1.2472E+2, 2.1159E+2, 2.1159E+2, INPUT453
 1447. * 2.1159E+2, 2.1159E+2, 2.1159E+2, 2.1159E+2, 2.1159E+2, 1.2067E+2, 1.2067E+2, INPUT454
 1448. * 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2691E+2, 1.2691E+2, INPUT455
 1449. * 1.2691E+2, 1.2691E+2, 1.2691E+2, 1.2691E+2, 1.2691E+2, 6.3628E+1, 6.3628E+1, INPUT456
 1450. * 6.3628E+1, 6.3628E+1, 6.3628E+1, 6.3628E+1, 6.3628E+1, 1.0309E+2, 1.0309E+2, INPUT457
 1451. * 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.1582E+2, 1.1582E+2, INPUT458
 1452. * 1.1582E+2, 1.1582E+2, 1.1582E+2, 1.1582E+2, 1.1582E+2, 9.4440E+1, 9.4440E+1, INPUT459
 1453. * 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.3005E+1, 9.3005E+1, INPUT460
 1454. * 9.3005E+1, 9.3005E+1, 9.3005E+1, 9.3005E+1, 9.3005E+1, 1.0765E+2, 1.0765E+2, INPUT461
 1455. * 1.0765E+2, 1.0765E+2, 1.0765E+2, 1.0765E+2, 1.0765E+2, 8.4985E+1, 8.4985E+1, INPUT462
 DATA (PFX(1),1=225,336)/
 1456. * 7.9413E+1, 7.9413E+1, 9.7425E+1, 9.7425E+1, 1.6706E+2, 1.6706E+2, 1.6706E+2, INPUT464
 1457. * 1.6706E+2, 1.6706E+2, 1.6706E+2, 1.6706E+2, 1.6706E+2, 8.2762E+1, 8.2762E+1, INPUT465
 1458. * 8.2762E+1, 8.2762E+1, 8.2762E+1, 8.2762E+1, 8.2762E+1, 1.3449E+2, 1.3449E+2, INPUT466
 1459. * 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 9.8562E+1, 9.8562E+1, INPUT467
 1500. * 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3314E+2, 1.3314E+2, INPUT468
 1501. * 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.0691E+2, 1.0691E+2, INPUT469
 1502. * 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.2894E+2, 1.2894E+2, INPUT470
 1503. * 1.2894E+2, 1.2894E+2, 1.2894E+2, 1.2894E+2, 1.2894E+2, 7.1250E+1, 7.1250E+1, INPUT471
 1504. * 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.4094E+1, 7.4094E+1, INPUT472
 1505. * 7.4094E+1, 7.4094E+1, 7.4094E+1, 7.4094E+1, 7.4094E+1, 1.1835E+2, 1.1835E+2, INPUT473
 1506. * 1.1835E+2, 1.1835E+2, 1.1835E+2, 1.1835E+2, 1.1835E+2, 9.8550E+1, 9.8550E+1, INPUT474
 1507. * 9.8550E+1, 9.8550E+1, 9.8550E+1, 9.8550E+1, 9.8550E+1, 1.4921E+2, 1.4921E+2, INPUT475
 1508. * 1.4921E+2, 1.4921E+2, 1.4921E+2, 1.4921E+2, 1.4921E+2, 7.9375E+1, 7.9375E+1, INPUT476
 1509. * 7.9375E+1, 7.9375E+1, 7.9375E+1, 7.9375E+1, 7.9375E+1, 6.4449E+1, 6.4449E+1, INPUT477
 1510. * 6.4449E+1, 6.4449E+1, 6.4449E+1, 6.4449E+1, 6.4449E+1, 1.2133E+2, 1.2133E+2, INPUT478
 1511. * 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.0957E+2, 1.0957E+2, INPUT479
 1512. * 1.0957E+2, 1.0957E+2, 1.0957E+2, 1.0957E+2, 1.0957E+2, 9.1212E+1, 9.1212E+1, INPUT480
 1513. * 9.1212E+1, 9.1212E+1, 9.1212E+1, 9.1212E+1, 9.1212E+1, 1.0334E+2, 1.0334E+2, INPUT481
 1514. * 1.0334E+2, 1.0334E+2, 1.0334E+2, 1.0334E+2, 1.0334E+2, 7.7799E+1, 7.7799E+1, INPUT482
 1515. * 7.7799E+1, 7.7799E+1, 7.7799E+1, 7.7799E+1, 7.7799E+1, 6.5935E+1, 6.5935E+1, INPUT483
 1516. * 6.5935E+1, 6.5935E+1, 6.5935E+1, 6.5935E+1, 6.5935E+1, 9.2543E+1, 9.2543E+1, INPUT484
 1517. * 9.2543E+1, 9.2543E+1, 9.2543E+1, 9.2543E+1, 9.2543E+1, 7.0615E+1, 7.0615E+1, INPUT487
 1518. * 7.0615E+1, 7.0615E+1, 7.0615E+1, 7.0615E+1, 7.0615E+1, 4.4087E+1, 4.4087E+1, INPUT488
 1519. * 4.4087E+1, 4.4087E+1, 4.4087E+1, 4.4087E+1, 4.4087E+1, 7.1948E+1, 7.1948E+1, INPUT489
 1520. * 7.1948E+1, 7.1948E+1, 7.1948E+1, 7.1948E+1, 7.1948E+1, 1.3492E+2, 1.3492E+2, INPUT490
 1521. * 1.3492E+2, 1.3492E+2, 1.3492E+2, 1.3492E+2, 1.3492E+2, 6.9742E+1, 6.9742E+1, INPUT491
 1522. * 6.9742E+1, 6.9742E+1, 6.9742E+1, 6.9742E+1, 6.9742E+1, 5.1990E+1, 5.1990E+1, INPUT492
 1523. * 5.1990E+1, 5.1990E+1, 5.1990E+1, 5.1990E+1, 5.1990E+1, 1.2563E+2, 1.2563E+2, INPUT493
 1524. * 1.2563E+2, 1.2563E+2, 1.2563E+2, 1.2563E+2, 1.2563E+2, 9.2667E+1, 9.2667E+1, INPUT494
 1525. * 9.2667E+1, 9.2667E+1, 9.2667E+1, 9.2667E+1, 9.2667E+1, 1.0154E+2, 1.0154E+2, INPUT495
 1526. * 1.0154E+2, 1.0154E+2, 1.0154E+2, 1.0154E+2, 1.0154E+2, 6.8967E+1, 6.8967E+1, INPUT496
 1527. * 6.8967E+1, 6.8967E+1, 6.8967E+1, 6.8967E+1, 6.8967E+1, 1.1554E+2, 1.1554E+2, INPUT497
 1528. * 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.6604E+2, 1.6604E+2, INPUT498
 1529. * 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.2162E+2, 1.2162E+2, INPUT499
 1530. * 1.2162E+2, 1.2162E+2, 1.2162E+2, 1.2162E+2, 1.2162E+2, 6.9295E+1, 6.9295E+1, INPUT500
 1531. * 6.9295E+1, 6.9295E+1, 6.9295E+1, 6.9295E+1, 6.9295E+1, 1.1087E+2, 1.1087E+2, INPUT501
 1532. * 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.0952E+2, 1.0952E+2, INPUT502
 1533. * 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0551E+2, 1.0551E+2, INPUT503
 1534. * 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, INPUT504
 1535. * 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, 1.0551E+2, INPUT505
 DATA (PFX(1),1=451,556)/


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1702.  NFI=K*NEF
1709.  IF (KR(3) - 5) 90,100,100
1710.  READ (WIN,400) (NFIA(I),EFIR(I),EFFIR(I),J=INF,NEF)
1711.  IF (KR(3) - 3) 10,95,95
1712.  WRITE (JAW) (NFIA(I),EFIR(I),EFFIR(I),J=INF,NEF)
1713.  GO TO 10
1714.  READ (JAW) (NFIA(I),EFIR(I),EFFIR(I),J=INF,NEF)
1715.  GO TO 10
1716.  DO 110 K=1,IS
1717.  C(I)=0.
1718.  DO 130 I=1,7
1719.  IF (JAT(I)) 115,130,115
1720.  DO 120 K=1,IS
1721.  IF (JAT(I) - K) 120,125,120
1722.  COS TIME
1723.  KK=1
1724.  GO TO 255
1725.  C(I)=AIFT(I)
1726.  COS TIME
1727.  WT=0.
1728.  IF (C(I) 140,135,140
1729.  WRITE (KOUT,405) (ALPT(K),JAT(K),K=1,7),SCRF,ANCA,ANOR
1730.  I=1
1731.  LAKK=0
1732.  DO 150 I=1,IS
1733.  IF (C(I)) 145,150,145
1734.  LAKK=LAKK+1
1735.  I=I+1
1736.  AIFT(I)=C(I)
1737.  UT=WT+C(I)*VAT(I)
1738.  IF (J - IS) 160,160,220
1739.  J=J-1
1740.  IF (J) 150,150,165
1741.  DO 185 I=1,JP
1742.  T(I)=T(I)
1743.  U(I)=C(I)
1744.  U(I)=0.
1745.  IF (UG) 170,185,170
1746.  DO 175 I=1,IL
1747.  U(I,U)=U(I,U)-U(I,I)*UGU
1748.  DO 180 I=JPL,JS
1749.  C(I)=C(I)-TAUT(I,L)*UGU
1750.  U(I,U)=0.
1751.  DO 195 I=1,IS
1752.  IF (KRC(C(I)) - .001) 165,195,200
1753.  TAU(I,U)=0.
1754.  GO TO 220
1755.  V(I,U)=1
1756.  U(I,U)=1.
1757.  DO 205 I=1,JD
1758.  U(I,U)=U(I,U)/C(I)
1759.  DO 210 I=1,IS
1760.  TAU(I,U)=C(I)/C(I)
1761.  VC=V(I,U)
1762.  DO 215 I=1,IS
1763.  C(I,U)=AIFT(I)
1764.  KK=J

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INPUT713
INPUT714
INPUT715
INPUT716
INPUT717
INPUT718
INPUT719
INPUT720
INPUT721
INPUT722
INPUT723
INPUT724
INPUT725
INPUT726
INPUT727
INPUT728
INPUT729
INPUT730
INPUT731
INPUT732
INPUT733
INPUT734
INPUT735
INPUT736
INPUT737
INPUT738
INPUT739
INPUT740
INPUT741
INPUT742
INPUT743
INPUT744
INPUT745
INPUT746
INPUT747
INPUT748
INPUT749
INPUT750
INPUT751
INPUT752
INPUT753
INPUT754
INPUT755
INPUT756
INPUT757
INPUT758
INPUT759
INPUT760
INPUT761
INPUT762
INPUT763
INPUT764
INPUT765
INPUT766
INPUT767
INPUT768
INPUT769

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1765.  KKK=J
1766.  J=J+1
1767.  GO TO 255
1768.  CONTINUE
1769.  IF (J - 15) 225,225,200
1770.  DO 250 I=1,N
1771.  V(I,I)=V(I,I)
1772.  DO 235 I=1,15
1773.  V(I,I)=0.
1774.  GO TO 250
1775.  DO 245 I=1,15
1776.  V(I,I)=0.
1777.  DO 245 I=1,15
1778.  V(I,I)=V(I,I)+C(I)*U(I,1)
1779.  V=V
1780.  KKK=I
1781.  IF=1+1
1782.  VC=6.
1783.  IF (KK(3) - 5) 260,290,290
1784.  DO 270 K=1,2
1785.  RA(K)=R(K)
1786.  RA(K)=R(K)+C(K)
1787.  PC(K)=R(K)+C(K)
1788.  PC(K)=R(K)+C(K)
1789.  PC(K)=R(K)+C(K)
1790.  PC(K)=R(K)+C(K)
1791.  PC(K)=R(K)+C(K)
1792.  PC(K)=R(K)+C(K)
1793.  PC(K)=R(K)+C(K)
1794.  GO TO 260
1795.  READ (R,290) (A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1796.  1 A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1797.  IF (KK(3)-3) 295,295,295
1798.  WRITE (J,1) (V(I,I), I=1,15)
1799.  1 A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1800.  GO TO 295
1801.  READ (R,1000) (A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1802.  1 A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1803.  IF (KK - 7) 300,10,300
1804.  IF (KK)=20000.
1805.  IF (KK(1) - 500(2)) 305,310,310
1806.  IF (KK(1) + 400(2) - 5) 310,320,310
1807.  WRITE (L,100,410) A(K),B(K),C(K),D(K),E(K),F(K),G(K),H(K),I(K),J(K),K(K),L(K),M(K),N(K),O(K),P(K),Q(K),R(K),S(K),T(K),U(K),V(K),W(K),X(K),Y(K),Z(K))
1808.  STOP
1809.  IF (KK(1)-1) 310,330,325
1810.  WRITE (J,1)=V(I,I)
1811.  IF (KK)=1,5,10
1812.  IF (KK)=1
1813.  V(K)=0.
1814.  V(K)=V(K)+C(K)
1815.  GO TO 345
1816.  IF (KK)=10,20,30,40,50,60,70,80,90,100,110,120,130,140,150,160,170,180,190,200,210,220,230,240,250,260,270,280,290,300,310,320,330,340,350,360,370,380,390,400,410,420,430,440,450,460,470,480,490,500,510,520,530,540,550,560,570,580,590,600,610,620,630,640,650,660,670,680,690,700,710,720,730,740,750,760,770,780,790,800,810,820,830,840,850,860,870,880,890,900,910,920,930,940,950,960,970,980,990,1000)
1817.  IF (21-5) 335,335,300
1818.  IF (KK)=1,5,10
1819.  IF (KK)=0
1820.  V(K)=V(I,I)
1821.  V(K)=V(I,I)

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1. SUBROUTINE KINET
2. DIMENSION XY(20),PRMU(10,50)
3.
4. REAL NFA(1),NFI(1),NFI(1),TAU(10,10)
5. EQUIVALENCE (NFI(1),A(1)), (NFI(1),A(1)), (NFI(1),A(1)),
6. 1(TAU(1),A(1))
7. DIMENSION TE(10),CIJ(10,1)
8. DIMENSION X(1),VLAM(10,1)
9.
10. COMMON
11. FMOA(10),FAOR(10),RA(10,2),RC(10,2),
12. M(10,2),RE(10,2),RE(10,2),TU(10,2),VN(10),
13. Y(10),WM(10),VM(10,10),FE(10),IFC(10),
14. IP(10),CP(10),H(10),SR(10),TC(10),VLIN(10),
15. E(10),LMT(10),GAMK(1,1)
16.
17. COMMON /PARA1/ KIN,KOUT,JAN,MOL,NAE,TC,H,KXX(3),KR(10),TILE(3),
18. TIMO,TTNAX,VISC,PR(1)
19.
20. COMMON /PARA2/ W,SCH,PHO,VEL,H1,NFF,FF4,TS,ISP,P,T,STP,HIP,
21. EL,ENL,FLIO,M,DEL,ISFG,KVALP,CPE,IRE,IER,BA,ITS,
22. IM,IL,IT,MOFF,HRELT,SEL,T,TRAX,TRIM,MET,SCMB,
23. SUPL,JG,H6,CPG,SWA,SWR,SWC,SWD,SUMC,NXC,SAT,
24. VACH,KR2Z,SP1,GAN,THI,MX,FRCHT,HCH,NCV,TOT,
25. IERZ,FOAT,SP1,IXG,SVI,KKJ,TXC,NXG,SH1,NOATO,
26. SAG,FFFAHS,PV,CNF,VA,HCS,CUMI,CUM2,FP,IFCJC,
27. ISD2,LTG,VF02,VTI
28.
29. COMMON /AGNAYS/ A(16,16),P(16),P(3),XC(50),XG(50),ZKE(10),
30. TLO(10),DRELOC(10),VALJP(10),FIR(10),ALP(10),
31. GAMH(10),GAMF(10),TODIG(3),TK(10,3),WAT(10),
32. IP(10),ICAT(10),KAT(10),UN(10,10),FPL(10)
33.
34. COMMON /KINETX/ MT,EKE(50),EAK(50),EYK(50),PRU(10,50),RPU(10,50),
35. PRP(50),PKK(50)
36.
37. EQUIVALENCE (H(1),X(1)), (GAMK(1),VALJP(1))
38.
39. COMMON /TEEFER/ TE(11),OKPT(50),PKE(50),PKR(50),KAT(50),DUR(50),
40. LL(50),NA(50)
41.
42. COMMON /CCKIN/ PRP(10),ROUCH,ICC
43. COMMON /ZKIN/ PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),
44. *PRX(50),PRX(10,50),PRX(10,50),TUP(50)
45.
46. EQUIVALENCE (PRX(1),X(1))
47.
48. TE(10,1)=1.0
49. TE(10,2)=1.0
50. TE(10,3)=1.0
51. TE(10,4)=1.0
52. TE(10,5)=1.0
53. TE(10,6)=1.0
54. TE(10,7)=1.0
55. TE(10,8)=1.0
56. TE(10,9)=1.0
57. TE(10,10)=1.0
58. TE(10,11)=1.0
59. TE(10,12)=1.0
60. TE(10,13)=1.0
61. TE(10,14)=1.0
62. TE(10,15)=1.0
63. TE(10,16)=1.0
64. TE(10,17)=1.0
65. TE(10,18)=1.0
66. TE(10,19)=1.0
67. TE(10,20)=1.0
68. TE(10,21)=1.0
69. TE(10,22)=1.0
70. TE(10,23)=1.0
71. TE(10,24)=1.0
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697. TE(10,650)=1.0
698. TE(10,651)=1.0
699. TE(10,652)=1.0
700. TE(10,653)=1.0
701. TE(10,654)=1.0
702. TE(10,655)=1.0
703. TE(10,656)=1.0
704. TE(10,657)=1.0
705. TE(10,658)=1.0
706. TE(10,659)=1.0
707. TE(10,660)=1.0
708. TE(10,661)=1.0
709. TE(10,662)=1.0
710. TE(10,663)=1.0
711. TE(10,664)=1.0
712. TE(10,665)=1.0
713. TE(10,666)=1.0
714. TE(10,667)=1.0
715. TE(10,668)=1.0
716. TE(10,669)=1.0
717. TE(10,670)=1.0
718. TE(10,671)=1.0
719. TE(10,672)=1.0
720. TE(10,67
```

```

55.      DO 602 J=1,3
56.      T=PP(J,8)
57.      PDX(M)=PDX(M)+DSI(J,8)*VU(J)
58.      ISI=DSI(1,M)
59.      IS2=DSI(2,M)
60.      IF (ISI.GT.0) FKS(M)=FKS(1,M)*VU(152)
61.      IF (IS2.GT.0) FKS(M)=FKS(2,M)*VU(152)
62.      FKS(M)=1.0+FKS(M)
63.      PDX(M)=1.0+PDX(M)
64.      FAF(M)=XX(M)/PDX(M)*FKS(M)
65.      GO TO 603
66.      T1=VU(1,M)
67.      T11=VU(1,M)
68.      PFX(M)=1.0
69.      FKS(M)=1.0
70.      FAK(M)=FPM(1,M)*H(11)-PMU(1,M)*H(111)
71.      FKF(M)=XX(M)/SQRT(FMU(1,M))*35.167*EXP((PAB(1,M)*SR(11)-KAB(1,M))*
72.      1SR(11))/1.9869)
73.      603 CONTINUE
74.      GO TO 10
75.      334 TFKR(9),FK(3) GO TO 801
76.      KR(9)=3
77.      DO 802 M=1,MT
78.      XKR(M)=FKR(M)
79.      801 DO 800 M=1,MT
80.      TFKR(M),FK(1) GO TO 800
81.      PDX(M)=PDX(1,M)
82.      GO TO 800
83.      PDX(M)=0.0
84.      GO 803 J=2,3
85.      T=PP(J,8)
86.      T1=PP(J,8)
87.      PDX(M)=PDX(M)+DSI(J,8)*VU(J) +KK(J,8)*VU(11)
88.      T1=PP(1,M)
89.      T=PP(1,M)
90.      PDX(M)=VU(11)+PDX(M)+FKX(1,M)*VU(1)
91.      FKF(M)=XX(M)+PDX(M)
92.      TFKR(9),FK(3) GO TO 10
93.      DO 11 M=1,MT
94.      11 PDX(M)=1.0
95.      10 RT=1.9869 * T
96.      DO 40 M=1,MT
97.      SUMC=0.
98.      SUMK=0.
99.      SUMW=0.
100.      SUMP=0.
101.      DO 15 IZ=1,4
102.      TFKR(SRMM(IZ,9)),I,1,M=-6) GO TO 17
103.      T=PP(IZ,3)
104.      TFKR(11),FK(1),FK(1),FK(1),FK(1) GO TO 14
105.      TFKR(11),FK(1),FK(1),FK(1),FK(1) GO TO 14
106.      VU2=0.0
107.      VU1=0.0
108.      GO TO 35
109.      14 SUMC=SUMC+PDX(IZ,3)*VU(I)
110.      15 SUMI=H(11)/MT+SUMC(1)/1.0069
111.      SUMK=SUMK
      -KMU(17,M)*VU(17)

```

KINE.6330
KINE.6340
KINE.6350
KINE.6360
KINE.6370
KINE.6380

63


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226.  PRAD(J,N) = LUP1
227.  C*****ADN CONTROLLING REACTION 1 TO ITS MASS BALANCE
228.  I1 = 1
229.  I2 = 1
230.  170 DO 175 J=1,15
231.  SUM=0.0
232.  DO 500 JJ=1,N
233.  I=PPF(JJ,N)
234.  V=VPE=VNU(I,J)
235.  I=PRP(JJ,N).61,15) GO TO 502
236.  V=VPP=0.
237.  IF(NPP(JJ,N).EQ.0) V=VPP=1.0
238.  I1 =NPF(JJ,N)
239.  V=VPE=VNU(I1,J)
240.  IF(NPF(JJ,N).GT.15) GO TO 503
241.  V=VPE=0.
242.  IF(NPF(JJ,N).EQ.0) V=VPE=1.0
243.  SUM=SUM+PRP(I1)*V
244.  100 I11 = PPR(JJ,N)/PRKS(N)*V=VPE
245.  GO CONTINUE
246.  DO 501 I2=1,4
247.  I12=PP(I2,N)
248.  V=VPP=VNU(I11,I2)
249.  I=CNK(I2,N).61,15) GO TO 504
250.  V=VKK=0.0
251.  IF(NPR(I2,N).EQ.0) J=V=VPP=1.0
252.  I12=NP(I2,N)
253.  V=VPP=VNU(I1,I2)
254.  IF(NPR(I2,N).GT.15) GO TO 505
255.  V=VPP=0.0
256.  IF(NPR(I2,N).EQ.0) V=VPP=1.0
257.  SUM=SUM+PRP(I2)*V=VPP=PRP(I2)*V=VPP=PRP(N)*V=VPP
258.  GO CONTINUE
259.  175 I11,I12 = N(I + 2,J + 2) = N(I + 2,J + 2) - SUM + PRP(I1,I2)
260.  SUM=0.0
261.  SUM=0.0
262.  DO 506 JJ=1,N
263.  PRP=0.0
264.  I12=PP(I2,N)
265.  IF(NPP(JJ,N).GT.15)
266.  *PRP=PRP(I1)*V=V(I1)
267.  SUM=SUM+PRP(I2)*V=V(I1)
268.  SUM=SUM+PRP(I2)*V=V(I1)
269.  SUM=SUM+PRP(I2)*V=V(I1)
270.  PRP=0.0
271.  I1=PP(JJ,N)
272.  IF(NPP(JJ,N).GT.15)
273.  *PRP=PRP(I1)*V=V(I1)
274.  SUM=SUM+PRP(I2)*V=V(I1)
275.  SUM=SUM+PRP(I2)*V=V(I1)
276.  DO 507 I2=1,4
277.  PRP=0.0
278.  I12=PP(I2,N).GT.15)
279.  *PRP=PRP(I2)*V=V(I1)
280.  I12=PP(I2,N)
281.  SUM=SUM+PRP(I2)*V=V(I1)
282.  SUM=SUM+PRP(I2)*V=V(I1)

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KINE1400
 KINE1410
 KINE1420
 KINE1430
 KINE1440

KINE1460
 KINE1470

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282.      NCF=0.0
283.      IF (I-12).GT.151
284.      *NCF=NCF+(1./N)*P0.0(N)
285.      T1=EMP(I2,N)
286.      T2=EMP(I2,N)
287.      SUFF=SUMF-EMP(I2,N)
288.      SUFF=SUMF-EMP(I2,N)
289.      SUFF=SUMF-EMP(I2,N)
290.      DO 140 I=1,I2
291.      U=1+P0.0(I)+P0.0(I,N)
292.      T1+2.0)=A(I+2.0)-U
293.      A(I+2.0)=A(I+2.0)+SUFF*P0.0(I,N)
294.      F(I)=F(I)+U
295.      U(I+2)=U(I+2)+U-5.0*F*P0.0(I,N)
296.      IF (I-17).GT.1) DO 200,140
297.      140 WRITE (NOUT,215)
298.      140 WRITE (NOUT,215)
299.      140 WRITE (NOUT,215)
300.      140 WRITE (NOUT,215)
301.      140 WRITE (NOUT,215)
302.      140 WRITE (NOUT,215)
303.      140 WRITE (NOUT,215)
304.      140 WRITE (NOUT,215)
305.      140 WRITE (NOUT,215)
306.      140 WRITE (NOUT,215)
307.      140 WRITE (NOUT,215)
308.      140 WRITE (NOUT,215)
309.      140 WRITE (NOUT,215)
310.      140 WRITE (NOUT,215)
311.      140 WRITE (NOUT,215)
312.      140 WRITE (NOUT,215)
313.      140 WRITE (NOUT,215)
314.      140 WRITE (NOUT,215)
315.      140 WRITE (NOUT,215)
316.      140 WRITE (NOUT,215)
317.      140 WRITE (NOUT,215)
318.      140 WRITE (NOUT,215)
319.      140 WRITE (NOUT,215)
320.      140 WRITE (NOUT,215)
321.      140 WRITE (NOUT,215)
322.      140 WRITE (NOUT,215)
323.      140 WRITE (NOUT,215)
324.      140 WRITE (NOUT,215)
325.      140 WRITE (NOUT,215)
326.      140 WRITE (NOUT,215)
327.      140 WRITE (NOUT,215)
328.      140 WRITE (NOUT,215)
329.      140 WRITE (NOUT,215)
330.      140 WRITE (NOUT,215)
331.      140 WRITE (NOUT,215)
332.      140 WRITE (NOUT,215)

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112.  H1=HL+VM*(C*(T)+FLIC+VVELT
113.  SL=SL+VM*(C*FLT)+FLIC+VVELT
114.  H1P=(H1+H1C)/AA
115.  STP=(SL+SLC)/AA
116.  H1=K*(1)-TFR2+KRF
117.  FAFSGA=EX
118.  IF (KR(4)) 60,50,55
119.  HTL=H1C/AA
120.  FAF=0.
121.  WSG=APAX1*(WS-W(3)+PPON,1,F-30)
122.  H1P=(H1C*(H1-VTH+H1C)/WSD)/AA
123.  STP=0.
124.  H1C=H1C*(1+1.5146)
125.  H1C=H1C*(1+1.5146)
126.  H1C=H1C*(1+1.5146)
127.  H1=H1C/WT*1.8
128.  SL=SL/WT
129.  SG=SG/WT
130.  H1C=H1C*1.8
131.  WSG=WTG/P
132.  W1=WTL/SP
133.  IF (KR(6)) 65,70,70
134.  WRITE (KOUT,355) WTR
135.  WRITE (KOUT,360) T1,T,P
136.  GO TO 100
137.  WRITE (KOUT,435)
138.  NSPIE = KKK(4)
139.  WRITE (KOUT,415) (SPIE(NSPIE,I),I=1,9)
140.  WRITE (KOUT,430) HOUCE
141.  WRITE (KOUT,410) RV,PPRF
142.  WRITE (KOUT,440) T1,T,P
143.  WRITE (KOUT,365) H1C,H1C,PPRF,RHO,WMG,WMU,WM
144.  IF (KKJ) 105,110,110
145.  VELSQ=(SVI*SI(SAI))*2.+(SVI/RHO)*SVI*Cos(SAI)
146.  1*2.1/45054.
147.  SA2=(ATAN(RHO/SVI*TAH(SAI)))*57.29577
148.  SVI=SAI*57.29577
149.  SHI=SHI*1.8
150.  SOMAK=VELSQ/GAM*WM/(1.9469*T)
151.  VMACH=ASQRT(SOMAK)
152.  VEL=ASQRT(VELSQ*45054.)
153.  FLUX=VEL*FV
154.  WRITE (KOUT,380) VEL,VMACH,SA2
155.  H1C=H1C*1.8
156.  WRITE (KOUT,385) SVI,SHI,PPRF,SVI,SVI,SVI
157.  SHI=SHI*1.8
158.  GO TO 140
159.  IF (KR(5)-1) 115,130,125
160.  IF (KR(5)) 120,140,140
161.  WRITE (KOUT,395)
162.  H1C=H1C*1.8
163.  SVI=SAI*57.29577
164.  SHI=SHI*1.8
165.  WRITE (KOUT,400) SVI,SVI,PPRF,SVI,SVI,SVI
166.  GO TO 140
167.  H1C=H1P
168.  SCH=SP

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***7

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[illegible]

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226.      WRITE (KOUT,460) (I,PERIL(I),I=1,N)
227.      WRITE (KOUT,462) (I,PKKK(I),I=1,NT)
228.      462 FORMAT(6HP RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PPG
229.      462
230.      205 IF (KR(1)) 215,220,210
231.      210 WRITE (KOUT,450)
232.      60 TO 240
233.      215 IF (KR(5)) 230,220,220
234.      220 IF (KR(4)) 235,225,235
235.      225 WRITE (KOUT,370)
236.      60 TO 240
237.      230 WRITE (KOUT,405)
238.      60 TO 240
239.      235 WRITE (KOUT,390)
240.      60 TO 255 I=1,N
241.      IF (IFC(I)-1) 255,245,255
242.      245 IF (KR(6)) 255,250,250
243.      250 V(I)=UN(I)/QK(I)*I
244.      255 V(I)=V(I)/P
245.      IF (ICV) 260,260,260
246.      260 IF (KR(7)-1) 265,265,260
247.      265 IF (I-E0) 270,270,275
248.      270 WRITE (KOUT,505) (FAMCA(I),FAMOB(I),V(I),I=1,N)
249.      60 TO 265
250.      275 WRITE (KOUT,510) (FAMCA(I),FAMOB(I),V(I),I=1,N)
251.      60 TO 265
252.      240 WRITE (KOUT,465) (FAMCA(I),FAMOB(I),V(I),IC(I),Y(I),VLPK(I),IFC(I),OUTP235
253.      1),F(I),CE(I),I=1,N)
254.      285 10 300 I=1,N
255.      IF (IFC(I)-1) 300,290,300
256.      290 IF (KR(6)) 300,295,295
257.      295 V(I)=V(I)/V(I)*W
258.      300 V(I)=V(I)*P
259.      305 IF (FL(I)) 315,315,310
260.      FSOL=1.-FI/I
261.      310 WRITE (KOUT,455) FAMOB(FI),FAMOB(CU(I)),FLIO,FSOL
262.      315 IF (ITS) 320,345,345
263.      320 IF (KR(5)) 325,340,325
264.      325 IF (KR(4)*P(5)) 335,335,335
265.      330 K(I)=1
266.      K(I)=4
267.      K(I)=7
268.      K(2)=1
269.      K(5)=3
270.      ACUS=0.
271.      ITS=0
272.      GASE=GAZ/(CAP - 1.)
273.      C TEST CURVES OF STAGNATION PRESSURE PERFORM SUCCESS
274.      271 0. + ( (GAS - 1.) / 2.) * (SOURK) * * GASE)*P
275.      CALL ETIE
276.      XDESLP
277.      RETURN
278.      345
279.      345
280.      280.
281.      C
282.      350 FORMAT (13HP SOLUTION TYPES,10X,13HP ITERATIONS = ,14,23,7HP I=IF = OUTP265

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**-3

[illegible]


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55. DATA (PRSP(1,1),I=1,4)/4HC0, 4HH2, 4H, 4P /,(PRSP(2,1),I=1
56. *,4)/4HC0, 4H, 4H, 4H /,(PRSP(3,1),I=1,4)/4HC2,4H, 4H
57. *,4H /,(PRSP(4,1),I=1,4)/4HC, 4H, 4H, 4H /,(PRSP
58. *(5,1),I=1,4)/4HC2, 4H, 4H, 4H /,(PRSP(6,1),I=1,4)/4HC3
59. *,4H, 4H, 4H /,(PRSP(7,1),I=1,4)/4HC4, 4H, 4H, 4H
60. *,4H, 4H, 4H /,(PRSP(8,1),I=1,4)/4HC5, 4H, 4H, 4H
61. DATA (TINP(1,1),I=1,8)/4HH20, 4HC02, 4HHC, 4HCLH, 4HFFH, 4H
62. *,4H /
63. DATA (POIS(1,1),I=1,8)/4HCLH, 4HFFH, 4H, 4H, 4H, 4H, 4H
64. *,4H /
65. DATA (FSS(1,1),I=1,5)/,125.,.261.,.012.,.130.,.00956/
66. DATA (FKFN(1,1),I=1,3)/12.5,12.5,0.771/(FKFN(1,1),I=1,3)/4.6F+4.
67. *,4.6F+4.5,4.55E+4/(FKFN(1,1),I=1,3)/0.0,0.0,0.0/(FKFN(1,2),I=1,3)/
68. *,2.63724E+3,3.434485E+6,5.136124E+5/(FKFN(1,2),I=1,3)/61910.5,
69. *,69431.3,124440.0/(FKFN(1,2),I=1,3)/0.0,0.0,0.0/(FKFN(1,3),I
70. *,1,3)/1.90F+5,1.90F+5,4.94F+7/(FKFN(1,3),I=1,3)/6.55E+4,6.55F+4,
71. *,1.295E+5/(FKFN(1,3),I=1,3)/0.0,0.0,0.0/(FKFN(1,4),I=1,3)/.0346A,
72. *,.0015,1.9133/(FKFN(1,4),I=1,3)/4.175,34.4175,34.57175,44/(FKFN(1,
73. *,4),I=1,3)/-.29, -.29,0.0/(FKFN(1,5),I=1,3)/.74,3.493,19610.44/(FA
74. *,K0(1,5),I=1,3)/451.4,451.4,110500.0/(FKFN(1,5),I=1,3)/0.0,0.0,0
75. *,0/(FKFN(1,6),I=1,3)/.478,14.4776, .017/(FKFN(1,6),I=1,3)/34308.2
76. *,.34308,2.34883,6/(FKFN(1,6),I=1,3)/.617, .617,0.0/(FKFN(1,7),I=1,
77. *,31/6.89046F+5,1.31779E+7,4.41603E+4/(FKFN(1,7),I=1,3)/101676.95,1
78. *,01676.95,117282.75/(FKFN(1,7),I=1,3)/.483, .833,0.0/
79. DATA (FKFN(1,8),I=1,3)/11.0901,208.87,0.70045/(FKFN(1,8),I=1,3)/
80. *,29386.7,29346.7,50640.4/(FKFN(1,8),I=1,3)/0.0,0.0,0.0/
81. DATA (PSID(1,1),I=1,8)/1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0/(PSID(1,
82. *,2,1),I=1,8)/1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0/(PSID(1,3),I=1,8)/
83. *,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0/(PSID(1,2),I=1,8)/151.32,26.05,
84. *,216.0,0.93,1145.0,0.0,0.0/(PSID(1,2,2),I=1,8)/46.75,166.49,
85. *,29.87,0.0,1325.44,0.0,0.0,0.0/(PSID(1,3,2),I=1,8)/0.0,0.0,0.55A,
86. *,0.0,0.0,53.355,0.0,0.0/(PSID(1,1,3),I=1,8)/1.0,1.0,1.0,1.0,1.0,1.0,
87. *,0.0,0.0,0.0/(PSID(1,2,3),I=1,8)/1.0,1.0,1.0,1.0,1.0,1.0,0.0,0.0/
88. DATA (PSID(1,3,3),I=1,6)/1.0,1.0,1.0,1.0,1.0,1.0/(PSID(1,3,3),I=1,6)/
89. *,SID(1,2,4),I=1,8)/,0331.,.064.,.021.,.0058,1.0,0.0,0.0,0.0/(PSID(1,5),I=1
90. *,4),I=1,8)/.0058, .0058,0.0,0.0,0.0,0.0,0.0,0.0/(PSID(1,2,5),I=1,8)
91. *,8)/163.87,399.3,166.5,13.12,100.0,0.0,0.0,0.0/(PSID(1,3,5),I=1,8)/0.
92. *,163.87,399.3,166.5,13.12,100.0,0.0,0.0,0.0/(PSID(1,1,5),I=1,8)/0.
93. *,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0/(PSID(1,1,6),I=1,8)/16.61,42.25,75
94. *,69,21.8, .1,0.0,0.0,0.0,0.0/(PSID(1,2,6),I=1,8)/16.61,42.25,75,69,21
95. *,8, .1,0.0,0.0,0.0,0.0/(PSID(1,3,6),I=1,8)/0.0,0.0,0.0,0.0,0.0,0.0,0
96. *,0.0,0.0,0.0,0.0,0.0/(PSID(1,1,7),I=1,8)/252.67,5018.31,.054, .0001,0.0,0.0,0.0,0
97. *,0/(PSID(1,2,7),I=1,8)/252.67,5018.31,.054, .0001,0.0,0.0,0.0,0.0/
98. DATA (PSID(1,3,7),I=1,8)/53.68,118.786, .059,0.0,0.0,0.0,0.0,0.0/
99. *,SID(1,3,7),I=1,8)/29.41,373.68,0.0,1.72, .01,2500,0.0,0.0,0.0/
100. DATA (PSID(1,1,8),I=1,8)/29.41,373.68,0.0,1.72, .01,2500,0.0,0.0,0.0/
101. *,(PSID(1,2,8),I=1,8)/88.38,20.19,13.69,0.0,0.0,0.0,0.0,0.0/
102. *,(PSID(1,3,8),I=1,8)/3.0,3.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,
103. DATA (FKKN(1,1),I=1,8)/3.0,3.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,3),I=1,8)/
104. *,2,1),I=1,8)/3.0,3.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,1,3),I=1,8)/
105. *,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,2),I=1,8)/0.0,0.0,0.0,0.0,0
106. *,0.0,0.0,0.0,0.0,0.0/(FKKN(1,2,2),I=1,8)/0.0,0.0,0.0,0.0,0.0,0.0,0
107. *,0.0,0.0,0.0,0.0/(FKKN(1,3,2),I=1,8)/0.0,0.0,0.0,0.0,0.0,0.0,0.0,0
108. *,(FKKN(1,1,3),I=1,8)/3.0,3.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,2,3),
109. *,I=1,8)/3.0,3.0,0.0,0.0,0.0,0.0,0.0,0.0/(FKKN(1,3,3),I=1,8)/0.0,
110. *,0.0,0.0,0.0,0.0,0.0,0.0,0.0/
111. DATA BLK/4H

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112. 5      MOVE=MM(1)
113.      IF (ITS) 50,10,50
114.      *16=0.
115.      *11=0.
116.      IF (K(R)) 40,40,15
117.      IF (IFC(N+1)-1) 25,20,25
118.      IF (1+.001-IF(N+1)) 25,25,30
119.      IFC(N+1)=-1
120.      VM(N+1)=0.
121.      DO 35 K=1,TS
122.      VM(N+1,K)=-TC(K,3)
123.      *11=-VM(N+1)
124.      SUM2=0.
125.      SUMN=0.
126.      DO 45 J=1,15
127.      PROS(T)=0.
128.      SLAR(T)=0.
129.      *FILT=0.
130.      FLIQ=0.
131.      *FILT=0.
132.      MELT=1
133.      TTIME=TIME
134.      *MAX=TIME
135.      *MAX=500.
136.      VA=ALOC(T / 3000.)
137.      *V=1-3000.
138.      VC=(T + 3000.)/2.
139.      *V=1-3000.
140.      *V=VC/100 * V(1)
141.      RT=1.5869*T
142.      IF (RCV) 65,65,55
143.      PIN=PA*10.*r-3
144.      *R=20.
145.      AA=PA*V
146.      IF (MOE) 65,65,60
147.      T=3000.
148.      CONTINUE
149.      I=1
150.      DO 255 IK=1,N
151.      J=2
152.      IF (RCV) 40,40,70
153.      IF (IFC(1)) 80,75,40
154.      *V(I)=VM(I)*PI
155.      Y(I)=ALOC(V(I))
156.      CONTINUE
157.      IF (IFC(1) + 1) 165,85,85
158.      IF (IFC(1)) 40,95,140
159.      IF (MOE - 1) 165,150,165
160.      IF (ITS) 165,160,165
161.      SUMN=SUMN+VM(I)
162.      *V=1-5*TR(I)*V(I)
163.      *V=1-5*V(I)*V(I)
164.      *V=2-2*V(I)*V(I)+V(I)*V(I)
165.      IF (IK - TS) 105,105,115
166.      *V(I)=V(I)
167.      IF (K(R)) 165,110,130
168.      SLAR(T)=V(I)/PI(T)

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165. GO TO 185
170. 36 125 K=1,IS
171. 6001=9001,60)*A(1)
172. IF (K=6) 125,120,125
173. 300(K)=S(A*(K)+0.01/EF(1)
174. 6005(6)=9005(6)+0.001
175. IF (K=6) 165,165,136
176. 30 125 K=1,IS
177. 300(K)=S(A*(K)+0.01/EF(1)
178. IF (K=6) 125,120,125
179. 6005(6)=9005(6)+0.001
180. IF (K=6) 165,165,136
181. IF (K=6) 125,120,125
182. IF (K=6) 165,165,136
183. IF (K=6) 125,120,125
184. IF (K=6) 165,165,136
185. IF (K=6) 125,120,125
186. IF (K=6) 165,165,136
187. IF (K=6) 125,120,125
188. IF (K=6) 165,165,136
189. IF (K=6) 125,120,125
190. IF (K=6) 165,165,136
191. IF (K=6) 125,120,125
192. IF (K=6) 165,165,136
193. IF (K=6) 125,120,125
194. IF (K=6) 165,165,136
195. IF (K=6) 125,120,125
196. IF (K=6) 165,165,136
197. IF (K=6) 125,120,125
198. IF (K=6) 165,165,136
199. IF (K=6) 125,120,125
200. IF (K=6) 165,165,136
201. IF (K=6) 125,120,125
202. IF (K=6) 165,165,136
203. IF (K=6) 125,120,125
204. IF (K=6) 165,165,136
205. IF (K=6) 125,120,125
206. IF (K=6) 165,165,136
207. IF (K=6) 125,120,125
208. IF (K=6) 165,165,136
209. IF (K=6) 125,120,125
210. IF (K=6) 165,165,136
211. IF (K=6) 125,120,125
212. IF (K=6) 165,165,136
213. IF (K=6) 125,120,125
214. IF (K=6) 165,165,136
215. IF (K=6) 125,120,125
216. IF (K=6) 165,165,136
217. IF (K=6) 125,120,125
218. IF (K=6) 165,165,136
219. IF (K=6) 125,120,125
220. IF (K=6) 165,165,136
221. IF (K=6) 125,120,125
222. IF (K=6) 165,165,136
223. IF (K=6) 125,120,125
224. IF (K=6) 165,165,136
225. IF (K=6) 125,120,125

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226. 315 AZ=P*1"
227. HCV=0
228. SURC=ROUC*
229. TAF=0
230. NUT=0
231. MS = 5
232. IF (KRR(9)-5) 335,411,411
233. 411 DO 607 N=1,A
234. DO 608 IZ=1,4
235. 608 IZ,M)=0.0
236. 408 IZ,M)=6.0
237. NRR(IZ,M)=1
238. 603 NRR(IZ,M)=1
239. DO 607 IZ=1,4
240. NPP(IZ,M)=1
241. PSI(IZ,M)=0.0
242. FKR(IZ,M)=0.0
243. FNAK(1,IZ,M)=RLK
244. FNAK(1,IZ,M)=1
245. 607 NPF(IZ,M)=1
246. 603 FOPFAT(IX,2A4,32H)SPECIES NOT FOUND IN THERMO DATA)
247. IF (KRR(81-4) 413,414,414
248. 414 IJ=1
249. MR=3
250. IRY=1
251. C*****H2O+C==CO+H2*****
252. RMU(1,IJ)=1.0
253. KRU(2,IJ)=1.0
254. PFI(1,IJ)=1.0
255. PMU(2,IJ)=1.0
256. IJ=2
257. GO TO 421
258. 413 IF (KPK(81-2) 416,415,416
259. 415 IJ=1
260. MP=3
261. IPX=2
262. C*****CO2+C==2CO*****
263. 421 RMU(1,IJ)=1.0
264. RMU(2,IJ)=1.0
265. PMU(1,IJ)=2.0
266. IF (MR .EQ. 1) GO TO 417
267. IJ=3
268. GO TO 422
269. 416 IJ=1
270. MR=1
271. IPX=3
272. C*****H2+2C==C2H2*****
273. 422 RMU(1,IJ)=1.0
274. RMU(2,IJ)=2.0
275. PMU(1,IJ)=1.0
276. 417 DO 418 I=1,MS
277. SURC=FLOAT(I)
278. RMU(1,I+MR)=SUFC
279. 418 PMU(1,I+MR)=1.0
280. MT=MR+MS
281. NICK=KRR(4)
282. IF (KRR(71) 701,702,701

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THERMO16R

[illegible]


```

1. SURROUTINE KININ
2. DIMENSION KRA(10,33),WRA(3,33),7A(33),PRA(33),TFA(3),TS(15)
3.
4. C
5. REAL A(1),ME(1),FFIN(1),TAU(10,10)
6. EQUIVALENCE (TFA(1),A(1)), (ME(1),A(51)), (FFIN(1),A(101)),
7. 1(TAU(1),A(151))
8. DIMENSION TE(100),CIJ(100,3)
9. DIMENSION X(1),VLAM(100,1)
10.
11. C
12. COMMON
13. 1 FADQA(100),FANDR(100),RA(100,2),RC(100,2),
14. 2 RC(100,2),PE(100,2),FF(100,2),TU(100,2),VF(100),
15. 3 Y(100),WTN(100),VNU(100,10),EF(100),IFC(100),
16. 4 IP(100),CP(100),H(100),SK(100),TC(100),VLWK(100),
17. 5 E(100),LAMI(100),GARK(1,1)
18.
19. C
20. COMMON /PARAM1/ KIN,KOUT,JGR,FOL,PAR,IOC,M,KFX(3),PR(10),TILE(3),
21. 1 TMIN,TMAX,VISC,PR(1)
22.
23. C
24. COMMON /PARAM2/ WM,SCH,RHO,VEL,N1,FF,FFA,TS,ISP,P,T,SIP,HJP,
25. 1 FL,EMI,FLIO,NQ,IFL,ISQ,KPALP,CPF,INF,TF,AA,TTS,
26. 2 IN,IL,IT,MCEE,HMELT,SELT,TMAX,TMIN,MELT,SUMN,
27. 3 SUP,LJC,HG,CPG,SVA,SVH,SVC,SVD,SUMC,NXC,SAI,
28. 4 VMACH,KRZ,SPJ,GAM,THI,MX,DACHI,HCH,NCV,TBT,
29. 5 IFRZ,FOAT,SP1,IXG,SVI,KKJ,IXC,IXG,SM1,NOATO,
30. 6 SAP,FEFF,WS,RV,CDF,VA,HOS,RUP,1,DUM2,EP,IFCJC,
31. 7 ISP2,ATG,VNU2,WL
32.
33. C
34. COMMON /ARRAYS/ # (16,16),B(16),N(3),XC(50),XG(50),ZKE(10),
35. 1 YLO(10),CMCLO(10),WALJP(10),EB(10),ALP(10),
36. 2 GAM,H(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
37. 3 IR(10),IOAT(10),KAT(10),UN(10,10),EPL(10)
38. EQUIVALENCE (TU(101),TF(1)), (VNU(1),CIJ(1))
39.
40. C
41. COMMON /KINETX/ NT,PKF(50),EAK(50),FKK(50),PMU(10,50),PMU(10,50),
42. 1 PMR(50),PKKK(50)
43.
44. C
45. EQUIVALENCE (B(1),X(1)), (GARK(1),VLAM(1))
46.
47. C
48. COMMON/CAPKIN/ KKK(10),ROUCH,NCC
49. COMMON/CONCRD/ Z,GARF,VR(3)
50. COMMON/STCPG/ PERCT,STPFR,CPEF
51. DATA (TFA(1),I=1, 8)/500.,1000.,1500.,2000.,2500.,3000.,3500.,
52. 14000./
53. DATA (TSA(1),I=1,15)/1200.,1400.,1600.,1800.,2000.,2200.,2400.,
54. 12600.,2600.,3000.,3200.,3400.,3600.,3800.,4000./
55. DATA KTF,KTS/R,15/
56. NCC=NCC+1
57.
58. 5 IF (NCC-1) 315,10,315
59.
60. 10 HEAD (KIN,360) KKK(2,PR,ZE,PC,POUCH,GARF,TILE
61. IF (KKK(1)-8) 20,15,20
62.
63. 15 KR(1)=8
64. GO TO 355
65.
66. 20 IF (KKK(4) .LT. 8) GO TO 33
67. READ(KIN,32) PERCT

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*COR
*COR
*COR
*--1

*COR
*-12

55. 32 FOR CAT(510,0)
56. STPR=700000000
57. CPER=1.-STPR
58. IF (KPK(5)-2) 40,25,40
59. KTF=0
60. KTF=KTF+1
61. KTF=KTF+1
62. IF (KPK(5)-2) 50,55,30
63. KTF=KTF+1
64. IF (KPK(5)-2) 60,45,60
65. KTS=0
66. KTS=KTS+1
67. KTS=KTS+1
68. IF (KPK(5)-2) 50,55,50
69. KTS=KTS+1
70. KTS=KTS+1
71. KTS=KTS+1
72. KTS=KTS+1
73. KTS=KTS+1
74. KTS=KTS+1
75. KTS=KTS+1
76. KTS=KTS+1
77. KTS=KTS+1
78. KTS=KTS+1
79. KTS=KTS+1
80. KTS=KTS+1
81. KTS=KTS+1
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92. KTS=KTS+1
93. KTS=KTS+1
94. KTS=KTS+1
95. KTS=KTS+1
96. KTS=KTS+1
97. KTS=KTS+1
98. KTS=KTS+1
99. KTS=KTS+1
100. KTS=KTS+1
101. KTS=KTS+1
102. KTS=KTS+1
103. KTS=KTS+1
104. KTS=KTS+1
105. KTS=KTS+1
106. KTS=KTS+1
107. KTS=KTS+1
108. KTS=KTS+1
109. KTS=KTS+1
110. KTS=KTS+1
111. KTS=KTS+1

112.	140	IF (KRR(1)-2) 145,145,170	KINI0117	*COR
113.	145	KRA(5,1)=0	KINI0118	*-12
114.		KRA(1,2)=0	KINI0119	
115.		KRA(2,2)=0	KINI0120	
116.		KRA(3,2)=0	KINI0121	
117.		KRA(4,2)=0	KINI0122	
118.		KRA(5,2)=0	KINI0123	
119.		KRA(9,2)=0	KINI0124	
120.		ZA(2)=0.0	KINI0125	
121.		KRA(2)=0.0	KINI0126	
122.		IF (KRR(1)-2) 155,150,155	KINI0127	
123.	150	KRA(5,2)=5	KINI0128	
124.	155	ICT=2		
125.		GO TO 215	KINI0141	
126.	170	IF (KRR(1)-3) 150,175,190	KINI0142	
127.	175	KRA(5,1)=2	KINI0143	
128.		KRA(1,2)=3	KINI0144	
129.		KRA(2,2)=0	KINI0145	
130.		KRA(3,2)=0	KINI0146	
131.		KRA(4,2)=0	KINI0147	
132.		KRA(5,2)=1	KINI0148	
133.		KRA(9,2)=0	KINI0149	
134.		ZA(2)=0.0	KINI0150	
135.		KRA(2)=2E	KINI0151	
136.		ICT=2		
137.		GO TO 215	KINI0164	*COR
138.	190	KRA(5,1)=2	KINI0165	*-12
139.		KRA(1,2)=3	KINI0166	
140.		KRA(2,2)=0	KINI0167	
141.		KRA(3,2)=0	KINI0168	
142.		KRA(4,2)=0	KINI0169	
143.		KRA(5,2)=1	KINI0170	
144.		KRA(9,2)=0	KINI0171	
145.		ZA(2)=0.0	KINI0172	
146.		KRA(2)=2E	KINI0173	
147.		KRA(1,3)=4	KINI0174	
148.		KRA(2,3)=0	KINI0175	
149.		KRA(3,2)=0	KINI0176	
150.		KRA(4,3)=0	KINI0177	
151.		KRA(5,3)=0	KINI0178	
152.		KRA(9,3)=0	KINI0179	
153.		ZA(2)=0.0	KINI0180	
154.		KRA(3)=0.0	KINI0181	
155.	195	IF (KRR(1)-5) 200,195,200	KINI0182	
156.	200	KRA(5,3)=3	KINI0183	
157.	205	ICT=3		
158.		GO 220 I=1,ICT	KINI0196	*COR
159.	215	KRA(10,1)=0	KINI0197	*-12
160.	220	IF (KRR(5)) 225,235,225	KINI0198	
161.	225	ICT=ICT+1	KINI0199	
162.		ICT=ICT+KTF	KINI0200	
163.		GO 230 I=ICT,ICT	KINI0201	
164.		KRA(1,1)=0	KINI0202	
165.		KRA(2,1)=0	KINI0203	
166.		KRA(3,1)=0	KINI0204	
167.		KRA(4,1)=0	KINI0205	
168.		KRA(5,1)=0	KINI0206	


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169. KRA(9,I)=0
170. ZAT(1)=TFA(T-NCT)
171. PRA(1)=0.0
172. CONTINUE
173. KRA(3,NCT1)=KPKSS
174. NCT3=NCT2+1
175. NCT4=NCT2+K15
176. GO TO 240
177. NCT3=NCT1+1
178. NCT4=NCT+K15
179. IF (KPK(6)) 245,240,245
180. NCT5=NCT3+1
181. DO 250 I=NCT3,NCT5
182. KPA(1,I)=0
183. KRA(2,I)=0
184. KRA(3,I)=0
185. KPA(4,I)=0
186. KRA(5,I)=0
187. KRA(9,I)=0
188. ZAT(1)=500.0
189. PRA(1)=0.0
190. WPA(2,I)=1.0F-19
191. CONTINUE
192. IF (KPK(5)) 260,245,260
193. KPA(3,NCT3)=KPKSS
194. KRA(4,NCT3)=2
195. ZAT(NCT5)=1000.0
196. NCT3=NCT3+2
197. NCT4=NCT4+2
198. DO 275 I=NCT3,NCT4
199. KRA(1,I)=0
200. KRA(2,I)=0
201. KPA(3,I)=0
202. KPA(4,I)=2
203. KPA(5,I)=0
204. ZAT(1)=TSA(T-F(C13+1))
205. PRA(1)=0.0
206. IF (KPK(8)-1) 265,265,270
207. KRA(9,I)=0
208. GO TO 275
209. KRA(9,I)=4
210. CONTINUE
211. IF (KPK(9)-1) 285,285,280
212. KRA(9,NCT4)=6
213. NCT3=NCT4+1
214. CONTINUE
215. IF (PC) 285,215,295
216. DO 305 I=1,NCT3
217. KPA(3,I)=1
218. DO 300 J=1,10
219. KPA(3,I)=KPA(3,I)+1
220. ZAT(1)=ZAT(1)+1
221. PRA(1)=PRA(1)+1
222. WPA(1,I)=KPA(3,I)+1
223. WPA(2,I)=KPA(3,I)+1
224. KPA(3,I)=KPA(3,I)+1
225. DO 310 I=1,10

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*COP
*-1

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KIN10207
KIN10208
KIN10209
KIN10210
KIN10211
KIN10212
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KIN10218
KIN10219
KIN10220
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KIN10256
KIN10257
KIN10258
KIN10259
KIN10260
KIN10261
KIN10262
KIN10263

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226. KRA(1,1)=KRA(1,2)
227. KRA(1,2)=0
228. KRA(2,2)=0
229. KRA(3,2)=0
230. ZA(2)=0.0
231. KRA(5,1)=0
232. ZA(1)=7
233. PRA(1)=PC
234. NCT3=CT3+1
235. IF (NCT3-UCT3) 325,320,320
236. NCC=0
237. GO TO 5
238. NO 330 I=1,10
239. KRA(1)=KRA(1,NCC)
240. CONTINUE
241. Z=ZA(NCC)
242. PF=PR(NCC)
243. KRA(1)=KRA(1,NCC)
244. KRA(2)=KRA(2,NCC)
245. KRA(3)=KRA(3,NCC)
246. IF (KRA(4)) 355,355,335
247. DO 345 I=1,PF,N
248. IF ((IFC(1)/3)*delta-IFC(1)) 340,345,340
249. NS=I-1
250. GO TO 350
251. CONTINUE
252. GO TO 355
253. VN(NS+1)=VN(NS+1)
254. TFC(NS+1)=TFC(NS+1)
255. TFC(NS+1)=TFC(NS+1)
256. VTC(NS+1)=VTC(NS+1)
257. FARGO(NS+1)=FARGO(NS+1)
258. FARGO(NS+1)=FARGO(NS+1)
259. N=NS
260. RETURN
261. C
262. FORMAT (J011,6F10.5,2A4,A2)
263. FORMAT (F10.5)
264. END

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KIN10264
KIN10265
KIN10266
KIN10267
KIN10268
KIN10269
KIN10270
KIN10271
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KIN10273
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KIN10275
KIN10276
KIN10277
KIN10278
KIN10279
KIN10280
KIN10281
KIN10282
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KIN10286
KIN10287
KIN10288
KIN10289
KIN10290
KIN10291
KIN10292
KIN10293
KIN10294
KIN10295
KIN10296
KIN10297
KIN10298
KIN10299
KIN10300
KIN10301
KIN10302

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1. C SUBROUTINE ZHIE
2.
3. REAL NELA(1),NEIR(1),FEIN(1),TAU(10,10)
4. EQUIVALENCE (NELA(1),A(1)), (FEIN(1),A(51)), (FEIR(1),A(101)),
5. 1(TAU(1),A(151))
6. DIMENSION YF(100),CJ(100,1)
7. DIMENSION X(1),VLAP(10,1)
8.
9. C
10. CCFRCH FANOA(100),FAFOR(100),RU(10,2),PC(130,2),
11. 1 R(100,2),RE(100,2),PE(100,2),TU(100,2),VN(100),
12. 2 Y(100),YTN(100),VNU(100,30),FF(100),IEC(100),
13. 3 IP(100),CP(100),M(100),Sd(155),TC(100),VLNK(100),
14. 4 E(100),LAMI(100),GAPK(1,1)
15.
16. C COMMON /PARA*1/ KTN,KOUT,JAN,WOL,JAP,IPC,P,KKX(3),KR(10),TILF(3),
17. 1 TMIN,TMAX,VISC,PR(1)
18.
19. C COMMON /PARA*2/ WP,SCH,RHO,VFL,R1,REF,FFA,IS,ISP,P,T,SIF,MTP,
20. 1 FL,FNL,FLIO,NO,IEL,ISPO,KRALP,CPE,TRF,TER,AA,ITS,
21. 2 IM,LL,IT,MODE,HMELT,SMELT,TMAX,TMTN,MELT,SUMN,
22. 3 SUPL,JC,HG,C6G,SVA,SVR,SVC,SVN,SURC,NXC,SAI,
23. 4 VMACH,KRZ2,SP1,GAR,THI,RX,INCHT,HCH,NCU,INT,
24. 5 IPZ,POAT,SRI,IXG,SVI,KKJ,TAC,DXG,SHI,MOATO,
25. 6 SA2,FFE,KS,RV,CME,VA,POS,DUM1,DUM2,EP,TEC,IC,
26. 7 ISP2,ITE,VNU2,WTL
27.
28. C COMMON /APRAYS/ A(16,16),R(16),W(3),XC(50),XC(50),ZKF(10),
29. 1 TLO(10),DMCLO(10),WALJP(10),FR(10),ALPI(10),
30. 2 GAPH(10),GAMF(10),TG(10,3),TX(10,3),WAT(10),
31. 3 LP(10),IOAT(10),KAT(10),DUM(10,10),FRL(10)
32.
33. C EQUIVALENCE (TU(10),TE(1)), (VNU(1),CJ(1))
34.
35. C COMMON /KINETX/ MT,FKEF(50),EAP(50),FKK(50),PNU(10,50),KMU(10,50),
36. 1 PMR(50),PKKK(50)
37.
38. C EQUIVALENCE (B(1),X(1)), (GAPK(1),VLAP(1))
39.
40. C COMMON/ACE1/GAPEX,PEFN,PCH,ACHSQ,SQNAK,XP
41.
42. C COMMON /DIFFER/ IC(11),ALPT(10),C(10),SORCF(2),RA(2),IR(10),
43. 1 IKK,J,VINT,VINT,JAT(10),LJM(10,10),FANA(10),
44. 2 FARB(10),KPAH2)
45.
46. C DIMENSION ATA(10),ATR(10),ATC(10)
47. EQUIVALENCE (TO(1),ATA(1)), (TO(11),ATR(1)), (TO(21),ATC(1))
48.
49. C COMMON/CAPKIN/ KPK(10),ROUCH,NCC
50. COMMON/CONCHO/ Z,GAMER,WR(3)
51. CALL FTIME
52. NFE=0
53. TIMIN=300.
54. TIMAX=20000.
55. Z=0.0
56. PR=0.0

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55. KKJ=0
56. PSV=P
57. JI=0
58. IF (ITS + 1) 5,10,5
59. GAMEX=0.6666667
60. W(1)=1.0
61. W(2)=0.
62. W(3)=0.
63. W(4)=0.
64. W(5)=1
65. NCV=0
66. NOAT=0
67. WP=20.
68. T=3000.
69. HIP=0.
70. STD=0.
71. KR(10)=0
72. ITS=0
73. TDC=1
74. KRALP=0
75. KKJ=0
76. WS=1.0
77. KRA=KR(8)
78. KRQ=KR(4)
79. CALL KIRIN
80. KX(1)=KR(P)
81. WRITE (ROUT,290) TILE,KR
82. KR(8)=0
83. KRZ=0
84. TET=501.
85. KR(4)=KR(4)-1
86. IF (KR(4)) 20,15,15
87. IF (KR(6)) 25,25,20
88. KR(6)=KR(6)-1
89. 25 IF (KR(7)) 35,35,20
90. KR(7)=KR(7)-1+1
91. 35 IF (ABS(W(1)) + ARSLUP(2)) + ABS(WR(3)) 45,45,40
92. 40 W(1)=WR(1)
93. W(2)=WR(2)
94. W(3)=WR(3)
95. KRALP=1
96. CONTINUE
97. IF (KR(1) - 5) 55,50,55
98. KR(1)=0
99. KR(P)=1
100. MOVE=KR(1)
101. KRALP=KRALP+IABS(KR8-KR(P))+IABS(KR4-KR(4))
102. SVA=0.
103. SVP=0.
104. TEZ=0
105. IF (MOVE - 5) 65,60,65
106. STOP
107. IF (GAMER) 70,95,70
108. 70 GAMF=SIGN(AFAXI,IABS(GAMER),0.0001),GAMER)
109. IF (KR(3)) 80,80,75
110. IF (KR(3)-9) 90,80,70
111. J=1

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ZIP10055
ZIP10056
ZIP10057
ZIP10058
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ZIP10066
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ZIP10076
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ZIP10078
ZIP10079
ZIP10080
ZIP10081
ZIP10082
ZIP10083
ZIP10084
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ZIP10086
ZIP10087
ZIP10088
ZIP10089
ZIP10090
ZIP10091
ZIP10092
ZIP10093
ZIP10094
ZIP10095
ZIP10096
ZIP10097
ZIP10098
ZIP10099
ZIP10100
ZIP10101
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ZIP10104
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ZIP10106
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ZIP10109
ZIP10110
ZIP10111

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112.      DO 85 IK=1,N
113.      EF(J)=EF(I)**(GAFER/GAFEX)
114.      J=J+1
115.      GAFEX=GAFEX
116.      IF (Z) 120,100,120
117.      100 IF (MORF-q) 105,155,270
118.      105 IF (MORF-3) 270,110,270
119.      110 IF (PR(S)) 270,270,115
120.      SIP=EXP
121.      GO TO 270
122.      120 IF (RCOF - 1) 125,125,140
123.      125 IF (T) 130,135,135
124.      T=T
125.      IFZ=1
126.      COTIME
127.      135 GO TO 270
128.      140 IF (MORF - 2) 270,255,145
129.      145 IF (MORF-4) 260,150,260
130.      T=7
131.      *COF=2
132.      *COF=2
133.      KKO=-1
134.      KK(S)=X0(P(5),1)
135.      KF(1)=2
136.      PRAC (R10,245) KVI,UR,HTP,PSB,PRCK,SAL,PR1
137.      PHOR=-9999.
138.      KPI=-9999.
139.      IF (UR) 165,170,140
140.      SVI=04
141.      GO TO 170
142.      SVI=VEL
143.      IF (HTP) 175,140,175
144.      HCH=HTP/1.6
145.      140 IF (KSO) 145,200,145
146.      145 IF (KSR + 9999.) 140,140,140
147.      SVI=PSB/1.6
148.      GO TO 266
149.      SVI=UTE
150.      IF (PRCK) 210,215,205
151.      SVI=PROR
152.      GO TO 215
153.      SP1=KOC
154.      215 IF (PR1) 225,230,220
155.      SVI=PR1
156.      GO TO 230
157.      SP1=P
158.      GO TO (235,240,245), KVI
159.      SVI=SGRI (HCH - SP1) * 9010P.)
160.      GO TO 250
161.      HCH=SP1+SVI/9010P.*SVI
162.      GO TO 250
163.      SHI=CH-SV1/9010P.*SVI
164.      SAI=SAI/57.29577
165.      SVA=(1.3146 * SH1 + SV1 * COS(SAI))**2./9010P.
166.      SVA=SVA*2./1.9869
167.      SVC=(SVI * COS(SAI))**2./9010P.+SHI
168.      SVI=SP1+SVB/(1.3146 * SH1)

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280 85 IK=1,N
281 EF(J)=EF(I)**(GAFER/GAFEX)
282 J=J+1
283 GAFEX=GAFEX
284 IF (Z) 120,100,120
285 100 IF (MORF-q) 105,155,270
286 105 IF (MORF-3) 270,110,270
287 110 IF (PR(S)) 270,270,115
288 SIP=EXP
289 GO TO 270
290 120 IF (RCOF - 1) 125,125,140
291 125 IF (T) 130,135,135
292 T=T
293 IFZ=1
294 COTIME
295 135 GO TO 270
296 140 IF (MORF - 2) 270,255,145
297 145 IF (MORF-4) 260,150,260
298 T=7
299 *COF=2
300 *COF=2
301 KKO=-1
302 KK(S)=X0(P(5),1)
303 KF(1)=2
304 PRAC (R10,245) KVI,UR,HTP,PSB,PRCK,SAL,PR1
305 PHOR=-9999.
306 KPI=-9999.
307 IF (UR) 165,170,140
308 SVI=04
309 GO TO 170
310 SVI=VEL
311 IF (HTP) 175,140,175
312 HCH=HTP/1.6
313 140 IF (KSO) 145,200,145
314 145 IF (KSR + 9999.) 140,140,140
315 SVI=PSB/1.6
316 GO TO 266
317 SVI=UTE
318 IF (PRCK) 210,215,205
319 SVI=PROR
320 GO TO 215
321 SP1=KOC
322 215 IF (PR1) 225,230,220
323 SVI=PR1
324 GO TO 230
325 SP1=P
326 GO TO (235,240,245), KVI
327 SVI=SGRI (HCH - SP1) * 9010P.)
328 GO TO 250
329 HCH=SP1+SVI/9010P.*SVI
330 GO TO 250
331 SHI=CH-SV1/9010P.*SVI
332 SAI=SAI/57.29577
333 SVA=(1.3146 * SH1 + SV1 * COS(SAI))**2./9010P.
334 SVA=SVA*2./1.9869
335 SVC=(SVI * COS(SAI))**2./9010P.+SHI
336 SVI=SP1+SVB/(1.3146 * SH1)

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P=SVH
GO TO 270
HIP=Z
GO TO 270
STP=Z
TF (SIP + 9.999.) 270,265,270
STP=SCH
SCHAK=0.
PSV=PCH
TF (PR) 275,265,260
KKJ=1
ACFSG=PR*F
GAME=GAME-1.0
PR=PSV*(1.+GAME/2.*SCHAK)/(1.+GAME/2.*ACHSK)**((GAM/GAME)
KR(5)=1
P=PR
AASP=WM
RETURN
C
290 FORMAT (1H19X,5HGRAPHITE SURFACE KINETICS (GASKET) 2A4,A2,5X10I1)
295 FORMAT (11,F9.4,5F10.4)
END

ZIP10169
ZIP10170
ZIP10171
ZIP10172
ZIP10173
ZIP10174
ZIP10175
ZIP10176
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ZIP10190

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SURROUTINE AFM4T
REAL NFIA(1),NFIB(1),FFIN(1),TAU(10,10)
EQUIVALENCE (NFIA(1),A(1)), (NFIB(1),A(51)), (FFIN(1),A(101)),
1(TAU(1),A(151))
DIMENSION TF(180),CIJ(180,1)
DIMENSION X(1),VLAM(180,1)

COMMON
1 FMOA(180),FAMOR(180),RB(180,2),RC(180,2),
2 RO(180,2),RE(180,2),RF(180,2),TU(180,2),VN(180),
3 Y(180),WTM(180),VNU(180,10),FF(180),IFC(180),
4 IP(180),CP(180),H(180),SH(180),TC(180),VLNK(180),
5 E(180),LMT(180),GAPK(1,1)

COMMON /PARAM1/ KIN,KOUT,JAN,MOL,NAB,IOC,N,KKX(3),KR(10),TILE(3),
1 TTMIN,TTMAX,VISC,PR(1)

COMMON /PARAM2/ WM,SCH,RHO,VEL,B1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
1 EL,ENL,FLIR,HQ,IFL,ISPG,KRALP,CPF,TRE,IER,AA,ITS,
2 IN,IL,IT,MODE,HMELT,SMELT,TMAX,TMIN,MELT,SUMN,
3 SUML,JC,HG,CPG,SVA,SVP,SVC,SVD,SUMC,NXC,SA1,
4 VMACH,KRZZ,SP1,GAM,THI,FX,DMCHI,HCH,NCV,TBT,
5 IFRZ,NOAT,SRI,IXG,SV1,KKJ,IXC,NXG,SH1,NOATO,
6 SA2,FFF,WS,RV,CHF,VA,HOS,DUM1,DUM2,EP,IFCJC,
7 ISP2,WTG,VMU2,WTL

COMMON /APRAYS/ A(16,16),H(16),W(3),XC(50),XG(50),ZKE(10),
1 TLO(10),DMCLO(10),WALJP(10),EB(10),ALP(10),
2 GAMH(10),GAPK(10),TO(10,3),TK(10,3),WAT(10),
3 IP(10),IOAT(10),KAT(10),UM(10,10),ERL(10)
EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))

COMMON /KINETX/ MT,FKE(50),EAK(50),EXK(50),PNU(10,50),PLU(10,50),
1 PMR(50),PKKK(50)

EQUIVALENCE (R(1),X(1)), (GAPK(1),VLAM(1))

COMMON /DIFFER/ IR(11),FNU(10),PNUS(10),SLAM(10),RE(10),RY(10),
1 INC(10),JJ(10),SLB(16),SLA(16,16)

IF TRYING TO PUSH THROUGH TMIN OR TMAX -- REINVERT AND DT TO ZERO
IF (ITS-NCV-1) 5,5,10
DTU=1000.
DTD=DTU.
TTMIN=300.
TTMAX=20000.
CONTINUE
X1=X(1)
IF (T - TMIN) 15,15,20
IF (X(1)) 95,30,20
IF (T - TMAX) 30,25,25
IF (X(1)) 30,30,95
IF NEW COMPENSED HAS NEG CORRECTION, DELETE AFTER REINVERT
IF (IFP) 45,65,35

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55. 35 IF (VN(IREF)) 40,40,65
56. 40 IF (X(IER) + 1.E-30) 45,65,65
57. 45 IF (IRE-N) 55,55,50
58. 50 JC=0
59. 55 CALL SWAP (A,R,SLA,SLR)
60. 60 DO 60 I=1,ISPO
61. 61 A(I,IER)=0.
62. 62 A(IER,I)=0.
63. 63 A(IER,IER)=1.E30
64. 64 R(IER)=-0.1
65. 65 IF (COUNT) 175,190,190
66. 66 IF S.E. ERROR AND CORRECTION ON T OF CONFLICTING SIGN,REINVERT
67. 67 IF (MODE - 1) 160,70,165
68. 68 IF (X(1) + R1) 55,75,75
69. 69 ON S.F. IF DELTA LN T .GT. .9 REINVERT NO 01 IF FL AND ENL ARE SAME
70. 70 IF (ABS(X(1)) - 0.9) 165,165,40
71. 71 IF (ENL - 0.02) 85,90,90
72. 72 IF (FL - 100.) 165,90,50
73. 73 NOFE=0
74. 74 REINVERT
75. 75 CALL SWAP (A,R,SLA,SLR)
76. 76 IF CONVERGED EXCEPT FOR T ON H OR S OPTIONS -- NON CONVERGENT
77. 77 IF (MODE - 1) 155,105,100
78. 78 IF (E1 + 100. * ENL - 1.E - 4) 205,205,155
79. 79 ON S.F. OPTION RESULT IN CONFLICTING FROM/CORRECTION OR T PUSH
80. 80 IF OTHER BALANCES RELATIVELY GOOD, SET T TO TMIN/TWAS AS PER ERROR
81. 81 AND GO TO THERE (IF T ALREADY THERE - NONCONVERGE) ELSE LT TO ZERO
82. 82 IF (ABS(R1) - 100. * (E1 + ENL)) 155,110,110
83. 83 TMIN=AMAX1(TMIN,DTU,300.)
84. 84 TMAX=AMIN1(TMAX,DTU,20000.)
85. 85 IF (X1+R1) 115,155,145
86. 86 IF (R1) 120,120,130
87. 87 IF (T-TMIN) 200,200,125
88. 88 T=AMAX1(TMIN,T-DTU)
89. 89 TMAX=T
90. 90 DTU=DTU/2.
91. 91 GO TO 195
92. 92 IF (T-TMAX) 135,200,200
93. 93 T=AMIN1(TMAX,T+DTU)
94. 94 TMIN=T
95. 95 DTU=DTU/2.
96. 96 IF (ABS(T - TF(JC)) - .001) 140,195,195
97. 97 JFC(JC)=1
98. 98 VN(JC)=1.E-3/VTN(JC)*WTG
99. 99 Y(JC)=0.
100. 100 GO TO 195
101. 101 IF (T-TMIN) 200,200,150
102. 102 IF (T-TMAX) 155,200,200
103. 103 Y(1)=0.
104. 104 MODE=0
105. 105 TMIN=TMIN
106. 106 TMAX=TMAX
107. 107 IN=IN-1
108. 108 IL=2
109. 109 GO TO 190
110. 110 Y(1)=0.
111. 115 IF (X(2) + 1.) 170,210,210

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AFMA0112
AFMA0113
AFMA0114
AFMA0115
AFMA0116
AFMA0117
AFMA0118
AFMA0119
AFMA0120
AFMA0121
AFMA0122
AFMA0123
AFMA0124
AFMA0125
AFMA0126
AFMA0127
AFMA0128
AFMA0129
AFMA0130
AFMA0131
AFMA0132

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1. SURROUTINF ALPST
2. COMMON/ACF1/GAMEX,REFM,PCH,ACHSQ,SQPAK,SXP
3.
4. REAL NFIA(1),NFIR(1),FFIN(1),TAU(10,10)
5. EQUIVALENCE (NFIA(1),A(1)), (NFIR(1),A(51)), (FFIN(1),A(101)),
6. 1(TAU(1),A(151))
7. DIMENSION TF(180),CIJ(180,1)
8. DIMENSION X(1),VLAM(180,1)
9.
10. COMMON
11. 1 FAMOA(180),FAMOB(180),RR(180,2),RC(180,2),
12. 2 RD(180,2),RE(180,2),RF(180,2),TU(180,2),VM(180),
13. 3 Y(180),WTM(180),VNU(180,10),FF(180),IFC(180),
14. 4 IP(180),CP(180),H(180),SB(180),TC(180),VLNK(180),
15. 5 E(180),LAMI(180),GAMK(1,1)
16.
17. COMMON /PARAM1/ KIN,KOUT,JAN,MOL,NAR,IDC,N,KXX(3),KR(10),TILE(3),
18. 1 TTMIN,TTMAX,VISC,PR(1)
19.
20. COMMON /PARAM2/ WM,SCH,RHO,VEL,R1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
21. 1 EL,ENL,FLIR,NQ,IFL,ISQ,KRALP,CP,IRE,IER,AA,ITS,
22. 2 IN,IL,IT,MODE,MWELT,SMELT,TMAX,TMIN,MELT,SUMN,
23. 3 SUML,JC,HG,CPG,SVA,SVR,SVC,SVD,SUMC,NXC,SAI,
24. 4 VMACH,KRZZ,SP1,GAM,THI,MX,DMCHI,HCH,NCV,TRT,
25. 5 IFR2,NOAT,SR1,IXG,SV1,KKJ,IXC,IXG,SH1,NOATO,
26. 6 SA2,FFF,WS,RV,CMF,VA,HOS,DUM1,DUM2,EP,IFCJC,
27. 7 ISP2,WTG,VMU2,NTL
28.
29. COMMON /ARRAYS/ A(16,16),B(16),W(3),XC(50),XG(50),ZKE(10),
30. 1 TLO(10),DMCLO(10),WALUP(10),ER(10),ALP(10),
31. 2 GAMH(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
32. 3 IR(10),IOAT(10),KAT(10),UP(10,10),EBL(10)
33. EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))
34.
35. COMMON /KINETX/ MT,EAK(50),EXK(50),PMU(10,50),RMU(10,50),
36. 1 PHR(50),PKKK(50)
37.
38. COMMON /FOURVALENCE (P(1),X(1)), (GAMK(1),VLAM(1))
39.
40. COMMON /DIFFER/ IC(1),ALPT(10),C(10),SORCE(P),RA(2),IM(10),
41. 1 IT,KK,J,VITI,YINT,JAT(10),LIP(10,10),FAKA(10),
42. 2 FAMB(10),KFHA(2)
43.
44. DIMENSION ATA(10),ATR(10),ATC(10)
45. EQUIVALENCE (TG(1),ATA(1)), (TG(11),ATR(1)), (TG(21),ATC(1))
46.
47. DATA REFD,FFAD/4HREFM,4HFFA /
48. DATA IS,Ic,I7/2H ,2HFI,2HFW/
49. TEMAX=20000.
50. IF (KR(3) - 7) 5,10,10
51. IF (NEF) 145,145,20
52. TGF=NEF
53. READ (VITI,475) NEF
54. NEF=NEF+TGF
55. IND=IND+1

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55. READ (KIN,455) (DEFIA(I),DEFIB(I),DEFIC(I),I=1,NF,DEF)
56. KIN(3)=9-KIN(2)
57. IF (DEFIA(NF) - DEFIB(NF)) 20,15,20
58. TFMAX=DEFIC(NF)
59. GO TO 30
60. IDEF=1
61. IF (DEFIA(1) - DEFIB(1)) 30,25,30
62. TFMAX=DEFIC(1)
63. JI=0
64. DO 50 I=1,NF
65. IF (DEFID-DEFIA(I)) 40,35,40
66. DEF=DEFIB(I)
67. JI=JI+1
68. GO TO 50
69. IF (DEFAC-DEFIB(I)) 50,45,50
70. FAF=DEFIB(I)
71. JI=JI+1
72. CONTINUE
73. IF (JI) 80,30,55
74. DO 75 J=1,M
75. FFC(J)=1.F+10
76. IF (UTP(J)-.01) 75,75,60
77. IF (IFC(J)) 65,70,65
78. IF (IARS(IFC(J))-3) 75,70,75
79. FFC(J)=(UTP(J)/REFM)**(FAF*GAMEX)
80. CONTINUE
81. WRITE (KOUT,460) DEF,FFA
82. IF (DEF-JI) 145,145,80
83. JI=1
84. WRITE (KOUT,460)
85. MP=0+1
86. DO 140 IK=1,NP
87. I=1
88. I1=15
89. I2=15
90. I3=15
91. I4=15
92. IF (IK-N) 85,85,105
93. IF (IFC(J)) 90,105,90
94. IF (IARS(IFC(J)) - 3) 95,105,95
95. IF (TFMAX - 20000.) 100,105,105
96. IFC(J)=TFMAX
97. I=0
98. GO TO 125
99. IF (DEFIA(I) - FANOA(J)) 135,110,135
100. IF (DEFIB(I) - FANOB(J)) 135,115,135
101. IF (DEFIC(I) - 100.) 130,120,120
102. FFC(J)=AMIN1(DEFIB(I),TFMAX)
103. WRITE (KOUT,465) FANOA(J),FANOB(J),FC(J),I1,I2
104. I1=I6
105. I2=I7
106. GO TO 135
107. FFC(J)=DEFIB(I)
108. WRITE (KOUT,470) DEFIA(I),DEFIB(I),DEFIC(I),I3,I4
109. FFC(J)=FFC(J)*GAMEX
110. I3=I6
111. I4=I7

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ALPS0055
ALPS0056
ALPS0057
ALPS0058
ALPS0059
ALPS0060
ALPS0061
ALPS0062
ALPS0063
ALPS0064
ALPS0065
ALPS0066
ALPS0067
ALPS0068
ALPS0069
ALPS0070
ALPS0071
ALPS0072
ALPS0073
ALPS0074
ALPS0075
ALPS0076
ALPS0077
ALPS0078
ALPS0079
ALPS0080
ALPS0081
ALPS0082
ALPS0083
ALPS0084
ALPS0085
ALPS0086
ALPS0087
ALPS0088
ALPS0089
ALPS0090
ALPS0091
ALPS0092
ALPS0093
ALPS0094
ALPS0095
ALPS0096
ALPS0097
ALPS0098
ALPS0099
ALPS0100
ALPS0101
ALPS0102
ALPS0103
ALPS0104
ALPS0105
ALPS0106
ALPS0107
ALPS0108
ALPS0109
ALPS0110
ALPS0111

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112. 135 I=I+1
113. IF (I - NFF) 105,105,140
114. J=J+1
115. NFF=0
116. VS=1.0
117. IF (KR(6)) 165,150,150
118. W(1)=0.
119. IF (KR(4)) 160,160,155
120. IF (KR(4) - 3) 170,160,170
121. W(1)=1.0
122. GO TO 170
123. VS=V(1)+V(2)+K(3)
124. MOAT=MOAT
125. MOAT=0.
126. NUP=0.
127. DO 230 K=1,IS
128. ALPH=(W(1) * TK(K,1) + W(2) * TK(K,2) + W(3) * TK(K,3))/VS
129. IF (ALPH) 175,175,230
130. IF (KAT(K)-99) 185,180,185
131. IF (K(6)) 230,225,225
132. IF (KR(6)) 225,190,205
133. IF (TK(K,1)) 195,195,230
134. IF (KR(8)) 225,225,206
135. IF (TK(K,3)) 225,225,230
136. IF (MOAT) 220,220,210
137. DO 215 KK=1,MOATG
138. IF (LOAT(KK) - K) 215,225,215
139. CONTINUE
140. CONTINUE
141. GO TO 230
142. MOAT=MOAT+1
143. SUM1=SUM1-ALPH
144. LOAT(MOAT)=K
145. CONTINUE
146. VS=VS*(1. + DUM1)
147. DO 235 K=1,IS
148. GAMF(K)=0.
149. ALPH(K)=(W(1) * TQ(K,1) + W(2) * TQ(K,2) + W(3) * TQ(K,3))/VS
150. TEST=1.0
151. IF (KR(6)) 315,245,240
152. STOP 222
153. C SURFACE MASS BALANCE PACKAGE GOFS HERE
154. IF (KR(4) - 2) 290,250,290
155. IF (NCV+KR(3)) 255,255,330
156. PMU2=0.
157. KR(4)=1
158. DO 265 K=1,IS
159. IF (WTM(K)-1.0) 265,260,260
160. VA=VN(K)/FF(K)
161. ZKF(K)=VA
162. PMU2=PMU2+VA*WTM(K)
163. CONTINUE
164. J=ISP
165. DO 280 IK=ISP,N
166. IF (WTM(IK)-1.0) 280,270,270
167. VA=VN(IK)/FF(IK)
168. PMU2=PMU2+VA*WTM(IK)

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169.      NO 275 K=1,IS
170.      ZKE(K)=ZKF(K)+VA*VNU(J,K)
171.      J=J+1
172.      NO 285 K=1,IS
173.      ZKE(K)=ZKF(K)/PMU2
174.      NO 310 I=1,IS
175.      K=IR(I)
176.      IF (KAT(I)-99) 295,300,295
177.      IF (W(1)) 305,305,310
178.      ALP(K)=0.
179.      GO TO 310
180.      ALP(K)=ALP(K)+ZKF(K)
181.      CONTINUE
182.      TEST=1.*W(2)+W(3)
183.      NO 320 K=1,IS
184.      TEST=TEST-ALP(K)*WTM(K)
185.      IF (ARS(TEST) - .001) 335,335,325
186.      WRITE (KOUT,485) . W
187.      STOP
188.      WRITE (KOUT,490)
189.      STOP
190.      IF (KR(3)) 340,340,400
191.      IF (INOAT) 400,400,345
192.      C      RETINITIALIZE SPECIES
193.      PIN=P/10.
194.      PLOG=ALOG(PIN)
195.      J=1
196.      NO 395 IK=1,N
197.      IF (IFC(J) + 1) 350,395,360
198.      IFC(J)=IFC(J)+3
199.      IF (J - IS) 370,370,355
200.      YC=0.
201.      GO TO 375
202.      IF (IFC(J) - 1) 355,395,365
203.      IFC(J)=IFC(J)-3
204.      YC=PLUG
205.      IF (IFC(J)) 385,390,380
206.      IFC(J)=1
207.      VN(J)=0.
208.      Y(J)=YC
209.      GO TO 395
210.      VN(J)=PIN
211.      Y(J)=PLUG
212.      J=J+1
213.      IF (INOAT) 450,450,405
214.      J=1
215.      NO 430 IK=1,N
216.      IF (INOAT - J) 425,410,410
217.      NO 420 L=1,NOAT
218.      K=IOAT(L)
219.      LAMT=LAMT(J)/2*(K - 1)
220.      LAMT=LAMT-(LAMT / 2)*2
221.      IF (LAMT) 415,420,415
222.      VN(J)=0.
223.      IFC(J)=IFC(J)-3
224.      GO TO 430
225.      CONTINUE
275      NO 275 K=1,IS
280      ZKE(K)=ZKF(K)+VA*VNU(J,K)
285      J=J+1
290      NO 285 K=1,IS
295      ZKE(K)=ZKF(K)/PMU2
300      NO 310 I=1,IS
305      K=IR(I)
310      IF (KAT(I)-99) 295,300,295
315      IF (W(1)) 305,305,310
320      ALP(K)=0.
325      GO TO 310
330      ALP(K)=ALP(K)+ZKF(K)
335      CONTINUE
340      TEST=1.*W(2)+W(3)
345      NO 320 K=1,IS
350      TEST=TEST-ALP(K)*WTM(K)
355      IF (ARS(TEST) - .001) 335,335,325
360      WRITE (KOUT,485) . W
365      STOP
370      WRITE (KOUT,490)
375      STOP
380      IF (KR(3)) 340,340,400
385      IF (INOAT) 400,400,345
390      C      RETINITIALIZE SPECIES
395      PIN=P/10.
400      PLOG=ALOG(PIN)
405      J=1
410      NO 395 IK=1,N
415      IF (IFC(J) + 1) 350,395,360
420      IFC(J)=IFC(J)+3
425      IF (J - IS) 370,370,355
430      YC=0.
435      GO TO 375
440      IF (IFC(J) - 1) 355,395,365
445      IFC(J)=IFC(J)-3
450      YC=PLUG
455      IF (IFC(J)) 385,390,380
460      IFC(J)=1
465      VN(J)=0.
470      Y(J)=YC
475      GO TO 395
480      VN(J)=PIN
485      Y(J)=PLUG
490      J=J+1
495      IF (INOAT) 450,450,405
500      J=1
505      NO 430 IK=1,N
510      IF (INOAT - J) 425,410,410
515      NO 420 L=1,NOAT
520      K=IOAT(L)
525      LAMT=LAMT(J)/2*(K - 1)
530      LAMT=LAMT-(LAMT / 2)*2
535      IF (LAMT) 415,420,415
540      VN(J)=0.
545      IFC(J)=IFC(J)-3
550      GO TO 430
555      CONTINUE

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226. 425 CONTINUE
227. 430 J=J+1
228. 435 IF (NOAT - 1) 445,435,435
229. 440 DO 440 L=1,NOAT
230. 445 K=10AT/L)
231. 450 J=IR(K)
232. 455 IFC(J)=IFC(J)+6
233. 460 CONTINUE
234. 465 RETURN
235. C
236. 455 FORMAT (2A4,F12.5,2A4,F12.5,2A4,F12.5)
237. 460 FORMAT (2A4, UPDATE OF DIFFUSION FACTORS/10X,7ASPECTSYLADIFFUSION)
238. 465 10N FACTOR)
239. 470 FORMAT (11X2A4,6XF10.3,2A2)
240. 475 FORMAT (11X2A4,6XF10.5,2A2)
241. 480 FORMAT (13X,5F6.5,F6.4)
242. 485 FORMAT (/5X54HALL GASEOUS DIFFUSION FACTORS RECALCULATED AS (MOL.WEIGHTS PER GRAM) )
243. 490 11/F7.3,3H)F6.3//)
244. 495 1 10X74H1. REARRANGEMENT OF ELEMENTS BETWEEN ENDF AND WALL SOLUTIONALPS245
245. 2NS (KX12).GT.0) /10X2A42. COMPONENT MASS FRACTION ( SET2.4,11H) MOALPS246
246. 3T EQUAL/16X71H10 ZERO FOR UNDEFINED COMPONENT (ALL ZERO GRAM-ATOMIALPS247
247. 4C-WEIGHTS PER GRAM) )
248. 490 1SOLUTION HAS NOT CONVERGENT OR/11X73HNEW FIRST GUESSES HAVE BEEN IALPS249
249. 2INTRODUCED IN INPUT SUBROUTINE (KX(3)=1 TO 4) )
250. 251. END
252.

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ALPS0226
ALPS0227
ALPS0228
ALPS0229
ALPS0230
ALPS0231
ALPS0232
ALPS0233
ALPS0234
ALPS0235
ALPS0236
ALPS0237
ALPS0238
ALPS0239
ALPS0240
ALPS0241
ALPS0242
ALPS0243
ALPS0244
ALPS0245
ALPS0246
ALPS0247
ALPS0248
ALPS0249
ALPS0250
ALPS0251
ALPS0252

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1. SUBROUTINE HELCH
2.
3. REAL MFI(1),MFI(1),MFI(1),TAU(10,10)
4. EQUIVALENCE (MFI(1),A(1)), (MFI(1),A(5)), (MFI(1),A(10)),
5. 1(TAU(1),A(15))
6. DIMENSION TC(100),CIJ(100,1)
7. DIMENSION X(1),VLAM(100,1)
8.
9. COMMON
10. FAMOA(100),FAMOB(100),RR(100,2),RC(100,2),
11. RQ(100,2),PE(100,2),PE(100,2),TU(100,2),VH(100),
12. Y(100),WTH(100),VH(100,10),FF(100),IEF(100),
13. IP(100),CP(100),H(100),SC(100),TC(100),VLAM(100),
14. E(100),LANT(100),GAMP(1,1)
15.
16. COMMON /PARAM1/ KTH,KOUT,JAN,NOL,DAE,IGC,G,KKK(3),PH(10),TTLF(3),
17. TTHIN,TNAX,VISC,PH(1)
18.
19. COMMON /PARAM2/ WM,SCARHO,VFL,B1,MFF,FFA,TS,ISP,P,T,SIF,HIP,
20. FL,ENL,FLTQ,NG,IFL,ISHQ,KRALP,CFE,IRF,IFR,AA,ITS,
21. IN,IL,IT,MDF,HMELT,SMELT,IMAX,TWIN,MELT,SUMN,
22. SIML,JG,HG,CPG,SVA,SVI,SVC,SVD,SUMC,NXC,SAT,
23. VMACH,KRZ2,SP1,GAH,THI,MX,DNCHT,ACH,NCV,TRT,
24. IFRZ,MOAT,SRI,IXG,SVI,KKJ,IXC,NXG,SHI,MOATO,
25. SAZ,FFF,WS,RV,CMF,VA,HOS,DUM1,DUM2,EP,IFCUC,
26. ISP2,WTC,VHU2,WTL
27.
28. COMMON /APRAYS/ A(16,16),H(16),W(3),YC(50),XG(50),ZKE(10),
29. TLO(10),DNCLG(10),SWAI,JP(10),FER(10),ALP(10),
30. GAMB(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
31. IP(10),IOAT(10),KAT(10),UM(10,10),FRL(10)
32. EQUIVALENCE (TU(10),TF(1)), (VHU(1),CIJ(1))
33.
34. COMMON /KINETX/ MT,FKE(50),EKK(50),PMU(10,50),PMU(10,50),
35. PMP(50),PKKK(50)
36.
37. EQUIVALENCE (B(1),X(1)), (GAMP(1),VLAM(1))
38.
39. COMMON /DIFFER/ IC(11),ALPT(10),C(10),SORCE(F),RA(2),IM(10),
40. II,KK,J,VINT,VINT,JAT(10),LIF(10,10),FAMA(10),
41. FAMB(10),KPH(2)
42.
43. DIMENSION ATA(10),ATR(10),ATC(10)
44. EQUIVALENCE (TR(1),ATA(1)), (TG(11),ATB(1)), (TR(21),ATC(1))
45.
46. IF (J - IS) 10,10,15
47.
48. JM=J-1
49. WRITE (KOUT,190) JM,IS,(FAMA(1),FAMB(1),I=1,JM)
50. WRITE (KOUT,195) (FAMA(1),FAMB(1),I=ISP,N)
51. STOP
52. DO 25 L=2,IS
53. JM=ISP-L
54. INJ=IN(JM + 1)
55. IF (JM - 1) 30,20,20
56. DO 25 K=1,JM

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*COR
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55. UGH=TAU(IPJ,K)
56. DO 25 I=1,IS
57.   IM(I,K)=UM(I,K)-UGH*UM(I,JM + 1)
58.   CONTINUE
59.   DO 50 I=1,IS
60.     IM(I,I)
61.     IF (IM(I - 1) 40.50,40
62.     DO 45 K=1,IS
63.       VSUM(K,IM)
64.       UPRK,IM)=UM(K,I)
65.       UM(K,I)=V
66.       IM(I)=IM(IM(I))
67.       IM(IM(I))=IM(I)
68.       GO TO 35
69.     CONTINUE
70.     ----ELEMENT -- BASE GAS CORRESPONDENCE
71.     C INITIALIZE ROW AND COLUMN SUMS
72.     TG=IS
73.     DO 55 I=1,IS
74.       IM(I)=1
75.       IC(I)=1
76.       C EVALUATE INITIAL SUMS
77.       LA=0.1
78.       DO 70 J=1,IS
79.         DO 65 J=1,IS
80.           LAMT=LAMIC(J)/LAMB
81.           IF (I,J)=LMT-(LAMY / 2)*2
82.             IF (I*(I,J)) 60,65,60
83.             IC(J)=IC(J)+1
84.             IM(I)=IM(I)+1
85.           CONTINUE
86.           LAMU=LAMU+LAMB
87.           C CHECK FOR ZLROS
88.           T2=0
89.           DO 165 I=1,IS
90.             IF (IC(I) - T2) 120,95,120
91.             DO 50 J=1,IS
92.               IF (LTH(J,I)) 95,90,95
93.               CONTINUE
94.               IC(I)=J
95.               IM(J)=I
96.               LTH(J,I)=0
97.               DO 115 K=1,IS
98.                 IF (I*(J,K)) 100,105,100
99.                 IC(K)=IC(K)+1
100.                LTH(J,K)=0
101.                IF (I*(K,I)) 110,115,110
102.                LTH(K,I)=0
103.                IM(K)=IM(K)+1
104.                CONTINUE
105.                GO TO 170
106.                IF (IP(I) - T2) 145,125,145
107.                DO 135 J=1,IS
108.                  IF (I*(I,J)) 130,135,130
109.                  IC(J)=1
110.                  IM(J)=J
111.                  LTH(I,J)=0

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BELC0055
BELC0056
BELC0057
BELC0058
BELC0059
BELC0060
BELC0061
BELC0062
BELC0063
BELC0064
BELC0065
BELC0066
BELC0067
BELC0068
BELC0069
BELC0070
BELC0071
BELC0072
BELC0073
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BELC0099
BELC0100
BELC0101
BELC0102
BELC0103
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BELC0109
BELC0110
BELC0111

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112.      GO TO 140
113.      CONTINUE
114.      DO 160 K=1,IS
115.      IF (LTP(K,J)) 145,150,145
116.      F(K)=F(C)-1
117.      LTP(K,J)=0
118.      IF (LTP(I,K)) 155,160,155
119.      LTP(I,K)=0
120.      TC(K)=IC(K)-1
121.      CONTINUE
122.      GO TO 170
123.      CONTINUE
124.      IZ=IZ+1
125.      GO TO 20
126.      J=IS+1
127.      IF (IS) 175,175,75
128.      DO 180 I=1,IS
129.      K=1+L(I)
130.      F(K)=F(C)+K
131.      F(K+1)=F(K)+K
132.      WRITE (MOUT,200) (I,ATC(I)),I=1,IS
133.      WRITE (MOUT,205) (F(K)+F(K+1)),I=1,IS
134.      DO 185 I=1,IS
135.      DO 185 I=1,IS
136.      TC(I)=0
137.      GO 185 K=1,IS
138.      TC(I)=TC(I)+L(I)*K+TC(K)+1
139.      RETURN
140.      C
141.      FORMAT (///15H ONLY FOLLOWING 13,230 CASE SPECIES FOUND FOR 13,
142.      1 5H ELEMENTS/(2X20A4))
143.      FORMAT (//30H OTHER SPECIES CONSIDERED VERF/(2X20A4))
144.      145  FORMAT (//X,9H ELEMENTS,7X,150H/(20X,15/4))
145.      200  FORMAT (//X,120H CASE SPECIES,3X,5(20A4,4X)/(20X,5(20A4,4X)))
146.      205  FORMAT (//X,120H CASE SPECIES,3X,5(20A4,4X)/(20X,5(20A4,4X)))
147.      END

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FELC0112
FELC0113
FELC0114
FELC0115
FELC0116
FELC0117
FELC0118
FELC0119
FELC0120
FELC0121
FELC0122
FELC0123
FELC0124
FELC0125
FELC0126
FELC0127
FELC0128
FELC0129
FELC0130
FELC0131
FELC0132
FELC0133
FELC0134
FELC0135
FELC0136
FELC0137
FELC0138
FELC0139
FELC0140
FELC0141
FELC0142
FELC0143
FELC0144
FELC0145
FELC0146
FELC0147

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1. SUBROUTINE CRECT (NCE)
2. DIMENSION DY(1),DYA(1)
3.
4. REAL NFA(1),NFB(1),FFIN(1),TAU(10,10)
5. EQUIVALENCE (NFA(1),A(1)), NFB(1),A(5)), (FFIN(1),A(10)),
6. 1(TAU(1),A(15))
7. DIMENSION TF(100),CLJ(100,1)
8. DIMENSION X(1),VLA(100,1)
9.
10. COMMON /PARA01/ FAKOR(100),RPA(100,2),RC(100,2),
11. RC(100,2),PE(100,2),PE(100,2),VM(100),
12. Y(100),KTB(100),VMU(100,10),FE(100),TEC(100),
13. IP(100),CF(100),H(100),SA(100),IC(100),VLOR(100),
14. E(100),LAMP(100),GAPK(1,1)
15.
16. COMMON /PARA02/ KTB,KOUT,JA,PAOL,NAP,TEC,P,KKX(3),KPB(10),TILE(3),
17. TMIN,TMAX,VISC,PK(1)
18.
19. COMMON /PARA03/ RP,SGH,RHO,VLA,MI,MFE,FEFA,IS,ISP,P,T,STF,HP,
20. EL,EML,FLIG,NO,TEL,ISQ,KHALP,CPE,TRF,TER,AA,ITS,
21. IP,IT,IT,MODE,HMELT,SELT,TRAX,TRIM,MEI,T,SUMN,
22. SUFF,JC,HG,CDE,SVA,SVR,SVC,SVD,SUMC,NXC,SAL,
23. VACH,KPZZ,SP1,GAM,DTT,EX,OPCHT,UCH,NCV,TRT,
24. IENZ,NDAT,CRI,1XG,SVI,MKJ,XC,XG,SH,NDATO,
25. SA2,FEF,MS,RV,CME,VA,HOS,DUU1,DUM2,FP,IFCJC,
26. ISP2,VTG,VMU2,NTL
27.
28. COMMON /ARRAYS/ A(16,16),P(16),N(3),VC(50),XG(50),ZKE(10),
29. TIC(10),DMCLO(10),VALJP(10),FR(10),ALP(10),
30. GAPK(10),GAPF(10),TG(10,3),TK(10,3),WAT(10),
31. IR(10),IOTAT(10),KAT(10),UR(10,10),EAL(10)
32.
33. EQUIVALENCE (TIC(1),TE(1)), (VMU(1),CIJ(1))
34.
35. COMMON /KINETX/ MT,FKE(50),EAK(50),FKK(50),PMU(10,50),PMU(10,50),
36. PPH(50),PKK(50)
37.
38. EQUIVALENCE (R(1),X(1)), (GAPK(1),VLAN(1))
39.
40. COMMON /DIFFER/ IG(1),FPU(10),PMUS(10),SLAM(10),PE(10),MY(10),
41. IRC(10),JJ(10),SLR(10),SLA(16,16)
42.
43. EQUIVALENCE (A(1),DY(1),DYA(1))
44.
45. N1=1
46. N=IR(1)
47. NTL=0,
48. VTE=0,
49. DIMP2=0,
50. T=1
51. ITW=RR(R)+N
52. DO 130 JK=1,IM
53. DYTCME=DY(TK)
54. IF (DYT) 10,5,10
55. IF (IFC(1)) 150,50,120
56. IF (IFC(1)) 90,15,115

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55. IF (IP(I)) 20,45,20
56. IF (M - IK) 25,30,25
57. IF (KOF) 45,45,35
58. M1=M1+1
59. M=IR(M1)
60. VP(I)=VN(I)*(1. + DYI)
61. IF (VN(I)) 45,45,40
62. Y(I)=ALOG(VN(I))
63. GO TO 50
64. Y(I)=Y(I)+DYI
65. VP(I)=EXP(Y(I))
66. VA=VTF(I)*VN(I)
67. WIG=WTG+VA
68. DU*2=DUP2+VA/FF(I)
69. IF (IK - IS) 55,55,65
70. PHUS(I)=VA(I)
71. IF (KR(6)) 130,60,60
72. SLAM(I)=VN(I)/FF(I)
73. GO TO 130
74. DO 75 K=1,IS
75. VA=VN(I)*K*VP(I)
76. IF (KR(6)) 75,76,75
77. SLAM(K)=SLAM(K)+VA/FF(I)
78. PHUS(K)=PAUS(K)+VA
79. IF (KR(6)) 130,130,80
80. DO 85 K=1,IS
81. SLAM(K)=SLAM(K)+VN(I)*VLAH(I,K)
82. C NON-PRESENT BASE CORRECTIONS AND TESTS
83. Y(I)=Y(I)+DYI
84. IF (Y(I)) 130,95,95
85. IF (IFC(I) + 1) 130,100,100
86. IF (KR(6)) 110,105,105
87. IF (T - TF(I) + .001) 130,110,110
88. Y(I)=0.
89. IFC(I)=+1
90. GO TO 130
91. VN(I)=VA(I)+DYI
92. IF (VN(I)) 125,125,120
93. PHI=PHI+VN(I)*MIN(I)
94. GO TO 130
95. VN(I)=0.
96. IFC(I)=-1
97. I=I+1
98. IF (KR(6)) 145,135,145
99. FFF=VTC/DUP2
100. DO 146 I=1,IS
101. SLAM(I)=SLAM(I)*FFF
102. RETURN
103. END

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CREC0055
CREC0056
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CREC0097
CREC0098
CREC0099
CREC0100
CREC0101
CREC0102
CREC0103

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1. C PROGRAM CASCT,INPUT,OUTPUT,PUNCH,TAPF16,TAPF5=INPUT,TAPF6=OUTPUT,CASK0000
2. C CASK0001
3. C *****
4. C CASK0004
5. C CASK0005
6. C CASK0006
7. C CASK0007
8. C CASK0008
9. C CASK0009
10. C CASK0010
11. C CASK0011
12. C CASK0012
13. C CASK0013
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15. C CASK0015
16. C CASK0016
17. C CASK0017
18. C CASK0018
19. C CASK0019
20. C CASK0020
21. C CASK0021
22. C CASK0022
23. C CASK0023
24. C CASK0024
25. C CASK0025
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27. C CASK0027
28. C CASK0028
29. C CASK0029
30. C CASK0030
31. C CASK0031
32. C CASK0032
33. C CASK0033
34. C CASK0034
35. C CASK0035
36. C CASK0036
37. C CASK0037
38. C CASK0038
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40. C CASK0040
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43. C CASK0043
44. C CASK0044
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95. C CASK0095
96. C CASK0096
97. C CASK0097
98. C CASK0098
99. C CASK0099
100. C CASK0100

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55. 1      T=C(10),C(10),SLB(10),SLA(10,16)
56. 2      *T=PPY(P)
57.
58. C      COMON(CASKEIN/ KKP(10),FOURK*CC
59. C      I/O SPECIFICATIONS ALSO IN RERY
60. KTR=5
61. KOUT=6
62. JAM=18
63. ACC=0
64. REFIN= JAM
65. ITS=0
66. CALL Z1PTN
67. IF (KP(2) + KP(3)) 10,10,15
68. 10  IF (KRALP) 40,40,45
69. 15  TI=0
70.  IF (KP(2)) 25,25,20
71.  CALL TMEI*
72.  IF (KP(3)) 35,35,25
73.  IF (KP(3) - 9) 30,35,35
74.  CALL THPUT
75.  CALL HELCH
76.  CALL THPUT
77.  REFIN= JAM
78.  CALL ALPST
79. 40  IF (KP(7) - 1) 45,45,60
80. 45  IF (KKJ) 50,55,55
81. 50  KKJ=-3
82.  GO TO 60
83. 55  IF (KP(1)-2) 60,65,65
84. 60  MONE=2
85.  JJC=JC
86.  IIT=IT
87.  CALL MAT1
88.  CALL MAT2
89.  CALL MAT3
90.  JC=JJC
91.  IIT=IT
92. 65  IF (KR(6)) 75,70,70
93. 70  ISPO=ISP2
94. 75  MONE=KR(1)
95.  CALL RERY (ISPO,7.0,8.0,0.0,IC)
96.  CALL PROPS
97.  KR(7)=MIN(1,KP(7))
98.  IQI=0
99.  IF (KKJ) 80,80,40
100. 80  CALL OUTPT
101. C      PRINCIPAL ITERATIVE LOOP
102. 85  IF (ITS) 4,95,90
103. 90  IF (MODE) 100,100,95
104. 95  CALL THEM
105.  IF (IFRZ) 100,100,150
106. 100 MONE=KR(1)
107.  FLTG=0.
108.  CALL MAT1
109.  CALL MAT2
110.  CALL MAT3
111.  ITS=ITS+1

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GASK0055
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GASK0111

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112.      R1=R(1)
113.      IF (KR(9)) 110,110,105
114.      CALL KINFT
115.      MOP=1
116.      IF (KR(7) - 1) 125,120,115
117.      I00=-2
118.      WRITE (KOUT,215) (I,I=1,IS)
119.      UP1F (KOUT,210) ITS,T,AA,FL,FUL,CHE,(E(1),I=1,IS)
120.      IF (ITS) 45,40,130
121.      IT=ITS
122.      IF (ITS-67) 140,135,140
123.      KR(7)=9
124.      I00=-2
125.      IF (ITS-70) 155,155,145
126.      NCV=1
127.      KR(7)=4
128.      I00=-2
129.      ITS=-1
130.      GO TO 45
131.      CALL SWAP (SLA,SLP,A,H)
132.      ICT=10
133.      DUM1=0.
134.      I01=100
135.      DO 170 I=1,IS
136.      IF (IFC(I) - 1) 170,170,165
137.      A(I + 2,I + 2)=1.F+10
138.      CONTINUE
139.      I00=101
140.      CALL PERAY (TR,A(7),I1) 40,ROIL) 41,0,100)
141.      ICT=ICT-1
142.      IF (ICT) 190,175,175
143.      IF (I00) 190,140,140
144.      CALL AFAT
145.      GO TO (140,45,145,185), I0
146.      CALL SCALE (M01)
147.      CALL CRECT (M01)
148.      IF (CMF - 1.F - 12) 130,190,205
149.      IF (ICV) 190,200,195
150.      CALL SWAP (A,B,SLA,SLP)
151.      GO TO 145
152.      NCV=1
153.      GO TO 45
154.      IF (KR(7) - 1) 65,45,60
155.      C
210.      FORMAT (/41X,14,F0.2,1P4E10.2/(10I0F12.5))
215.      FORMAT (10I,40Z,40Z,1TC TEEF  PAFS+MET F04UL FR  PAFSAI FR  SCALF
1      /16(13.70 F4S.0L1))
156.      END

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GASK0112
GASK0113
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1.      C      COMMON /PARAM1/ KTN,KNTY,JAN,MOL,NAF,IPC,N,KKX(3),KR(10),TITLE(1),
2.      REAL NFA(10),NFB(1),FFIN(1),TABU(10,10)
3.      EQUIVALENCE (NFA(1),N(1)), (NFB(1),N(5)), (FFIN(1),A(101)),
4.      102(1),A(11))
5.      DIMENSION TF(180),CIJ(180,1)
6.      COMPLEX X(1),W(1),W(180,1)
7.
8.      C
9.      COMMON /PARAM2/ W,SCH,RHO,VFL,B1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
10.      RD(180,2),RE(180,2),RF(180,2),TU(180,2),VN(180),
11.      Y(180),WTH(180),VNU(180,10),FF(180),IFC(180),
12.      IP(180),CP(180),M(180),SH(180),TC(180),VLNK(180),
13.      E(180),LANT(180),GAPK(1,1)
14.
15.      C      COMMON /PARAM1/ KTN,KNTY,JAN,MOL,NAF,IPC,N,KKX(3),KR(10),TITLE(1),
16.      17.      TTPIN,TTMAX,VISC,PR(1)
17.      C
18.      COMMON /PARAM2/ W,SCH,RHO,VFL,B1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
19.      EL,EHL,FLIQ,MQ,IFL,ISPG,KKALP,CPF,IRE,IER,AA,ITS,
20.      IN,IL,IT,PODE,HMELT,SMELT,TMAX,TMIN,MELT,SUMN,
21.      SUML,JC,MG,CPG,SVA,SVR,SVC,SVD,SUMC,NXC,SAL,
22.      VNA,CH,KRZ2,SP1,GAB,THI,MA,PRCHI,HCH,NCV,TBT,
23.      IFP2,NOAT,SRI,IXG,SVI,MKJ,IXC,NKG,SHI,NCATO,
24.      SA2,FFF,WS,RV,CNF,VA,HOS,DUM1,DUM2,EP,IFCJC,
25.      ISP2,WT6,VNU2,WTL
26.
27.      C      COMMON /ABRAYS/ A(16,16),B(16),X(3),XC(50),XG(50),ZKE(10),
28.      1      TLO(10),CPCLC(10),WALJP(10),ER(10),ALP(10),
29.      2      GAMH(10),GAMF(10),IG(10,3),TK(10,3),NAT(10),
30.      3      IR(10),IOAT(10),KAT(10),UM(10,10),EBL(10)
31.      EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))
32.
33.      C      COMMON /KTMETX/ MT,FKF(50),EAK(50),FYK(50),PMU(10,50),RMU(10,50),
34.      1      PFR(50),PKKK(50)
35.      C
36.      EQUIVALENCE (B(1),X(1)), (GAMK(1),VLAM(1))
37.
38.      C      COMMON /DIFFER/ IR(11),FNU(10),PMUS(10),SLAM(10),RE(10),BY(10),
39.      1      IHC(10),JU(10),SLR(16),SLA(16,16)
40.      C
41.      WSSE=AS
42.      DO 5 I=1,IS
43.      IBC(1)=IFC(1)
44.      IF (KR(6)) 40,15,10
45.      USSE=MIN(1,(1),C,)+AMIN1(W(2),0,)+AMIN1(W(3),0,.)
46.      WS=W(1)+V(2)+W(3)
47.      GO TO 20
48.      CONTINUE
49.      IF (ITS) 25,40,40
50.      DO 35 I=1,IS
51.      IF (IBC(1)-1) 35,30,35
52.      IFC(1)=-1
53.      CONTINUE
54.      RV=VCS-XTH/WT6

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55. IF (KR(7) - 1) 60.45,50
56. IF (ITS) 40.55,60
57. WRITE (KOUT,325) FFF,WL,WIG,AA,PV,ALP,PNUS,SLAM
58. KR(7)=KR(7)-1
59. IF (KR(7) - 1) 60.55,60
60. WRITE (KOUT,330) (I,I=1,IS)
61. C INITIALIZE
62. EL=0.
63. CP6=0.
64. EP=P
65. CFF=0.
66. JC=0
67. JCS=0
68. TSPQ=IS+2
69. R(1)=0.
70. R(2)=0.
71. A(1,1)=0.
72. A(1,2)=0.
73. A(2,1)=0.
74. A(2,2)=0.
75. C ----INITIALIZE CONTRIBUTION OF MOST SIGNIFICANT SPECIES IN EACH
76. DO 65 I=1,IS
77. ER(I)=0.
78. E(I)=AA*ALP(I)
79. TSP2=TSPQ
80. C -- - MAIN RASE SPECIES LOOP
81. DO 315 IK=1,IS
82. I=2-IND(IK)
83. IF (KAT(IK)-99) 75,70,75
84. DUS(I-2)=0.
85. C ZERO MATRIX
86. DO 80 K=1,TSPQ
87. AK,IJ=0.
88. IF (ITS) 100,85,100
89. C NORMALIZE ON PRESSURE ON FIRST PASS
90. VN(I-2)=VN(I-2)/SUMH
91. ERL(I-2)=0.
92. IF (INC(I-2)) 100,90,95
93. Y(I-2)=Y(I-2)-SUML
94. GO TO 100
95. IF (SUMC.NE. 0.0) VN(I-2)=VN(I-2)/SUMC
96. IF (SUMC.EQ. 0.0) VN(I-2)=0.0
97. C INITIALIZE SOME MORE
98. R(I)=0.
99. A(I,1)=0.
100. IP(I-2)=0.
101. C SET FLAG INDICATING SIGNIFICANCE OF SPECIES IN MASS
102. C BALANCE(S) AND INCREMENT COUNT ON SIGNIFICANT SPECIES
103. IF (VN(I-2) - ERL(I-2)) 110,110,105
104. IP(I-2)=1
105. C TREAT RASE SPECIES CONTAINING BUT NOT REPRESENTING NON-PRESENT
106. C ELEMENTS IN SAME MANNER AS NON-PRESENT COMPENSED SPECIES
107. IF (INC(I-2)+1) 315,115,115
108. IF (INC(I-2)) 170,205,120
109. A(I,I)=1.
110. VA=VN(I-2)
111. IF (IABS(JAC(I-2)-3)-1) 125,270,130

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112. 125 A(2,I)=1.0
113. GO TO 270
114. 130 IF (EAI - 2) - APS(VA)) 135,140,140
115. 135 EAI - 2)=ABS(VA)
116. 140 TH1 - 2)=J-2
117. 145 IF (I - 2)=F(I - 2)-VA
118. 150 IF (K(6)) 145,150,150
119. 155 DO 155 K=1,IS
120. 160 A(2,I)=EAI*(I-2)*(PIQS(K)/LTG+GANE(K))
121. 165 A(I,I)=A(I,I)+1.
122. 170 YPNE=AXI(TFII,TF(I - 2))
123. 175 IF (T - TF(I - 2) + .001) 165,165,170
124. 180 A(I,I)=1.0E+10
125. 185 F(I - 2)=VM(I - 2)*1.001E+10
126. 190 VMIE=0
127. 195 IF (K(6)-1) 175,180,175
128. 175 IF (K(6)) 270,270,140
129. 180 IF (TF(I - 2) + .001 - T) 315,185,185
130. 185 IF (JC) 195,195,190
131. 190 IF (Y(I-2)-QJC) 315,315,195
132. 195 QJC=Y(I-2)
133. JCS=JC
134. TMAX=TF(I - 2)
135. JC=I-2
136. TFCJC=TFC(I-2)
137. 200 A(I,JCS+2)=0.
138. A(I,I)=1.0
139. R(I)=QJC
140. GO TO 315
141. C ----GAS PHASE
142. 205 VA=VM(I - 2)
143. PFE=CPG+VA*CF(I - 2)
144. A(I,I)=VA
145. A(2,I)=VA
146. EP=EP-VA
147. 210 IF (KAT(I)-49) 210,265,210
148. 215 DO 220 K=1,IS
149. 220 A(K+2,I)=GAP(I-2,K) + GAP(K) * H(T-2))*VA
150. A(I,I)=A(I,I)+VA*V
151. 225 DO 235 K=1,IS
152. 235 K=1,IS
153. 240 IF (EAI - 2) - APS(VA) + 2.1)) 225,230,230
154. 245 F(K)=ABS(A(K + 2,I))
155. 250 T(I)=I-2
156. 255 F(K)=F(K)-A(K + 2,I)
157. 260 A(K + 2,I)=A(K + 2,I)+HUR2*PQUS(K)
158. 265 GO TO 270
159. 270 HUR1=TH1(I - 2)/NTG+VA
160. 275 HUR2=WT/NTG*HUR1
161. 280 IF (K(4)) 245,245,250
162. 285 FWT=0.
163. 290 VA=HUR + 1.)*VA
164. 295 GO TO 255
165. 300 HUR1=HUR1*(1. - FFE / FFE(I - 2))
166. 305
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168.

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110


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55. IF (IFC(J)) 70.345.105
56. IF (IFC(J)+1) 345.30.30
57. IF (ITS) 50.35.50
58. VA(J)=VN(J)/SUMC
59. IF (IFC(J)) 50.45.40
60. IF (SUMC .EQ. 0.0) VN(J)=VN(J)/SUMC
61. IF (SUMC .EQ. 0.0) VN(J)=0.0
62. GO TO 50
63. V(J)=Y(J)-SUMC
64. F(J)=V(LK(J))-Y(J)
65. DO 65 I=1,IS
66. IF (IFC(I)) 60.60.55
67. FNU(I)=0.
68. GO TO 45
69. FNU(I)=VN(I)*(J,I)
70. E(J)=E(J)+FNU(I)*V(I)
71. CONTINUE
72. EAP=ABS(E(J))
73. IF (IFC(J)) 70.250.105
74. COMPENSED SPECIES
75. FAB=E(J)
76. IF (KR(I)) 45.75.75
77. IF (1-IF(J)*.001) 80.85.85
78. FAB=0.
79. IF (KR(5)) 195.195.205
80. IF (E(J) - EER) 195.195.90
81. FFP=E(J)
82. IF (IFP) 95.95.100
83. ISPO=ISPO+1
84. IF=ISPO
85. IF=IFN
86. IF=IK
87. GO TO 110
88. ISPO=ISPO+1
89. IF=ISPO
90. WT=0.
91. IF (KR(5)) 120.115.115
92. TMIN=MAX1(TE(J),TMIN)
93. WTR=WTN(J)/WTG
94. DO 125 I=1,ISPO
95. A(I,IF)=0.
96. A(TE,I)=0.
97. DO 140 K=1,IS
98. PUN1=VNU(J,K)
99. IF (IFC(K)-1) 130.130.140
100. VA=0.001*VNU(J)
101. A(K+2,IC)=PUN1-WTR*(PNU(K) +GAMF(K)*WTG)
102. RE(K)=RE(K)-VA
103. IF (ABS(VA) - ER(K)) 140.140.135
104. ED(K)=ABS(VA)
105. TS(K)=IK
106. CONTINUE
107. K=TE-ISP2
108. IF (IK-I) 165.165.145
109. JK(K)=JC
110. A(IE)=Y(JC)
111. IF (JC-IS) 155.155.150

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112.	150	ATF(J)=TC(JC)	8AT20111
113.		ATF(J)=JC	8AT20112
114.	155	FFJ=Z(J)	8AT20113
115.		IF (H(JC) 375,375,160	8AT20114
116.	160	FA=AS(FA)	8AT20115
117.		GO TO 375	8AT20116
118.	165	AKO=J	8AT20117
119.		ATF(J)=TC(J)	8AT20118
120.		ATF(J)=JC	8AT20119
121.	170	IF (T+COI-TC(J)) 175,175,170	8AT20120
122.		IF (H(JC) 190,190,200	8AT20121
123.	175	IF (H(JC) - 1) 180,185,186	8AT20122
124.	180	IF (H(JC) 190,185,185	8AT20123
125.	185	ATF(J)=J+10	8AT20124
126.		ATF(J)=H(JC)+J,001E+10	8AT20125
127.		DOFF=0	8AT20126
128.	190	IF (H(JC) - 2) 195,195,240	8AT20127
129.	195	IF (H(JC) - 1) 375,300,375	8AT20128
130.	200	IF (T-TC(J)-H(JC)) 205,205,220	8AT20129
131.	205	IF (JC) 215,215,210	8AT20130
132.	210	IF (H(JC)-H(JC) 365,365,215	8AT20131
133.	215	FA=H(JC)	8AT20132
134.		JC=IF	8AT20133
135.		TC(JC)=TC(JC)	8AT20134
136.		TX=TC(JC)	8AT20135
137.	220	IF (H(JC) 225,225,220	8AT20136
138.		IF (H(JC)-2) 365,225,210	8AT20137
139.	225	H(JC)=JC	8AT20138
140.		DO 230 H(JC)+5	8AT20139
141.	230	ATF(J)+2)=H(JC)	8AT20140
142.		ATF(J)=TC(J)	8AT20141
143.		GO TO 365	8AT20142
144.	235	H(JC)=H(JC)	8AT20143
145.		GO TO 345	8AT20144
146.	240	H(JC)=H(JC)	8AT20145
147.	245	ATF(J)=H(JC)	8AT20146
148.		ATF(J)=ATF(J)-VL(J)*H(JC)	8AT20147
149.		CFF=CF+CF(J)*H(JC)	8AT20148
150.		GO TO 375	8AT20149
151.	C	605 PLASE SPEC DS	8AT20150
152.	250	IF (J)=0	8AT20151
153.		IF (H(JC) 255,275,255	8AT20152
154.	255	TC=0	8AT20153
155.		CFF=CF+H(JC)*H(JC)	8AT20154
156.		IF (H(JC) 265,260,265	8AT20155
157.	260	FFJ=FF/JC	8AT20156
158.	265	H(JC)=H(JC)+H(JC)	8AT20157
159.		H(JC)=2*H(JC)+H(JC)	8AT20158
160.		IF (H(JC) 270,270,285	8AT20159
161.	270	IF (H(JC) 275,275,290	8AT20160
162.	275	DOFF=0	8AT20161
163.		FFJ=1.0	8AT20162
164.		GO TO 285	8AT20163
165.	280	H(JC)=H(JC)+H(JC)-FF(J)	8AT20164
166.	285	GO 290 H(JC)+5	8AT20165
167.		TC=TC(H(JC)	8AT20166
168.		VA=VA+H(JC)-2)*H(JC)	8AT20167

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169. IF (KAT(K1)-99) 260,305,290
170. IF (K0(F1) 305,306,295
171. VA=VA+V*VF(J)*VF(J,I - 2) + G*VF(I - 2) * u(J)
172. VF(I - 2)=VF(I - 2)-VA
173. ACSV=ACSV(VA)
174. VA=VA+P*VF(I - 2)*VF(J)
175. GO TO 310
176. VF=VA+VF(J)
177. VA=VA+VA*VF
178. VF(I - 2)=VF(I - 2)-VA
179. ACSV=ACSV(VA)
180. VA=VA+SL*VF(I - 2)*VF(J)+P*VF(I - 2)
181. GO TO 310
182. VF(I - 2)=VF(I - 2)-VA
183. ACSV=ACSV(VA)
184. IF (ACSV - FUL(I - 2)) 320,320,315
185. I=I+1
186. IF (ACSV - FUL(I - 2)) 330,330,325
187. IF (ACSV(VI) - FUL(I - 2)) 340,340,330
188. FUL(I - 2)=ACSV
189. I=I - 2=IF
190. DO 345 K=1,ISF2
191. A(T,K)=A(T,K)+V*VF(J,K - 2)
192. P(T)=P(T)-V*VF(J)
193. A(T,1)=A(T,1)-V*VF(J)
194. A(T,1)=A(T,1)+VF(J)*FNU(I - 2)
195. CTIME=CTIME
196. IF (IC) 375,375,345
197. FP=FP-VF(I)
198. IF(J)=1
199. F(J)=R(2)-VF(J)*F(J)
200. A(2,1)=A(2,1)-VF(J)*TC(J)
201. IF (MOIE - 2) 370,350,355
202. HOS=H(J)*VF(J)
203. GO TO 360
204. HOS=VF(J)*(SF(J) - 1.9669 * Y(J) - 1.9669)
205. DO 365 I=1,ISF2
206. A(1,1)=HOS*FNU(I - 2)+A(1,1)
207. A(1,2)=A(1,2)-HOS
208. A(1,1)=A(1,1)-HOS*TC(J)
209. P(1)=P(1)-HOS*E(J)
210. CPF=CPF+VF(J)*P(1)
211. IF (FL - FAP) 360,365,345
212. FI=FI+VF
213. J=J+1
214. CONTINUE
215. RETURN
216. FIC

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1. SUPROUTINE MAT3
2. DIMENSION L(10),AR(10)
3.
4. C
5. REAL NFIA(1),NEIB(1),FFIN(1),TAU(10,10)
6. EQUIVALENCE (NFIA(1),A(1)), (NEIB(1),A(5)), (FFIN(1),A(101)),
7. 1(TAU(1),A(151))
8. DIMENSION TF(180),CIJ(180,1)
9. DIMENSION X(1),VLAM(180,1)
10. C
11. COMMON
12. FAKOAA(180),FAMOR(180),RR(180,2),RC(180,2),
13. RO(180,2),PE(180,2),RE(180,2),TU(180,2),VP(180),
14. Y(180),WTM(180),VNU(180,10),FF(180),IFC(180),
15. IP(180),CP(180),H(180),SR(180),TC(180),VLAK(180),
16. E(180),LAHI(180),GAPK(1,1)
17. C
18. COMMON /PARAM1/ KIN,KOUT,JAN,MOL,NAR,IDC,M,KKX(3),KP(10),TILE(3),
19. TTMIN,TTMAX,VISC,PR(1)
20. C
21. COMMON /PARAM2/ WM,SCH,RHO,VEL,R1,NFF,FFA,IS,ISP,P,T,SIF,HIP,
22. EL,ENL,FLIO,HG,IFL,ISPG,KRALP,CPE,TRE,TER,AA,ITS,
23. IM,IL,IT,MODE,HMELT,SMELT,TMAX,TMIN,MELT,SUMN,
24. SUML,JC,HG,CPE,SVA,SVC,SVD,SUMC,NXC,SA1,
25. VACH,KRZ2,SP1,GAN,THJ,NX,NMCHI,HCH,NCV,TRT,
26. IERZ,MQAT,SR1,IXG,SV1,KKJ,IXC,NXG,SH1,NOATO,
27. SAP,FFE,NS,RV,CPE,VA,HOS,DUM1,DUM2,EP,IFCJC,
28. ISP2,WTG,VNU2,WTL
29. C
30. COMMON /ARAYS/ A(16,16),H(16),K(3),VC(50),XE(50),7KE(10),
31. TLO(10),DFCLO(10),NALJP(10),FRI(10),ALPI(10),
32. GAPH(10),GAPK(10),TG(10,3),TK(10,3),WAT(10),
33. IP(10),IGAT(10),KAT(10),UF(10,16),FRL(10)
34. EQUIVALENCE (U(16),TF(1)), (VNU(1),CIJ(1))
35. C
36. COMMON /KINETX/ MT,FKE(50),FAK(50),FVK(50),PMU(10,50),PMU(10,50),
37. PWP(50),PKKK(50)
38. C
39. EQUIVALENCE (P(1),X(1)), (GAPK(1),VLAM(1))
40. C
41. COMMON /DIEFFH/ IR(11),FRU(10),PLUS(10),SLAM(10),PE(10),MY(10),
42. IRC(10),JU(11),SLR(16),SLA(16,16)
43. C
44. ISP3=IS+3
45. IF (MODE - 2) 50,5,25
46. CPA=CPPE+T
47. SUMLT=HFFIT*VH(FEIT)
48. FHS=AA*HID+A(1,2)
49. IF (KKJ+1) 26,10,20
50. DUM1=SVH/AA*T+T
51. FHS=AA*SVH-DUM1+A(1,2)
52. HIP=-A(1,2)/AA
53. A(1,2)=-AA*SVH-DUM1
54. CPA=(CPE + 2. * EUP1 / T)*T
55. DUM2=SVH/AA*T
56. PPE=EP

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*COR
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112. DO 160 IF=TSF3,JSPG
113. IV=IV+1
114. IF (IV - 1) 140,140,120
115. C REDUCE NEW ROW BY PREVIOUS ROWS
116. DO 135 J=2,IV
117. K=I(J - 1)
118. OTV=ATF(K + 2)
119. IF (OTV) 125,135,125
120. ATF(K + 2)=0.
121. JP=J+ISP
122. DO 130 K=3,ISP2
123. ATF(K)=ATF(K)+OTV*ATF(K)
124. CONTINUE
125. C SECK VALID NOT-2E00 ELEMENT
126. DO 150 J=IV,IS
127. K=I(J)
128. IF (ABS(ATF(K + 2)) - .01) 150,150,145
129. IF (IFC(K)) 153,155,150
130. CONTINUE
131. C SINGULAR CONDENSED SET
132. GO TO 165
133. I(J)=I(IV)
134. I(IV)=K
135. OTV=ATF(K + 2)
136. ATF(K + 2)=1.
137. C NORMALIZE NEW ROW
138. DO 160 J=3,ISP2
139. ATF(J)=ATF(J)/IV
140. C COMPLETES FLJOR LOOP=NON SINGULAR
141. GO TO 85
142. C EXTRACT COEFFICIENTS ON SINGULAR SET=POORASE
143. DO 170 J=2,IV
144. K=I(J - 1)
145. AR(J - 1)=ATF(K + 2)
146. AR(IV)=1.
147. C EXTRACT COEFFICIENTS ON SINGULAR SET - BASE
148. DO 185 K=1,IS
149. IF (IFC(K)) 185,185,175
150. IF (ABS(ATF(K + 2)) - .01) 185,185,180
151. IV=IV+1
152. AR(IV)=ATF(K + 2)
153. J(IV)=K
154. CONTINUE
155. C ISOLATE NEW CONDENSED CANDIDATE
156. DO 195 J=1,IV
157. K=J(J)
158. IF (VA(K)) 190,190,195
159. JZ=J
160. KZEK
161. GO TO 200
162. CONTINUE
163. STOP
164. C WHO MUST GO TO ALLOW ENTRY OF NEW CANDIDATE
165. TEST=-1.0F10
166. JX=0
167. DO 220 J=1,IV
168. IF (ABS(ATF(J))-.01) 220,220,205

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169. 205 DUM1=AR(J2)/AR(J)
170. IF (DUM1) 210,220,220
171. K=J(J)
172. DUM1=DUM1+VN(K)
173. IF (DUM1 - TEST) 220,220,215
174. TEST=DUM1
175. JX=J
176. KX=K
177. CONTINUE
178. IF (AR(JX) .NE. 0.0) TEST=VN(KX)/AR(JX)
179. IF (AR(JX) .EQ. 0.0) TEST=0.0
180. C DOES NEW CANDIDATE ENTER
181. IF (E(K2) - E(KX)) 85,85,225
182. C YES
183. 225 GO TO 230 J=J+1
184. K=J(J)
185. VN(K)=VN(K)-TEST*AR(J)
186. KR(7)=KR(7)+1
187. VN(KX)=0.
188. KZ=KX
189. JZ=JX
190. GO TO A5
191. C FLTMINATE TERMS CORRESPONDING TO PRESENT RASF CONDENSED
192. DO 250 K=1,IS
193. IF (IFC(K)) 250,250,240
194. 240 GO 245 IE=ISP3,ISP4
195. 245 A(IE,K + 2)=0.
196. CONTINUE
197. IF (J2) 270,270,255
198. C FLY MATRIX TO YIELD SMALL NEG CORRECTION ON ELIMINATED SPECIES
199. IF (KX - IS) 265,265,260
200. KZ=JZ+IS
201. A(KZ + 2,KZ + 2)=1.E+15
202. R(KZ + 2)=-1.E+10
203. CONTINUE
204. R(2)=EP+R(2)
205. IF (MODF - 1) 310,290,280
206. IF (ABS(EHS / A(1,1)) - .0001) 310,310,320
207. 285 IF (ABS(R(1)) - 1.E - 4) 310,310,320
208. IF (IFCJC) 295,285,305
209. 295 IF (JC - TRJ) 305,305,300
210. GO TO 285
211. MODE=0
212. TMIN=TTSL
213. TMAX=TTMAX
214. GO TO 285
215. 310 IF (FI - 1.E - 4) 315,315,320
216. 315 IF (FOL - 1.E - 5) 335,335,320
217. 320 IV=ISP2
218. IL=1
219. IF (MODE) 325,325,330
220. 325 IF=ISP2-1
221. IL=2
222. X(1)=0.
223. RETURN
224. 335 IF (MY(9)) 340,340,330
225. 340 TKE=-2

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'A130225
'A130226

GO TO 30
END

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227.

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1. SUBROUTINE PROPS
2. DIMENSION T(1), RHO(1), CPM(1), SC(1), CAPC(1)
3. DIMENSION ZA(10), ZT(10), VK(10), VI(10)
4. COMMON/ACF1/GAMPX,REFP,PCF,ACHSQ,SCMAY,SXF
5.
6. REAL A(1),REFP(1),FFTN(1),TAU(10,10)
7. EQUIVALENCE (DEFIA(1),A(1)), (DEFI(1),A(5)), (DEFI(1),A(10)),
8. 1(TAU(1),A(10))
9. DIMENSION TE(10),CTJ(10,1)
10. DIMENSION X(1),VLN(10,1)
11.
12. COMMON FFA(0A(10)),FA(0A(10)),RE(10,2),RC(10,2),
13. 1 RC(10,2),DE(10,2),SC(10,2),TO(10,2),VM(10),
14. 2 Y(10),VTH(10),VMH(10),FF(10),IFC(10),
15. 3 IP(10),CP(10),H(10),SC(10),TC(10),VLN(10),
16. 4 F(10),LMT(10),GAMP(1,1)
17.
18. COMMON /PAE/RI/ KTH,KOUT,JAN,MOL,NAR,IDC,N,KKX(3),KE(10),TILF(3),
19. 1 TTMIN,TTMAX,VISC,PR(1)
20.
21. COMMON /PAS/2/ WM,SCM,RHO,VEL,R1,REF,FEA,TS,ISP,P,1,SIP,MIP,
22. 1 FL,ENL,FLIQ,0,IEL,ISP,G,KFALP,CPE,IFE,IER,AA,TTT,
23. 2 IM,IL,IT,MOFE,MPFEL,SUEL,TAAX,TMID,MELT,SOMA,
24. 3 SMC,JP,HG,CPG,SVA,SVC,SVD,SUMC,FXC,SAT,
25. 4 VMACH,KOZZ,SP1,GA,TH,DX,DNCHI,HCH,KCV,TH,
26. 5 IFZ,MGAT,CR1,IXG,SV1,PKJ,IXC,MKG,SH1,MGATG,
27. 6 S2,FFE,VS,RV,CNF,VA,HOS,DIMP1,DIMP2,EP,IFCJC,
28. 7 ISP2,ATG,VNU2,ATL
29.
30. COMMON /APRAYS/ A(16,16),P(16),W(3),XC(50),XG(50),ZKE(10),
31. 1 T(10),DPCLO(10),UAL,P(10),FR(10),ALP(10),
32. 2 GAVH(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
33. 3 IR(10),IOAT(10),KAT(10),UM(10,10),FBL(10)
34. EQUIVALENCE (NUCI(1),TE(1)), (VNU(1),CIJ(1))
35.
36. COMMON /MTFEX/ MT,FKE(50),FAK(50),FKK(50),PRU(10,50),PMU(10,50),
37. 1 PMR(50),PKKK(50)
38.
39. EQUIVALENCE (P(1),X(1)), (GAMP(1),VIAP(1))
40.
41. COMMON /DIFFER/ IR(11),FRU(10),PRUS(10),SLAM(10),RE(10),RY(10),
42. 1 IPC(10),JU(10),SLB(16),SLA(16,16)
43.
44. ALF=A(2,1)/A(1,1)
45. CSP=1./A(1,1)*AA
46. IF (MODE - 3) 5,10,5
47. CSP=CSP/T
48. RETAS=*(A(2,2) - A(1,2) / A(1,1) * A(2,1))-1.
49. GAMP=1.-MIF
50. GAMP=1./11.*RETA-1.9869/AA*GAMP/CSP*GAMP*P
51. IF (KR(5)) 15,20,15
52. GAMP=GAMP
53. ITS=-1
54. HMY=0.

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55. CAPC(1)=1.
56. I1=1
57. WM=AA/P
58. IS=IS-1
59. TT(1)=T*1.8
60. RHO(1)=AA/(1.3146 * T)
61. CBRK(1)=CPF
62. ASTR=1.15
63. FORM NECESSARY SUMMATIONS
64. PKU2=0.
65. CPTL=0.
66. HTL=0.
67. HTZ=0.
68. PKU2=0.
69. PKU1=0.
70. TKU3=0.
71. CGG=0.
72. CGGPR=0.
73. IER=0
74. IF=0
75. DO 55 K=1,15
76. VK(K)=0.
77. ZK(K)=0.
78. IF (WAT(K)-0.1) 25,30,30
79. IF=K
80. IF (IFC(K)) 35,40,45
81. IF (KR(6)) 40,55,55
82. IF (WTK(K)-0.1) 50,50,45
83. 2K(K)=VN(W)/EF(K)
84. VK(K)=VN(W)
85. CONTINUE
86. I=1
87. DO 85 IK=1,N
88. IF (WTK(I)-0.1) 60,75,75
89. IER=IK
90. ME=H(I)
91. WTE=VTK(I)
92. CPE=CP(I)
93. H(I)=0.
94. WTK(I)=0.
95. CPT(I)=0.
96. IF (IA-IS) 85,85,65
97. DO 70 K=1,15
98. VK(K)=VK(W)+V(I)*V(W)(T,K)
99. GO TO 85
100. IF (IFC(I)) 85,80,85
101. PKU1=PKU1+V(I)*EF(I)**(1./6/MEX)
102. I=I+1
103. VKU1=PKU1/P
104. PKU6=0.
105. WU2=1.385
106. WD2=1.2*ASTR/PKU1
107. WD7=WD7/PKU1-PK2
108. WKU=0.284*WU2
109. WU5=0.32*WU1STH/PKU1
110. WD9=WD9/PKU1+0.5
111.

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112. I=1
113. DO 165 I=1,N
114. IF (IFC(I)) 165,95,90
115. 90 IF (K0(6)) 95,165,165
116. 95 IF (WTM(I)-0.1) 165,100,100
117. 100 VA=VN(I)/EFF(I)
118. IF (IFR) 130,150,105
119. IF (IK-IS) 110,110,115
120. 110 CEJ=CTJ(1F,1)
121. GO TO 125
122. 115 CFJ=0.
123. DO 120 K=1,IS
124. CEJ=CEJ+VN(I)*CTJ(IF,K)
125. HTI=HTI-CEJ*HE
126. CP(I)=CP(I)-CEJ*CPH
127. WT(I)=WT(I)-CEJ*WTE
128. VC=VA*HT(I)
129. P*G2=PHI2+VH
130. HT2=HT2+VA*HT(I)
131. IF (IK-IS) 145,145,135
132. 135 DO 140 K=1,IS
133. VK(K)=VK(K)+VN(I)*VNU(I,K)
134. 140 ZK(K)=ZK(K)+VA*VNU(I,K)
135. 145 FFT=FF(I)
136. IF (IFC(I)) 155,150,155
137. 150 FFT=FF(I)*(1./68*FX)
138. 155 VA=VN(I)/EFF
139. VU=VA*WU(I)
140. VC=VN(I)*EFF
141. PH2=PH2+VH
142. T*U3=T*U3+VA
143. CFTL=VA*CP(I)+CFTL
144. WTL=HTL+VA*HT(I)
145. CPG=CPG+VN(I)*CP(I)
146. H*U5=H*U5+VN(I)*H(I)
147. A*U5=A*U5+VA/(PH2 -VC * WU7 )
148. P*U6=P*U6+VA/(U4 -VC * X*U6 )
149. IF (IFC(I)) 165,160,165
150. 160 CPGH=CPGH+VN(I)*CP(I)
151. 165 T=1+1
152. V*U5=A*U5/AA
153. V*U6=(PH2 + CFTL / 1.9860 - 2.5 * T*U3)/P
154. PH2=PH2/P
155. V*U3=T*U3/P*U2
156. HT=HT/P*U2*1.P
157. DO 170 K=1,IS
158. VK(K)=VK(K)/AA*WU(K)
159. ZK(K)=ZK(K)/PH2*WU(K)
160. 170 DO 175 I=1,IS
161. 175 ZT(I)=0.
162. VT(I)=0.
163. DO 175 K=1,IS
164. VT(I)=VT(I)+CTJ(K,T)*VK(K)/WTM(K)*NAT(I)
165. 175 ZI(I)=ZI(I)+CTJ(K,T)*ZK(K)/WTM(K)*NAT(I)
166. CPG=CPG/AA
167. CPH=CPH/AF
168. H*U5=H*U5/AA

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*COR
*COR
*COR
*COR
*COF
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PK0P0221
PK0P0222

1 . . 9H (CA4FA =Ff.3.1H)/1X10(4XI3.5X1)
END

226.
227.


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1. SUBROUTINE SCALF (NCE)
2. DIMENSION CDEF(130)
3. DIMENSION PV(1),PVX(130,3)
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55.      TRC(J)=TRC(J - 1)
56.      TRC(J - 1)=JA
57.      K=1
58.      GO TO 20
59.      IR(J)=1000
60.      CONTINUE
61.      IF (K) 25,25,5
62.      TRC(J5 + 1)=10000
63.      M=TRC(J)
64.      M1=1
65.      L=TS+2
66.      L=0
67.      LL=1
68.      LIP=M+K*(2)
69.      DO 240 IK=1,LL
70.      I=1+1
71.      IF (IK - IS) 30,30,45
72.      SLAN(I)=0.
73.      TRC(I)=IFC(I)
74.      PMS(I)=0.
75.      IF (IK(I) - 1) 35,35,75
76.      DYI=X(I + 2)
77.      IF (IFC(I) + 1) 275,40,40
78.      IF (IFC(I)) 205,95,230
79.      IF (IFC(I) + 1) 75,50,50
80.      IF (IFC(I)) 70,55,45
81.      VA=E(I)-TC(I)*Y(I)
82.      DO 65 J=1,JS
83.      IF (IRC(J)) 60,60,65
84.      VA=VA+VNU(I,J)*X(J + 2)
85.      CONTINUE
86.      DYI=VA
87.      GO TO 95
88.      IF (IK - TRE) 75,60,75
89.      DYI=0.
90.      GO TO 275
91.      IFC(I)=1
92.      DYI=X(IER)
93.      GO TO 230
94.      I=I+1
95.      IF (L - IER) 90,85,90
96.      DYI=X(I)
97.      GO TO 230
98.      DATG=D+TR+VN(I)*DYI*WTM(I)
99.      IF (IP(I)) 100,195,100
100.      IF (IK - N) 105,145,105
101.      IF (VN(I) - NUMP) 110,140,140
102.      IF (NOF) 195,195,115
103.      IF (DYI) 120,275,125
104.      IF (VN(I) / RUMP - .9999995 - CMF * DYI) 275,275,130
105.      IF (RUMP / VN(I) - 1. - CMF * DYI) 135,275,275
106.      CMF=(VN(I) / RUMP - .9999995)/DYI
107.      GO TO 275
108.      CMF=(RUMP / VN(I) - 1.)/DYI
109.      GO TO 275
110.      IF (NOF) 175,175,150
111.      M1=M1+1

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112. M=IR(MI)
113. IF (DYI) 155,275,160
114. IF (DYI * CMF + .999) 165,275,275
115. IF (DYI * CMF - 9.) 275,275,170
116. CMF=-.999/DYI
117. GO TO 275
118. CMF=9./DYI
119. GO TO 275
120. IF (DYI * CMF - 2.303) 180,190,190
121. IF (DYI * CMF + 6.909) 185,275,275
122. CMF=-6.909/DYI
123. GO TO 275
124. CMF=2.303/DYI
125. GO TO 275
126. IF (Y(I) - RULP + ARS(DYI) * CMF) 275,200,200
127. CMF=-Y(I) - RULP/ARS(DYI)
128. GO TO 275
129. NON-PRESENT BASE
130. IF (KR(6)) 215,210,210
131. IF (T - TE(I) + .001) 275,215,215
132. IF (Y(I) + CMF * DYI - 0.1) 275,220,220
133. DUM1=(.1 - Y(I))/DYI
134. IF (DUM1 - .001) 275,275,225
135. CMF=DUM1
136. GO TO 275
137. DWTL=DWTL+DYI*WTF(I)
138. IF (DYI) 235,275,250
139. IF (VNI) 250,250,240
140. IF (VNI) + DYI * CMF) 245,250,250
141. CMF=-VNI/DYI+1.00001
142. IF (KR(6)) 265,255,255
143. CLIP=ARS(CLIP/WTF(I))
144. IF (ARS(CMF * DYI) - CLIP) 275,275,260
145. CMF=CLIP/ARS(DYI)
146. GO TO 275
147. IF (ARS(CMF * DYI) - P) 275,275,270
148. CMF=P/ARS(DYI)
149. CMF(I)=CMF
150. DY(IK)=DYI
151. IF (KR(6)) 290,285,285
152. RUL=ARMAX(.1,RV/2.)
153. CMF=ARMAX(CMF,RUL) / ARS(ABS(DWTL - DWTG / WTE * WTL) / RVL - DWTG)
154. IF (KR(7)-1) 300,300,295
155. NO=1
156. WRITE (KOUT,350) (FARNG(J),VNI(J),Y(J),DYA(J,LL),CMFF(J),F(J),IFC(J),J=1,NO)
157. IF (J=1,NO)
158. WRITE (KOUT,360) (FR(I),I=1,IS)
159. WRITE (KOUT,360) (X(I),I=1,IS)
160. WRITE (KOUT,355) (TRIT),I=1,IS)
161. CONTINUE
162. IF (X(I)) 305,345,305
163. X1=X(I)*C*F
164. ARX=ARS(X(I))
165. IF (ARS(X1) - .5) 315,315,310
166. CMF=.5/ARY
167. X1=CMF*X(I)
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169. 315 IF (X1) 325,345,320
170. 320 TP=TMAX
171. X1=ATM1(.2,X1)
172. GO TO 330
173. 325 TP=TM10
174. X1=AMAX1(-0.2,X1)
175. 330 OTR=(TM - T)/(TP * X1)
176. IF (OTR - 1.) 335,340,340
177. 335 CPE=OTR*C-F
178. T=TP
179. GO TO 345
180. T=T/(1. - X1)
181. 345 AA=AA*EXP(CMF * X(2))
182. RETURN
183. C
184. -350 FORMAT (1X2(1X2H0.9X1HY8Y2H0Y7X5HSCAL E7X1)H4X5H1FC 1P)/(1X40,5E
185. 1 10.3,13.12,1X,44,5E10.3,13,12))
186. 355 FORMAT (10I5)
187. 360 FORMAT (8F12.4)
188. END
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SECTION 3

SAMPLE PROBLEMS

Presented in this section are three sample problems which were run on a Univac 1108 digital computer. An attempt was made to utilize almost all of the options available in the GASKET2 program. For each sample problem, the following is presented:

- A brief description of the nature of the problem and solution
- A listing of the input data deck
- A few typical pages of the program output

Sample Problem 1

In this problem, ablation rates at the throat of a rocket nozzle are calculated. The propellant gases are comprised of seven elements, including both hydrogen and oxygen. The surface material option of ATJ bulk graphite is used. The program options which utilize built-in physical data are selected; hence, only 10 cards of input data are required for the complete sequence of calculations. The ideal chamber conditions (propellant flame temperature of 3764°K, ideal pressure of 68.02 atm) are input. After redefining the elemental set to include the fictitious element "GRAPHITE," subsequent calculations performed by the program include determination of the actual chamber state (54.42 atm) and an isentropic expansion to the throat (unity Mach no.). The frozen edge state is computed for the built-in array of eight temperatures, and the surface ablation rate is computed for the built-in array of fifteen surface temperatures.

Listing of Input

1.	3005110600	3764.	54.42	-1.0	68.02	0.969	0.
2.	7						
3.	1	HYDROGEN	1.008	3.3192			
4.	4	BERYLLIUM	9.012	1.4265			
5.	6	CARBON	12.011	0.9236		1.0	
6.	7	NITROGEN	14.007	0.8342			
7.	8	OXYGEN	16.0	1.9161			
8.	9	FLUORINE	19.0	0.8680			
9.	17	CHLORINE	35.453	0.4012			
10.	8						

Sample Problem 1 Output

GRAPHITE SURFACE KINETICS (GASKET) PROG. 1

0110000+00

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00500	.0330797	.0000000
4	BERYLLIUM	9.01200	.0142129	.0000000
6	CARBON	12.01100	.0092023	.0000000
7	NITROGEN	14.00700	.0063215	.0000000
8	OXYGEN	16.00000	.0190910	.0000000
9	FLUORINE	19.00000	.0086483	.0000000
17	CHLORINE	35.45300	.0039973	.0000000
106	GRAPHITE	12.01100	.0000000	.0032570

ELEMENTS	HYDROGEN	BERYLLIUM	CARBON	NITROGEN	OXYGEN
	FLUORINE	CHLORINE	GRAPHITE		

BASE SPECIES	H2	BE	CO2	CCLH	H2O
	PH	CLH	C*		

Sample Problem 1 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROB. 1

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DLNW/DLNT	DLNW/DLNP	GAMMA
.49545+00	.12580+01	-.57602+00	.35229-01	.11334+01

PROPERTY ROUTINE OUTPUT IN

TEMP	VISS	COND	DBAR	PR	SC
.67752+04	.61615-04	.75106-04	.23259-03	.51461+00	.72427+00
MU1	MU2	POL.WT	HTIL	CPTIL	HTIL*
.77603+00	.20648+02	.25599+02	.42582+04	.86999+00	.23444+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER (GAMEX = .667)

1	4	6	7	9	17	104
.33335-01	.12809+00	.11053+00	.11656+00	.30546+00	.16432+00	.00000
.89675-01	.69022-01	.13622+00	.14390+00	.23111+00	.14498+00	.00000

SOLUTION TIMES

ITERATIONS = 32

TIME = 9.2A7 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS =	.21215+00
TEMP = 6775.2000 DEG R.	= 3764.0000 DEG K.
PRESS =	68.02000 ATM

ENTHALPY - BTU/LRM	GAS	CONDENSED	COMPOSITE
ENTROPY - BTU/LRM DEG R	.24931+03	-.54624+04	-.78736+03
DENSITY - LRM/FT3	.24060+01	.15349+01	.25855+01
MOLECULAR WEIGHT	.29030+00	.35189+00	.35189+00
	21.1144	25.0120	25.5946

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.28681-02	H2	.51374+00	H2O	.52155-01	CO	.00000
FM	.26427-01	BE	.37865-02	CCL4	.85119-07	C2H2	.31456-07
C	.12442-04	C2	.66064-10	C3	.21189-12	C4	.84802-18
C2BE	.74619-09	HECL	.37108-02	HECLF	.36218-01	3ECL2	.82985-02
REF2	.40610-01	HEMO	.66279-02	HEM2	.19498-03	3EH2O2	.36210-02
BE2CL4	.35445-07	HE2O2	.27032-03	HE3O3	.24759-03	HE4O4	.85633-04
BE6O6	.20125-06	CCL	.36754-08	CCLF0	.54481-09	CCLF3	.79560-17
CCL3F	.43880-17	CCL4	.12540-17	CF	.21456-07	CF4	.44796-08
CF2O	.42082-09	CF3	.70361-14	CF4	.41132-17	CH	.10493-06
CHCL2F	.86493-14	CHCL3	.47047-14	CHFO	.79573-07	CHF3	.44654-14
CHNO	.95549-06	CHO	.45571-04	CH2	.57441-07	CH2CLF	.24644-11
CH2F2	.10232-11	CH2O	.27401-05	CH3	.44354-06	CH3CL	.10870-08
CH4	.97096-07	CN	.24543-05	C2F2	.14879-15	C2F4	.28364-22
C2H4O	.19663-14	C2H2	.24440-09	C3O2	.41003-10	C4H2	.75546-17
CLF	.84849-07	CLF03	.60026-24	CLF3	.87612-21	CLH0	.17413-05
ClO	.15244-05	ClO2	.89297-11	CL2O	.85230-11	F	.11110-03
FN	.68111-08	FNO	.10759-08	FO	.39131-08	F2O	.52961-15
H	.69679-01	HN	.40321-04	HO	.38114-02	H2N	.24586-04
H3N	.18218-04	HNP2	.45197-11	N	.27902-04	NO	.36568-03
N2O	.58770-07	N2O3	.10572-15	N2O4	.28330-21	N2O5	.17632-25
O3	.22818-11	CCL2F2	.72649-17	CCL0	.51757-05	CF0	.14886-06
FN02	.41704-14	CLN02	.41138-13	F2N	.62872-13	FN03	.19497-20
BEH	.17145-04	HN02	.20359-08	HN03	.18560-13	RE2O	.10682-02
HO2	.12061-06	NO3	.47587-14	CF4O	.84379-23	CCL2	.82626-10
F2N2	.42902-17	H2N2	.28486-08	RE2F2O	.17103-01	CH2	.84652-09
CLF5	.11751-36	BEH	.65441-15	FO2	.24159-11	C2H	.12570-07
C2CL4	.12864-20	C2CL6	.28053-30	C2HF	.67411-11	C2CL2	.17562-12
CHCL	.40746-08	CHF	.35408-08	C2F3N	.17697-19	F3N0	.16489-24
CL2	.30746-05	N2	.10623+00	O2	.14642-04	CNO	.14911-06
C2H3	.71395-10	C2H6	.84166-14	C3H	.61907-11	C3H2	.56004-12
C3H4	.45045-14	C3H5	.20283-13	C4H	.34384-14	C4H2	.57922-15
CL4HNO4	.00000	HEW2O2	.00000	HE*	.00000	HEO*	.17912+00
BE3N2*	.00000	BECL2*	.00000	HEF2*	.00000		

Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROP. 1      2000200+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLNM/DLNT      DLNM/DLNP      GAMMA
.49506+00      .13039+01      -.60504+00      .36699-01      .11327+01

PROPERTY ROUTINE OUTPUT IN LB-MASS,FT,SEC,RTU,AND DEG-R
TEMP      VISC      COND      DBAR      PR      SC
.67212+04      .61287-04      .74620-04      .28689-03      .31494+00      .72426+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.77499+00      .20619+02      .25514+02      .43013+04      .A6896+00      .24063+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      2      3      4      5      6      7      8      9      10      11      12      13      14      15      16      17      18      19      20
.33335-01      .12809+00      .11053+00      .11656+00      .30546+00      .16432+00      .14172+00      .00000
.89982-01      .69338-01      .13601+00      .1436A+00      .23836+00      .17807+00      .14496+00      .00000

SOLUTION TIMES
ITERATIONS = 3      TIME = 1.249 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MARS GAS = .21195+00
TEMP = 6721.2491 DEG R. = 3734.0273 DEG K.      PRESS = 54.42000 ATM

ENTHALPY - BTU/LBM      GAS      CONDENSED      COMPOSITE
.29254+03      -.58969+04      -.78736+03
ENTROPY - BTU/LBM DEG R      .2A272+01      .15297+01      .26009+01
DENSITY - LBM/FT3      .23351+00      .282A6+00      .25.5143
MOLECULAR WEIGHT      21.0627      25.0120      25.5143

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES)....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
C02      .291A3-02      H2      .31040+00      H2O      .32357-01      C*      .00000      CLH      .40019-01
FH      .26414-01      BE      .40393-02      CCLN      .67381-07      CO      .23178+00      CLM2      .19219-07
C      .10445-06      C2      .43A31-10      C3      .1154A-12      C4      .35696-18      C5      .31440-21
C2BE      .49368-09      BECL      .37338-02      HECLF      .3572A-01      HECL2      .A1426-02      REF      .44293-01
REF2      .40808-01      REMO      .6727A-02      REM2      .17333-03      REMO4      .375A2-02      REO      .27294-03
RE2CL4      .27308-07      HE2O2      .243A6-03      RE3O3      .27990-03      HE3O5      .35546-05
BE6O6      .23314-06      CCL      .28A17-0A      CCLFO      .46249-09      CCL2O      .19074-09
CCL3F      .269A8-17      CCL4      .770A2-1A      CF      .17226-07      CFH      .33543-0A      CF2      .A9300-10
CF2O      .33469-09      CF3      .47004-14      CF4      .25784-17      CH      .A1195-07      CHCLF2      .60000-14
CHCL2F      .541A4-14      CHCL3      .29411-14      CHFO      .63030-07      CHF3      .27583-14      CHN      .39842-04
CHNO      .75218-06      CHO      .38831-04      CH2      .42021-07      CH2CLF      .1A030-11      CH2CL2      .23708-11
CH2F2      .643A3-12      CH2O      .21617-05      CH3      .30546-06      CH3CL      .64674-09      CH3F      .14695-09
CH4      .62909-07      CN      .19843-05      C2F2      .10752-15      C2F4      .13399-22      C2H4      .118A0-10
C2HNO      .97335-15      C2N2      .14962-09      C3O2      .25290-10      C4H2      .28097-17      CL      .620A3-02
CLF      .79011-07      CLFO3      .47634-24      CLF3      .58176-21      CLHO      .16440-05      CLNO      .16589-07
CLO      .15549-05      CLO2      .86633-11      CL2O      .76640-11      F      .11359-03      FHO      .12099-07
FN      .59609-0A      FNO      .97331-09      FO      .37407-08      F2O      .43854-15      F3N      .16507-19
H      .73024-01      HN      .36701-04      HO      .40034-02      H2      .25088-04      H2O2      .50087-07
H3N      .14492-04      H4N2      .27351-11      N      .27506-04      NO      .3A019-03      NO2      .94613-0A
N2O      .54463-07      N2O3      .88768-16      N2O4      .22938-21      N2O5      .13586-25      O      .54542-03
O3      .23779-11      CCL2F2      .44727-05      CFC      .12598-06      CF6      .26A43-20
FNO2      .36221-14      CLNO2      .36384-13      F2H      .48535-13      FNO3      .15578-20      HNO      .76643-06
BEN      .15949-04      HNO2      .186A9-0A      HNO3      .14144-13      AF2O      .11155-02      HNO2      .79529-33
MO2      .12141-06      NO3      .44848-14      CF4O      .44198-23      CCL2      .60609-10      CCL3      .10845-13
F2N2      .29146-17      H2N2      .21249-08      HE2F2O      .16646-01      CN2      .63233-09      C2O      .17887-07
CLF5      .55342-37      HEH      .50405-15      FO2      .22464-11      C2H      .A1308-0A      C2N      .60477-09
C2CL4      .62617-21      C2CL6      .10766-30      C2HF      .34A15-11      C2CL2      .10515-12      C2HCL      .92043-10
CHCL      .29571-08      CHF      .26186-0A      C2F3H      .A5421-20      F3HO      .11A94-24      F2      .27915-10
CL2      .29698-05      N2      .10589+00      O2      .22352-04      CNO      .12322-06      N3      .66642-09
C2H3      .38503-10      Z2H6      .34929-14      C3H      .31964-11      C3H2      .26160-12      C3H3      .42033-13
C3H4      .17873-14      C3H5      .72244-14      C4H      .15952-14      C4H2      .21827-15      CLH4H*      .00000
CLH4NO4*      .00000      BEH2O2*      .00000      HE*      .00000      9EO*      .17798+00      CRE2*      .00000
RE3N2*      .00000      BECL2*      .00000      REF2*      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASNET) PROBL 1      5000100+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN  CP-EQUIL  DLNM/DLNT  DLNM/DLNP  GAMMA
.49587+00  .12511+01  -.54367+00  .31434+01  .11302+01

PROPERTY ROUTINE OUTPUT IN  LH=MASS,FT,SEC+RTU,ATM  OFG=R      SC
TEMP      .63793+04  .59220+04  .72322+04  .49482+03  .39575+00  .72433+00
MU1       .77413+00  .20594+02  .25606+02  .3A464+04  .A7149+00  .20679+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . . (GAMEX = .667)
      1      4      6      7      8      9      17      106
      .33335-01  .12809+00  .11053+00  .11656+00  .30866+00  .16432+00  .14172+00  .00000
      .91019-01  .65809-01  .13771+00  .14546+00  .23345+00  .17956+00  .14659+00  .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = 2.331 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .22523+00
TEMP = 6379.3015 OFG M. = 3544.0564 OFG M.  PRESS = 31.47837 ATM

ENTHALPY - RTU/LHM      GAS      CONDENSED      COMPOSITE
.72630+02      -.61156+04      -.10649+04
ENTROPY - RTU/LHM DEG K  .29496+01      .14963+01      .26004+01
DENSITY - LBM/FT3      .14230+00      .25.0120      .17436+00
MOLECULAR WEIGHT      21.0621      25.0120      25.8059

ABOVE ARE STATIC PROPERTIES      K-KINETIC = .27759+03 HTU/LHM
VEL. = .372A+04 FT/SEC  FLUX = .84496+03 LHM/FT2SEC  MACH = 1.00004

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.
C02      .27318-02  H2       .32262+00  H2O      .30764+01  C#       .00000      CLW      .41191+01
FH       .26684+01  HE       .29799+02  CCLM     .36403+07  CO       .23449+00  C#H2     .84514+08
C        .49832-07  C2       .12001-10  C#       .24174+13  C#       .51448+19  C#       .36000+22
C#RE     .16436-09  HECL     .28715+02  HECLF    .37215+01  HECL2    .81873-02  HEF      .38901+01
HFF2     .44390-01  HEHO     .48529+02  HEH2     .10469+03  HEH2O2   .30026-02  HEU      .16674-03
HE2CL4   .15897-07  HE2C2    .19662+03  HF303    .24291+03  HE404    .88306+04  BE505    .33307+05
RE606    .23615-06  CCL      .11200+08  CCLF0    .25637+09  CCLF3    .14808+17  CCL20    .94859+10
CCL3F    .75742-18  CCL4     .21567+18  CF       .15868+08  CF       .37747+10  CF2      .20543+14
CF20     .17744+09  CF3      .10443+14  CF4      .82064+18  CH       .51811+07  CHCLF2   .20543+14
CHCL2F   .18370-14  CHCL3    .10163+14  CHEF0    .35444+07  CHE3     .94948+15  CHN      .26279+04
CHNO     .43530+06  CHO      .23341+04  CH2      .18336+07  CH2CLF   .71700+12  CH2CL2   .98335+12
CH2F2    .25524-12  CH2O     .13182+05  CH3      .15837+06  CH3CL    .34490+09  CH3F     .67572+10
CH4      .36865-07  CN       .10136+05  C2F2     .25193+16  C2F4     .21301+23  C2H4     .44985+11
C2H4N    .25111-15  C2N2     .57503+10  C3O2     .41461+11  CH2F2    .47399+18  CL       .55665+02
CLF      .44974-07  CLF03    .47909+25  FIF3     .83535+22  CLH0     .99812+06  CLNO     .73927+08
CLO      .84962-06  CLO2     .27124+11  CL20     .27719+11  F       .78547+04  F#O      .55665+08
FN       .23708+08  F#O      .38823+09  FO       .14624+08  F#H      .90912+16  F#O2     .26601+20
H        .65694+01  HN       .20948+04  HO       .29439+02  H2N      .15136+04  H2O2     .22176+04
H3N      .97000+05  H#N2     .81142+12  N        .15777+04  NO       .25032+03  H2O      .39910+08
N2O      .27127+07  N2O3     .14671+14  N2O4     .23465+22  N2U5     .81268+27  O        .35124+03
O3       .62527+12  CCL2F2   .12648+17  E2#      .12414+13  E#O3     .65594+07  C2F6     .28846+31
F#O2     .88244+15  CLN02    .10025+13  E2#      .12414+13  F#O3     .17591+21  H#O      .38449+06
REN      .76398+05  H#N02    .72831+09  H#O3     .39992+14  HE2O     .70420+03  F#N2     .34641+34
H02      .53615-07  H2N2     .99771+15  C#O      .65570+24  CCL2     .28277+10  CCL3     .35788+14
F2N2     .53440+18  H2N2     .48877+09  HE2F20   .15761+03  C#2      .22592+09  C2O      .71904+08
CLF5     .18459+38  HEH      .69606+14  F02      .60519+12  C2#      .31929+08  C2#      .23183+09
C2CL4    .12229+21  C2CL6    .10144+11  C2HF     .13129+11  C2CL2    .34554+13  C#HCL    .36300+10
CHCL     .11644+08  CHF      .10842+04  C2F3#    .16422+20  F3#O     .11447+25  F2       .10375+10
CL2      .21579+05  H2       .10770+00  O2       .13016+04  C#O      .58038+07  H#       .24375+09
C2H3     .12922+10  C2H6     .99422+15  C3#      .97580+12  C3#2     .65852+13  C#H#     .10497+13
C3H#     .43219+15  C3#5     .14449+14  C#H      .30223+15  C#H2     .43396+16  CLH#H#   .00000
CLH#H#H# .00000  EEH2O2#  .00000    HE#      .00000    HE0#     .14966+00  CHE2#    .00000
RESN2#   .00000  HECL2#   .00000    HFF2#    .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROR. 1      00000000000

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLHP/DLHP      DLHP/DLHP      GAMMA
.36603+00      .49852+02      -.43601+01      .49949+01      .99459+00

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT. SEC. RTU. AND DEG-R
TEMP      VISC      COCD      DBAR      PR      SC
.90000+03      .16292-04      .15778-04      .17653-04      .50751+00      .72433+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.77413+00      .20596+02      .25806+02      -.52830+03      .48840+00      -.13648+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      4      6      7      8      9      17      104
.33335-01      .12809+00      .11053+00      .11656+00      .50546+00      .16432+00      .14172+00      .00000
.91019-01      .65809+01      .15771+00      .14544+00      .23385+00      .17954+00      .14659+00      .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = .414 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT
MASS CONDENSED/MASS GAS = .22523+00
TEMP = 900.0000 DEG K. = 500.0000 DEG K.      PRESS = 31.47837 ATM

ENTHALPY - RTU/LHM      GAS      CONDENSED      COMPOSITE
-4.22911+04      -.10178+05      -.37409+04
ENTROPY - RTU/LHM DEG R      .29345+01      .29797+00      .17153+01
DENSITY - LBM/FT3      .10687+01      .12359+01      .12359+01
MOLECULAR WEIGHT      21.0621      25.0120      25.8059

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .2731A-02      H2      .32264+00      H2O      .30265-01      C#      .00000      CLH      .41121-01
C      .26684-01      HE      .29748-02      CLCN      .36303-07      CO      .23469+00      CLH2      .88519-08
C2      .42812-07      C2      .12001-10      C3      .28174-13      C4      .51448-19      C5      .36090-22
C2RE      .16436-09      HECL      .28718-02      HECLF      .37213-01      4ECL2      .81873-02      HEE      .38901-01
REF2      .44390-01      BEHO      .48529-02      FEH2      .10869-03      4F+2O2      .30026-02      REF      .16679-03
REFCL4      .15897-07      HEF2O2      .19662-03      REF3O3      .24291-03      4E+O4      .88306-04      REF5O5      .33307-05
HE6O6      .23615-06      CCL      .11200-08      CCLFO      .25637-09      CCLF3      .14808-17      CCL2O      .94859-10
CCL3F      .78742-18      CCL4      .21869-18      CF      .73674-08      CCF      .15664-08      CF2      .37747-10
CF2O      .17754-09      CF3      .14443-14      CF4      .42068-18      CH      .31811-07      CHCLF2      .20569-14
CHCL2F      .18370-14      CHCL3      .10163-14      CHF3      .35446-07      CH4      .94948-15      CH5      .67572-10
CHNO      .43530-06      CHD      .23341-04      CH2      .18436-07      CH2CLF      .17100-12      CH2CL2      .26279-04
CH2F2      .25524-12      CH2O      .15182-05      CH3      .15837-06      CH3CL      .34490-09      CH3F      .98355-12
CH4      .36865-07      CH      .10136-05      C2F2      .25193-16      C2F4      .21301-23      C2H4      .44993-11
C2H4O      .25131-14      C2H2      .57403-10      C3O2      .91461-11      C4H2      .47399-18      CL      .55665-02
CLF      .44978-07      CLF3      .47909-25      CLF5      .83556-22      CLH2O      .99812-06      CLNO      .73927-08
CLO      .84982-06      CLO2      .27128-11      CL2O      .18429-08      F2O      .78547-04      F3N      .57663-08
FN      .23708-04      FNO      .38823-09      HO      .29434-02      F2O      .78547-04      F3N      .57663-08
H      .65694-01      HN      .20448-04      H      .15777-04      V2O5      .11268-27      C2F6      .24885-31
H3N      .97000-05      H4N2      .81192-12      N      .23865-22      CFO      .65594-07      H4O      .38649-06
N2O      .27127-07      N2O3      .14471-16      N2O4      .12418-13      F2O      .70920-03      F4N2      .34641-34
O3      .62527-12      CCL2F2      .12844-17      F2U      .12418-13      F2O      .70920-03      F4N2      .34641-34
FNO2      .88244-18      CLNO2      .10023-13      HNO3      .49920-14      CCL2      .23277-10      C2H3      .20189-09
BEH      .76398-05      HNO2      .72831-09      HNO3      .49920-14      CCL2      .23277-10      C2H3      .20189-09
H2O      .53845-07      N2O3      .14471-16      H2O      .53845-07      CCL2      .23277-10      C2H3      .20189-09
F2N2      .53840-14      H2N2      .68778-09      F2O      .70920-03      CCL2      .23277-10      C2H3      .20189-09
CLF3      .18449-38      BEH      .69606-16      F2O      .70920-03      CCL2      .23277-10      C2H3      .20189-09
C2CL4      .12224-21      C2CL6      .10169-11      C2H4      .13129-11      C2CL2      .34558-13      C2HCL      .10373-10
CHCL      .11634-08      CHF      .10942-08      C2F3H      .16422-20      F3O      .11447-25      F2      .10373-10
CL2      .21579-05      H2      .10720+00      O2      .13016-04      CNO      .65038-07      N3      .24375-09
C2H3      .12922-10      C2H6      .99522-15      C3H      .92460-12      C3H2      .65852-13      C3H3      .10447-13
C3H4      .43239-15      C3H5      .14499-14      C4H      .30223-15      C4H2      .43396-16      CLH4#      .00000
CLH4#      .00000      BEH2O2#      .00000      H4#      .00000      BEC#      .14966+00      CRE2#      .00000
HEH2#      .00000      BECL2#      .00000      HEF2#      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROC. 1      0003000+00
CP-FROZEN= .36624+00

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, RTU, AND DEG-R
TEMP      VISC      COND      DBAR      PR      SC
.90000+03 .16355-04 .99522+05 .17653-04 .60185+00 .72464+00
MU1       MU2       MOL.WT      HTIL      CPTIL     HTIL*
.94288+00 .25172+02 .26508+02 -.36450+04 .43371+00 -.37859+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      2      3      4      5      6      7      8      9      10
.71313-01 .87637-01 .11139+00 .13714+00 .22999+00 .20646+00 .15608+00 .00000
.91019-01 .65809-01 .13771+00 .14546+00 .23385+00 .17956+00 .14659+00 .00000

SOLUTION TIMES
ITFRATIONS = 34      TIME = 9.753 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS AT: GRAPHITE
MASS TRANSFER COEFFICIENT ROUGH = .96900+00
RHO V WALL/RHOE DE CM = .10000-16      BPRIME = .00000

STATE ADJACENT TO THE SURFACE . . .
TEMP = 900.0000 DEG R = 500.0000 DEG K      PRESS = 31.47837 ATM

      GAS      CONDENSED      COMPOSITE
ENTHALPY - RTU/LBM      -.41003+04      .00000      -.41003+04
ENTROPY - BTU/LBM DEG R      .14084+01      .00000      .00000
DENSITY - LBM/FT3      .12695+01      .00000      .12695+01
MOLECULAR WEIGHT      26.5080      .0000      26.5080

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = BPRIME CONDENSED ) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .23277-07      H2      .56440-01      H2O      .26938+00      C*      .00000      CLH      .11182+00
FH      .27636-03      HE      .00000      CCLN      .75120-27      CO      .34549-10      C2H2      .12954-27
C      .00000      C2      .00000      C3      .00000      C4      .00000      C5      .00000
C2RE      .00000      RECL      .15712-13      HFCLF      .43118-02      RECL2      .28301-03      REF      .72840-27
REF2      .14155+00      REHO      .24712-31      REM2      .97115-34      HFH2O2      .14283-03      REO      .00000
BE2CL4      .10721-08      BE2O2      .00000      RF3O3      .63335-25      RF4O4      .92324-17      RE5O5      .21536-10
BE6O6      .14516-01      CCL      .00000      CCLFO      .67369-25      CCLF3      .00000      CCL2O      .23793-25
CCL3F      .00000      CCL4      .00000      CF      .00000      CFN      .15286-37      CF2      .00000
CF2O      .18187-24      CF3      .00000      CF4      .00000      CH      .00000      CHCLF2      .45249-31
CHCL2F      .22641-30      CHCL3      .27769-28      CHFO      .15428-19      CHF3      .14261-30      CHN      .38271-16
CHNO      .44346-17      CHD      .32711-28      CH2      .00000      CH2CLF      .43060-22      CH2CL2      .31835-18
CH2F2      .64381-24      CH2O      .30833-15      CH3      .14482-19      CH3CL      .76154-09      CH3F      .89693-15
CH4      .24588+00      CN      .00000      C2F2      .00000      C2F4      .00000      C2H4      .32929-15
C2H4O      .13713-30      C2N2      .64819-17      C3O2      .00000      C4N2      .00000      CL      .92420-21
CLF      .21185-36      CLF03      .00000      CLF3      .00000      CLH0      .10898-25      CLN0      .00000
CLO      .00000      CLO2      .00000      CL2O      .00000      F      .14740-37      FHO      .00000
FN      .00000      FO      .00000      FO      .00000      F2O      .00000      F3N      .00000
H      .29398-21      HN      .34121-15      H0      .12689-26      H2N      .54404-20      H2O2      .15944-36
H3N      .42508-01      H4N2      .15408-21      H      .00000      VO      .60951-32      H02      .00000
N2O      .23507-35      N2O3      .00000      N2O4      .00000      N2O5      .00000      O      .00000
O3      .00000      CCL2F2      .00000      CCL0      .36405-27      CF0      .17024-37      C2F6      .00000
FN02      .00000      CLN02      .00000      F2N      .00000      FN03      .00000      HNO      .98354-36
REN      .00000      HN02      .00000      HN03      .00000      RE2O      .00000      F4N2      .00000
H02      .00000      N03      .00000      CF4O      .00000      CCL2      .00000      C2O      .00000
F2N2      .00000      H2N2      .31209-28      BE2F2O      .17438-03      CN2      .00000      C2H      .00000
CLF5      .00000      BE4      .00000      F02      .00000      C2H3      .00000      C2HCL      .24619-36
C2CL4      .00000      C2CL6      .00000      C2HF      .00000      F3N0      .07000      F2      .00000
CHCL      .00000      CHF      .00000      C2F3N      .00000      CNO      .00000      N3      .00000
CL2      .11230-20      N2      .10851+00      O2      .00000      C3H2      .00000      C3H3      .00000
C2H3      .86419-35      C2H6      .20206-06      C3H      .00000      C4H2      .00000
C3H4      .73722-31      C3H5      .28923-26      C4H      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROB. 1      5002000+40
CP-FROZEN= .41587+00

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, ATU, AND DFG-R
TEMP      VISC      COND      DGR      PR      SC
.25200+04 .32185-04 .33969-04 .97419-04 .39403+00 .72449+00
MU1       MU2      MCL.WT  HTIL    CPTIL   HTIL*
.80934+00 .21579+02 .23272+02 -.12491+04 .75158+00 -.17734+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPX = .667)
      1      2      3      4      5      6      7      8      9      10      11      12      13      14      15      16      17      18      19      20
.39722-01 .81106-01 .13133+00 .13745+00 .23048+00 .20404+00 .17147+00 .00000
.90963-01 .65695-01 .13893+00 .14526+00 .23553+00 .17927+00 .14635+00 .00000

SOLUTION TIMES
ITERATIONS = 8      TIME = 5.121 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS ATJ GRAPHITE
MASS TRANSFER COEFFICIENT RHO CM = .96900+00
RHO V WALL/RHOE UE CM = .14042-02      RPRIME = .14042-02

STATE ADJACENT TO THE SURFACE . . .
TEMP = 2420.0000 DEG R = 1400.0000 DEG K      PRESS = 31.47857 ATM

ENTHALPY = BTU/LBM      GAS      CONDENSED      COMPOSITE
-.24804+04      .00000      .00000      -.24804+04
ENTROPY = BTU/LBM DEG R      .22753+01      .00000      .00000
DENSITY = LBM/FT3      .39804+00      .00000      .39804+00
MOLECULAR WEIGHT      23.2721      .0000      23.2721

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE (UE CM)) . . .
1= .49822-04 2= .67044-04 3= .12046-11 4= .24574-19 5= .11522-21
6= .30147-21 7= .27480-26 8= .26413-28

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .27438+01 2= .27438+01 3= .75284+01 4= .27438+01 5= .75284+01
6= .20656+02 7= .20442+02 8= .19474+00

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = RPRIME CONDENSED ) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .85921-02      H2      .38445+00      H2O      .30121-01      C*      .00000      CLH      .33103-01
FH      .39627-02      BE      .46478-13      CCLN      .17192-09      CO      .23852+00      C2H2      .15142-06
C      .36925-20      C2      .31321-23      C*      .74905-22      C*      .24869-28      C5      .13041-28
C2H6      .31974-19      HEC1      .37022-09      HECLEF      .47444-01      HECLE2      .12952-01      HFF      .75549-07
HEF2      .74927-01      HEH0      .15085-08      HEH2      .84046-10      HEH2O3      .22544-02      HFO      .17640-15
BE2CL4      .67036-07      BEF2O2      .14076-12      BE3O3      .47439-07      BE4O4      .60434-05      HES05      .57045-04
BE6O6      .38201-02      CCL      .44444-14      CCLFO      .45752-12      CCLFA      .27107-22      CCL2O      .60625-12
CCL3F      .24804-22      CCL4      .23116-22      CF      .15439-17      CF*      .22236-13      CF2      .46445-17
CF2O      .61283-12      CF3      .31722-22      CF4      .25451-22      CH      .10714-17      CHCLE2      .61564-17
CHCL2F      .14021-16      CHCL3      .49242-16      CHFO      .24971-14      CH*      .32045-17      CHN      .37644-04
CHNO      .25429-08      CHO      .93430-08      CH2      .73062-13      CH2CLEF      .52464-12      CH2CL2      .92022-11
CH2F2      .47337-13      CH2O      .25500-05      CH3      .24142-06      CH3CL      .52715-06      CH3F      .31217-08
CH4      .73102-02      C*      .25181-12      C2F2      .62044-25      C2F4      .44047-31      C2H4      .13545-05
C2H4O      .25441-13      C2H2      .74447-11      C3O2      .60514-11      C4H2      .67244-18      CL      .45545-07
CLF      .28423-14      CLEO3      .00000      CLE*      .00000      CLH0      .17927-11      CLN0      .40521-17
CLO      .43769-16      CLO2      .16245-27      CLO3      .15744-23      F      .72122-13      F*      .95043-18
FN      .38846-21      FNO      .14545-20      FO      .61591-24      F2O      .21925-36      F*      .00000
H      .53855-06      HN      .52442-12      HO      .80142-09      H2O      .43551-08      H2O2      .11415-15
H3N      .22196-03      H4H2      .64144-14      H*      .23443-15      NO      .40605-11      NO2      .22003-20
H2O      .48229-14      H2O3      .56012-36      H2O4      .00000      N2O5      .00000      O      .10360-14
O3      .16403-32      CCL2F2      .22278-22      CCLO      .11786-08      CFC*      .11241-12      CPE*      .44041-38
FNO2      .38048-31      CLN02      .61906-28      F2*      .72493-29      F*O3      .00000      H4O      .49163-14
BE*      .81119-14      HNO2      .12122-14      HNO3      .15244-28      HE2O      .54114-14      F*NO2      .00000
H2O2      .76146-19      NO3      .76544-14      CH4O      .44046-18      CCL2      .33734-17      CCL*      .11915-19
F2N2      .26453-34      H2N2      .20224-13      HE2F2O      .21678-01      CH2      .46774-17      C2O      .69201-14
CLF5      .00000      BEH      .00000      FO2      .62441-11      C2H*      .13954-12      C*H      .80212-16
C2CL4      .20215-24      C2CL6      .93260-17      C2HF      .26451-15      C2CL2      .24070-16      C2HCL      .47193-11
CHCL      .25239-15      CHF      .27044-15      C2F3N      .52410-25      F3CL      .00000      F2      .54023-25
CL2      .77717-10      H2      .11405-00      O2      .34436-16      CH*      .27460-13      *      .66649-19
C2H3      .30471-10      C2H4      .73444-04      C3H      .27704-14      C3H2      .13457-13      CH*H      .26247-11
C3H4      .14646-09      C3H5      .57432-08      C4H      .20547-17      C4H2      .34442-14

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Sample Problem 1 Output (Concluded)

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GRAPHITE SURFACE KINETICS (GASKET) PROB. 1      5002000+00      6 6

CP-FROZEN= .52269+00

PROPERTY ROUTINE OUTPUT IN LB-MASS,FT+SEC+RTU+AND OFG-H
TEMP      VISC      COND      DBAR      PR      SC
.72000+04 .64280+04 .66452+04 .55595+03 .50561+00 .72553+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL+
.87984+00 .23487+02 .24810+02 .84810+04 .73985+00 .69927+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASF) = .667)
1      2      3      4      5      6      7      8      9      10      11      12      13      14      15      16      17      18      19      20
.34442-01 .34894-01 .55762+00 .75109+01 .12072+00 .95579+01 .81641-01 .00000
.59850-01 .34231-01 .53805+00 .77487-01 .12461+00 .98065+01 .72704-01 .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = 4.693 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS ATJ GRAPHITE
MASS TRANSFER COEFFICIENT ROUN = .96900+00
RHO V WALL/RHOE UE CM = .90496+00      BPRIME = .90496+00

STATE ADJACENT TO THE SURFACE . . .
TEMP = 7199.9999 DEG R = 4000.0000 DEG K      PRESS = 31.47837 ATM

ENTHALPY = BTU/LBM      GAS      CONDENSED      COMPOSITE
.58476+04      .00000      .45474+04
ENTROPY = BTU/LBM DEG R      .24015+01      .00000      .00000
DENSITY = LBM/FT3      .14852+00      .00000      .14852+00
MOLECULAR WEIGHT      24.8099      .0000      24.8099

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM) . . .
1= .68928-08 2= .50169-08 3= .31663-01 4= .10204-02 5= .56004-02
6= .10715-02 7= .14080-03 8= .24100-05

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .12717+01 2= .12717+01 3= .16173+01 4= .12717+01 5= .16173+01
6= .20564+01 7= .26157+01 8= .33264+01

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = BPRIME CONDENSED ) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .40920-06      H2      .14220+00      H2O      .26537-05      C#      .00000
FH      .23877-01      FE      .68840+02      CCLN      .11922-03      CO      .18706+00
C      .16619-02      C2      .17498-02      C3      .81174+02      C4      .74222+04
C2H6      .52947-02      BECL      .29082-02      HCLF      .13700+01      HECL2      .21961-02
BEF2      .21516-01      HFNO      .69443-06      HFH2      .50970-04      3FH2O2      .20260+00
HE2CL4      .11603-08      HF2O2      .47866-11      HF3O3      .17855-15      HE4O4      .31693+20
BE6O6      .19430-31      CCL      .23411-04      CCLFO      .30144+09      CCLF3      .20419+17
CCL3F      .54822-14      CCL4      .10582-14      CF      .18453-03      CFH      .10499+04
CF2O      .30941-09      CF3      .37664-10      CF4      .14679-13      CH      .51956+03
CHCL2F      .67811-11      CHCL3      .24704-11      CHFO      .28027-07      CHF3      .70992+11
CHNO      .14881-06      CHO      .22842-04      CH2      .68656-06      CH2CLF      .14420+08
CH2F2      .76764-09      CH2O      .46237-06      CH3      .19064+03      CH3CL      .22271+05
CH4      .12706-04      CHN      .77914-02      C2F2      .20741-08      C2H4      .27694+15
C2H4O      .13140-12      C2H2      .41630-05      C3O2      .27134+07      C4H2      .51145+04
CLF      .18686-06      CLF3      .37722-14      CLF3      .39304+20      CLHO      .30383+09
CLO      .84935-09      CLO2      .14854-17      CLO2      .33655-14      F      .43851+03
FN      .14854-07      FNO      .37945-12      FO      .47587+11      F2O      .84752+18
H      .10666+00      HI      .30843-04      HO      .11849+05      4H      .73866-05
H3N      .13402+05      H3N2      .89843-13      H      .60870+04      JO      .11125+06
N2O      .73472-11      N2O3      .11633-26      F2O4      .84252+36      42O5      .00000
O3      .16508-21      CCL2F2      .13176-13      CCLO      .33264+05      CFO      .16610+06
FNO2      .41029-21      CLNO2      .23826-20      F2H      .14381+12      FNO3      .71199+31
BEN      .15094-04      HNO2      .61988-16      HNO3      .15354+24      HE2O      .12312+06
HO2      .10567-13      NO3      .12518-24      CF4O      .12314+22      CCL2      .24126+06
F2N2      .44303-17      H2F2      .31478-09      3E2F2O      .57605+06      CN2      .12552+05
CLF5      .11706-35      HEH      .25768-14      FO2      .71634+18      2H      .78099+01
C2CL4      .20610-14      C2CL6      .20847-24      C2HF      .33483+04      C2CL2      .77916+06
CHCL      .68925-04      CHF      .10444+04      C2F3H      .61728+13      FMO      .19937+27
CL2      .34953-05      N2      .37622-01      O2      .36844+11      CNO      .83820+07
C2H3      .63328-04      C2H6      .37445-09      CH      .68832+01      C3H2      .25206+02
C3H4      .25480-04      C3H5      .48875-05      CH4      .88971+01      C4H2      .43112+02

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Sample Problem 2

The shockwave option of GASKET is utilized in this problem. The surface material is made of 15% SiC/PG. The boundary layer edge state is specified as the stagnation condition behind a normal shock wave with an upstream Mach number of two. The shock is assumed to exist in the divergent section of a nozzle and, thus, conditions upstream of the shock are calculated via an isentropic expansion from input ideal chamber conditions. Since the edge gases contain both hydrogen and oxygen, all three kinetically-controlled surface reactions are possible. Two temperatures are input for both the frozen edge and surface temperature arrays. Finally, the diffusion factors are updated for 16 selected species.

Listing of Input

1.	5094220400	3901.	40.81	-2.0	66.02	0.463	0.0	PROP. 2
2.	.15							
3.	1000.							
4.	1500.							
5.								
6.	1200.							
7.	1400.							
8.								
9.	6							
10.	1 HYDROGEN	1.008	3.2219					
11.	6 CARBON	12.011	.56490		1.0			
12.	7 NITROGEN	14.008	.5366					
13.	8 OXYGEN	16.0	2.2486					
14.	13 ALUMINUM	26.98	1.013					
15.	17 CHLORINE	35.453	.5398					
16.	1	0.0	-9999.		0.0			
17.	16							
18.	C	0.69100CH	0.74920CH4		0.93570CH		1.02670	
19.	CO	1.01700CO2	1.29140C2H2		1.17460H		0.30180	
20.	H2	0.38930H2O	0.77490N		0.74930NO		0.99810	
21.	N2	1.026200	0.7397002		1.00000C2		1.02530	
22.	8							

Sample Problem 2 Output

GRAPHITE SURFACE KINETICS (GASKET) PROB. 2 0110000*J0

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00800	.0322205	.0000000
6	CARBON	12.01100	.0052493	.0000000
7	NITROGEN	14.00800	.0053663	.0000000
8	OXYGEN	16.00000	.0224271	.0000000
13	ALUMINUM	26.98000	.0101305	.0000000
17	CHLORINE	35.45300	.0053983	.0000000
14	SILICON	28.09000	.0000000	.0037407
106	GRAPHITE	12.01100	.0000000	.0745088

ELEMENTS	HYDROGEN CHLORINE	CARBON SILICON	NITROGEN GRAPHITE	OXYGEN	ALUMINUM
BASE SPECIES	H2 CLH	CO2 CH3CL3S	ALN C*	H2O	AL

Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) SOLUTION          PROB. 2

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN CP-EQUIL DLNFM/DLNT DLNFM/DLNP GAMMA
.42289+00 .12704+01 -.81279+00 .49323+01 .11173+01

PROPERTY ROUTINE OUTPUT IN LB-MASS.FT.SEC+RTU.AND OFG-H
TEMP      WISC      COND      UBAR      PR      SC
.70218+04 .62950+04 .84839+04 .24681+03 .20753+00 .72419+00
MU1        MU2      MOL.WT      HTIL      CPTIL      HTIL*
.73200+00 .19437+02 .33303+02 .65193+04 .96142+00 .43301+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .667)
      6      7      8      13      14      106
.32478+01 .67853+01 .75170+01 .35979+00 .27332+00 .19134+00 .00000 .00000
.11322+00 .11673+00 .12994+00 .26974+00 .46727+01 .20364+00 .00000 .00000

SOLUTION TIMES
ITERATIONS = 27          TIME = 5.727 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72922+00
TEMP = 7021.8000 DEG R. = 3901.0000 DEG K.    PRESS = 64.02000 ATM

ENTHALPY = BTU/LBM      GAS      CONDENSED      COMPOSITE
.19521+04      .45284+04      -.78073+03
ENTROPY = HTU/LBM DEG R. .21114+01      .48044+00      .72097+01
DENSITY = LBM/FT3      .25544+00      .101.9600      .44172+00
MOLECULAR WEIGHT      19.2588      101.9600      31.3027

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
C02      .34049+02      H2      .32612+00      H2O      .10142+00      C*      .00000
AL      .34049+02      ALN      .62793+06      CH3CL3S      .00000      C*      .14134+00
C      .61816+07      C2      .27773+11      C3      .05550+14      C4      .61009+20
CAL      .15823+08      ALCL      .30440+01      ALCL0      .57887+02      ALCL2      .10091+01
ALH      .47985+03      ALH02      .26119+02      AL0      .22285+02      AL2CL6      .23514+10
AL202      .13163+04      CCL      .40185+08      CCLN      .54882+07      CCL20      .13645+08
CH      .46292+07      CHCL3      .21843+13      CHN      .12377+04      CHN0      .71144+06
CH2      .20564+07      CH2CL2      .62869+11      CH20      .22208+05      CH3      .12179+06
CH4      .21208+07      CH4      .81008+06      C2H4      .13280+11      C2H40      .40575+15
C302      .67075+11      C4H2S1      .00000      C4H2      .24948+19      CL      .19093+01
CLH3SI      .00000      CLN0      .20144+06      CL0      .19467+04      CL02      .46439+09
CL2H2SI      .00000      CL20      .30342+09      CL2S1      .00000      CL3HS1      .00000
H      .92093+01      HN      .54434+04      HO      .16302+01      HSI      .00000
H202      .78294+06      H3N      .16734+04      H4N2      .46761+11      H4S1      .00000
N0      .14889+02      N02      .14505+06      N1      .00000      H20      .22032+06
N204      .67070+19      N205      .16845+22      O      .26379+02      CSI      .00000
O3      .17671+04      SI      .00000      S12      .00000      S13      .00000
CLN02      .17850+11      HN0      .34743+05      HN02      .28577+07      HN03      .10030+11
H02      .20316+05      N03      .31540+12      CCL2      .19426+09      CCL3      .89640+13
CN2      .28294+09      C20      .67827+08      C2H      .10781+08      CSI      .00000
C2N      .80606+10      C2S1      .00000      HSI2      .00000      C2CL4      .41566+20
AL02      .30844+03      C2CL2      .68407+13      C2HCL      .27460+10      CHCL      .38211+08
CL2      .24563+04      N2      .48527+01      O2      .32099+03      CND      .14687+06
C2H3      .50618+11      C2H6      .42556+15      C3H      .10796+13      C3H2      .10796+13
C3H4      .66570+16      C3H5      .29253+15      C4H      .20527+16      C4H2      .28295+17
CSI*      .00000      CLH40*      .00000      CLH40*      .00000      ALCL1*      .00000
AL205SI*      .00000      C3AL4*      .00000      H4S1*      .00000      AL*      .00000
O2SI*      .00000      SI*      .00000      AL013S*      .00000

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CLH      .10317+00      C2H2      .21043+08      C5      .15053+23      ALCL4      .16885+03
C2H0      .14059+02      AL20      .14059+02      CCL4      .16440+16      CH0      .43111+04
CH3CL      .65644+09      C2N2      .14714+10      CLH0      .18083+04      CLS1      .00000
CLH03      .00000      CLH04      .00000      H2N      .13589+04      F      .43874+04
H2N      .13589+04      F      .43874+04      F203      .65235+14      C2S1      .00000
CCL0      .12090+02      ALH0      .30329+02      H2N2      .31542+08      CS12      .00000
C2CL6      .66177+29      CL3S1      .00000      N3      .10342+08      C3H4*      .00000
ALH0      .16381+14      ALCL0*      .00000      ALN*      .00000      AL203*      .13774+08

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Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) PROJ. 2 2000200*00

DERIVATIVE PROPERTY OUTPUT

CP=FROZEN	CP=EQUIL	DLNM/DLNT	DLNM/DLNP	GAMMA
.42237+00	.13866+01	-.90234+00	.53735-01	.11154+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, RTU, AND DEG-R

TEMP	VISC	COND	DBAP	PR	SC
.68843+04	.62125-04	.83769-04	.39809-03	.2073A+00	.72416+00
MU1	MU2	MOL.WT	HTIL	CPIL	HTIL*
.72854+00	.19343+02	.32992+02	.66964+04	.96181+00	.44251+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER (GAMEX = .667)

1	6	7	8	13	17	14	106
.32478-01	.67853-01	.75171-01	.35979+00	.27332+00	.19138+00	.00000	.00000
.11334+00	.11629+00	.12945+00	.28969+00	.67757-01	.28347+00	.00000	.00000

SOLUTION TIMES

ITERATIONS = 4

TIME = 1.144 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72521+00

TEMP = 6A84.3399 DEG R. = 3A24.6333 DEG K. PRESS = 40.81000 ATM

ENTHALPY - BTU/LBM	GAS	CONDENSED	COMPOSITE
	18708 ± 0%	55750 ± 0%	70073 ± 0%

ENTHALPY = BTU/LBM	.19709+04	-.45750+04	-.78073+03
ENTROPY = BTU/LBM DEG R	.29646+01	-.97375+00	-.31277+01

ENTROPY = BTU/DEG R	.29848+01	.97375+00	.21277+01
DENSITY = LBM/FT3	.15522+00		.26779+00

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
C02	.66546-02	H2	.31914+00	H2U	.94954-01	C	.00000	CLH	.10313+09
AL	.38011-02	ALN	.50442-06	C3HCL3S	.00000	C0	.17944-08	CM2	.74189-09
C	.42776-07	C2	.34498-11	C3	.15450-14	C4	.97545-21	C5	.15391-24
CAL	.91928-09	ALCL	.31646-01	ALCLO	.60046-02	ALCL2	.87705-02	ALCLO	.12395-03
ALH	.42844-03	ALH02	.26300-02	ALO	.24446-02	AL2CL6	.79259-11	AL2C3	.14617-02
AL202	.13715-05	CCL3	.23072-0A	CCL4	.32720-05	CCL20	.74649-09	CCL4	.50571-17
CM	.2647-07	CHL	.71824-14	CH	.72723-05	CH0	.41400-06	CH0	.29746-04
CM2	.10254-07	CH2CL2	.12817-05	CH20	.12917-05	CH3	.541-07	CH3CL	.24218-09
CH4	.83002-08	CN	.51440-06	C2H4	.31748-12	C2H40	.81722-16	CH20	.17727-11
C302	.22951-11	C4H2S1	.00000	C4H2	.35153-20	C	.12125-01	CLH0	.15154-06
CLH3S1	.00000	CLN0	.15142-06	CL0	.18806-04	CL02	.38063-09	CLS1	.00000
CLH2S2S1	.00000	CL20	.21360-09	CL2S1	.00000	CL3HS1	.00000	CL4S1	.00000
H	.10200+00	HN	.43880-04	H0	.17379-01	HS1	.00000	H2N	.22965-74
H202	.60506-06	H3N	.99957-05	H4N2	.14790-11	H4S1	.00000	N	.41830-04
NO	.15441-02	H02	.13285-06	H51	.00000	N20	.17530-00	N203	.37571-14
N204	.33807-19	H205	.72549-23	H	.31949-02	OS1	.00000	N2S1	.00000
O3	.16687-09	SI	.00000	SI2	.00000	S13	.00000	OS0	.33900-05
CLN02	.11848-11	H4N0	.27467-05	HU02	.21334-07	HU03	.65512-12	ALH0	.30315-02
HL02	.10717-05	N03	.25374-12	CL2	.91370-10	CCL3	.34541-13	H2N2	.16010-08
CN2	.13420-09	C20	.33590-08	C2H	.42842-09	C51	.00000	CS12	.00000
C2N	.30556-10	C2S1	.00000	NS12	.00000	C2CL4	.77890-21	C3CL6	.68144-30
AL02	.34649-03	C2CL2	.28166-13	C2HCL	.92944-11	CHCL	.18481-08	CL3S1	.00000
CL2	.21420-04	N2	.87684-01	O2	.38874-03	CN0	.93847-07	N3	.60613-09
CLH	.13369-11	C2H6	.63114-16	C3	.31154-13	CSH2	.21307-14	CSH3	.26940-15
CSH4	.91207-17	C3H5	.31438-16	C4H	.30331-17	CHW2	.31891-18	CLH00	.00000
C3H	.00000	CLH4H0	.00000	CLH4H0H4	.00000	ALCL3	.00000	ALN0	.00000
AL205S1*	.00000	C3AL4*	.00000	NA51S1*	.00000	AL*	.00000	AL203*	.13662+00
O2S1*	.00000	SI*	.00000	AL6013S*	.00000				

Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET)   PROB. 2   5000100*00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN   CP-EQUIL   DLNM/DLNT   DLNM/DLNP   GAMMA
.42267+00   .11508+01   -.62810+00   .33430-01   .11111+01

PROPERTY ROUTINE OUTPUT IN LB-MASS.FT*SEC*BTU*AND DEG-R
TEMP      VISC      COND      DBAR      PR      SC
.58395+04   .55713-04   .77229-04   .22498-02   .19013+00   .72459+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.71314+00   .18914+02   .34303+02   .54259+04   .98836+00   .35344+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      6      7      8      13      17      14      106
.32478-01   .67853-01   .75170-01   .35979+00   .27332+00   .19138+00   .00000
.12227+00   .12477+00   .13877+00   .26677+00   .35429-01   .31199+00   .00000

SOLUTION TIMES
ITERATIONS = 8                      TIME = 2.154 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT
MASS CONDENSED/MASS GAS = .88144+00
TEMP = 5439.4862 DEG R. = 3244.1602 DEG K.   PRESS = 5.49553 ATM

ENTHALPY - BTU/LBM      GAS      CONDENSED      COMPOSITE
.14629+04   .14629+04   -.49294+04   -.15324+04
ENTROPY - BTU/LBM DEG R   .31944+01   .91785+00   .21277+01
DENSITY - LBM/FT3        .21492-01   .44203+01
MOLECULAR WEIGHT         18.2305   101.9600   34.3033

ABOVE ARE STATIC PROPERTIES      K-KINETIC = .75168+03 BTU/LBM
VEL. = .6134+04 FT/SEC   FLUX = .27115+03 LBM/FT2SEC   MACH = 2.00009

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES)....
SPECIES   MOLE FR.   SPECIES   MOLE FR.   SPECIES   MOLE FR.   SPECIES   MOLE FR.   SPECIES   MOLE FR.
CO2        .57216-02   H2         .35496+00   H2O        .83429+01   C*         .00000      CLH        .13076+00
AL         .10219-02   ALN        .28250-07   CH3CL3S    .00000      CO         .18806+00   C2H2       .34405-10
C          .22047-04   C2         .36449-13   C3         .86103-17   C4         .75224-24   C5         .42889-28
CAL        .13454-10   ALCL       .19183-01   ALCLO      .81966-02   ALCL2      .59746-02   ALCL3      .91144-04
ALH        .66549-04   ALH2       .73142-03   ALD        .43774-03   AL2CL6     .87286-12   AL2O       .22585-03
AL2O2      .16610-05   CCL        .10738-09   CLN        .34864-04   CCL2O      .87612-10   CCL4       .97907-19
CH         .10625-08   CHCL3      .23164+15   CHN        .14237-05   CH2O       .55778-07   CH3CL      .17698-05
CH2        .52156-09   CH2CL2     .10484-12   CH2        .20662-06   CH3        .43080-08   CH3CL      .17698-05
CH4        .87956-09   CN         .49273-07   C2H4       .60120-14   C2H4O      .50464-18   C2H2       .12991-12
C3O2       .52186-13   C4H2SI     .00000      C4H2       .36796-23   CL         .19782-01   CLH2O      .35802-05
CLH3SI     .00000      CLN2       .14008-07   CLD        .36828-05   CL2        .12846-10   CLSI       .00000
CL2H2SI    .00000      CL2O       .11589-10   CL2SI      .00000      CL3H3SI    .00000      CL4SI      .00000
H          .80459-01   HN         .70494-05   HO         .74131-02   HSI        .00000      H2N        .39376-05
H2O2       .47484-07   H3N        .21441-05   H4N2       .18131-13   H4SI       .00000      H2N        .76693-05
NO         .46806-03   NO2        .99751-08   NSI        .00000      N2O        .19283-07   N2O3       .00000
N2O4       .26890-22   N2O5       .10035-26   O          .10040-02   O2         .00000      O2SI       .00000
O3         .31641-11   SI         .00000      S12        .00000      S13        .00000      CCLO       .16998-05
CLN2       .23702-13   HN2        .31141-06   HN2O2      .11069-08   HN2O3      .78013-14   ALH2O      .10207-02
H2         .16208-06   NO3        .23454-14   CCL2       .44799-11   CCL3       .10606-14   H2N2       .74808-10
CN2        .36106-11   C2O        .13467-09   C2H        .13260-10   CSI        .00000      CS12       .00000
C2N        .55699-12   C2SI       .00000      NS12       .00000      C2CL4      .35771-23   C2CL6     .33426-33
AL2O2      .49744-04   C2CL2      .61986-15   C2HCL      .31046-12   CHCL       .79986-10   CL3SI     .00000
CL2        .10691-04   N2         .91795-01   O2         .93117-04   CNO        .73102-08   N3         .20733-10
C2H3       .19746-13   C2H6       .39104-18   C3H        .27295-15   C3H2       .10612-16   ALCL2O*    .00000
C3H4       .31700-19   C3H5       .53164-19   C4H        .51075-20   C4H2       .56120-21   ALCL3*     .00000
CS1*       .00000      CLH4H*     .00000      CLH4H*     .00000      ALCL3*     .00000      AL*        .00000
AL2O5SI*   .00000      C3AL4*     .00000      N4S13*     .00000      AL*        .00000
O2SI*      .00000      SI*        .00000      AL6O13S*   .00000

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Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET)  PROGR. 2  4000300+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN  CP-EQUIL  DLNM/DLNT  DLNM/DLNP  GAMMA
.42208+00  .14694+01  -.95479+00  .55542-01  .11133+01

PROPERTY ROUTINE OUTPUT IN  LB-MASS,FT,SEC,RTU,AND DEG-R
TEMP      VISC      COND      DBAR      PH      SC
.66873+04  .60935-04  .82537-04  .67562-03  .20531+00  .72416+00
MU1       MU2      MOL.WT    HTIL      CPTIL    HTIL*
.72372+00  .19211+02  .32842+02  .67796+04  .96604+00  .44566+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .667)
      1      6      7      8      13      17      14      106
.32478-01  .67453-01  .75171-01  .35979+00  .27332+00  .19138+00  .00000  .00000
.11435+00  .11673+00  .12993+00  .28765+00  .65560-01  .28578+00  .00000  .00000

SOLUTION TIMES
ITERATIONS = 6              TIME = 1.642 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .73616+00      PRESS = 22.91442 ATM
TEMP = 6687.2614 DEG R. = 3715.1452 DEG K.

ENTHALPY - RTU/LBM      GAS      CONDENSED      COMPOSITE
.30291+01  .19543+04  -.46420+04  -.84259+03
ENTROPY - BTU/LBM DEG R  .30291+01  .96388+00  .21534+01
DENSITY - LBM/FT3      .84753-01  .15409+00
MOLECULAR WEIGHT      18.9163      101.9600      32.8417

VEL2 = .1760+04 FT/SEC      MACH2 = .52408      THETA 2 = .000000 DEG
ABOVE ARE STATIC CONDITIONS DOWNSTREAM OF THE SHOCK FOR ...
VEL1 = .613+04 FT/SEC      H1-STATIC = -.153+04 RTU/LBM      H-TOT = -.781+03 RTU/LBM
P1 = 5.49553 ATM      RH01 = .44203-01 LBM/FT3      THETA 1 = .000000 DEG

STATIC CHEMICAL STATE (MOLE FR.=MOLECULES/TOTAL GAS PHASE MOLECULES)...
SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.
CO2      .65572-02  H2       .31644+00  H2O      .95764-01  C*      .000000  CLH*     .10146+00
AL       .58066-02  ALN      .34344-04  CH3CL3S .000000  CO       .17894+00  C2H2     .24640-09
C        .25328-07  C2       .11828+11  C3       .36136-15  C4       .12391-21  C5       .12456-25
CAL      .42995-09  ALCL     .31215-01  ALCLU    .53265-02  ALCL2    .75948-02  ALCL3    .93504-04
ALH      .34166-03  ALH2     .24153-02  ALU      .25390-02  AL2CL6   .27008-11  AL2O     .13289-02
AL2O2    .12234-04  CCL      .11578-08  CCLN     .16876-07  CFL2O    .38431-09  CCL4     .14001-17
CH       .13112-07  CHCL3    .21492-14  CHN      .40859-05  CH*O     .22341-06  CHO      .19150+04
CH2      .46012-08  CH2CL2   .72125-12  CH2O     .71645-06  CH3      .22814-07  CH3CL    .86541-10
CH4      .31908-08  CH4      .29621-06  C2H4     .67417-13  C2H4O    .15619-16  C2H2O    .15312-11
C3O2     .70543-12  C4H2SI   .000000  C4H2     .36169-21  CL       .25150-03  CLMO     .11745-04
CLH3SI   .000000  CLN2     .10243-06  CL2SI    .000000  CL2      .24139-09  CLSI     .000000
CL2H2SI  .000000  CL2O     .12447-09  CL2SI    .000000  CL3H2SI  .000000  CL4SI    .000000
H        .10940+00  HN       .31434-04  HO       .17240-01  HSI      .000000  H2N      .14683-04
H2O2     .40442-06  H3N      .57443-05  H4O2     .40745-12  H4SI     .000000  H       .35563-04
NO       .14605-02  NO2      .10217-06  HSI      .000000  H2O      .12316-06  H2O3     .15545-14
N2O4     .11272-19  N2O5     .18577-23  O        .34610-02  O2       .000000  O2SI     .000000
O3       .11910-04  SI       .000000  S12      .000000  S13      .000000  CLO      .54905-05
CLN02    .63045-12  HNO      .19269-05  HNO2     .14443-07  HNO3     .33111-12  ALMO     .28044-02
H02      .14622-05  N03      .13378-12  CCL2     .40636-10  CFL3     .000000  H2N2     .72596-09
CN2      .55106-10  C2O      .14718-08  C2H      .15315-09  CCL3     .000000  CS12     .000000
CPN      .14102-10  C2SI     .000000  H5I2     .000000  C2CL4    .12619-21  C2CL6    .57432-31
AL02     .32283-03  C2CL2    .81011-14  C2HCL    .24981-11  CHCL     .79824-09  CL3SI    .000000
CL2      .18137-04  N2       .67341-01  O2       .41144-03  CNO      .53474-07  N3       .30164-09
C2H3     .32188-12  C2H6     .86408-17  C3H      .68220-14  C3H2     .36974-15  C3H3     .39846-16
C3H4     .11337-17  C3H5     .30216-17  C4H      .38134-18  C4H2     .35184-19  ALCLO*   .000000
CSI*      .000000  CLH4H*   .000000  CLH4H04* .000000  ALCL3*   .000000  ALN*     .000000
AL2O5SI*  .000000  C3AL4*   .000000  H4SI3*   .000000  AL*       .000000  AL2O3*   .13648+00
O2SI*     .000000  SI*       .000000  AL6O13S* .000000

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Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROB. 2

DERIVATIVE PROPERTY OUTPUT
 CP-FROZEN CP-EQUIL DLNM/DLNT DLNM/DLNP GAMMA
 .42198+00 .14901+01 -.97911+00 .57415-01 .11137+01

PROPERTY ROUTINE OUTPUT IN LB-MASS.FT.SEC+RTU+AND DFG-R
 TEMP VISC COND DBAR PR SC
 .67695+04 .61431-04 .82941-04 .59241-03 .20701+00 .72413+00
 MU1 MU2 MOL.WT HTIL CPTIL HTIL*
 .72531+00 .19255+02 .32735+02 .68589+04 .96296+00 .45142+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)

1	6	7	8	13	17	14	106
.32478-01	.67853-01	.75171-01	.35479+00	.27332+00	.19138+00	.00000	.00000
.11354+00	.11600+00	.12912+00	.28951+00	.48365-01	.28346+00	.00000	.00000

SOLUTION TIMES
 ITERATIONS = 3 TIME = .954 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72300+00
 TEMP = 6769.4843 DEG R. = 3760.8246 DEG K. PRESS = 26.66895 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LHM	.19907+04	-.46140+04	-.78073+03
ENTROPY - BTU/LHM DEG R	.48105+01	.96803+00	.21534+01
DENSITY - LBM/FT3	.10248+00		.17658+00
MOLECULAR WEIGHT	18.9990	101.9600	32.7352

ABOVE ARE ISENTROPIC STAGNATION CONDITIONS DOWNSTREAM OF THE SHOCK FOR . . .
 VELL = .613+04 FT/SEC H1-STATIC = -.153+04 BTU/LHM H-TOT = -.781+03 BTU/LHM
 P1 = 5.49553 ATM RH01 = .44203-01 LBM/FT3 THETA 1 = .000000 DEG

ISEN. STAG. CHEMICAL STATE (MOLE FR.=MOLECULES / TOTAL GAS PHASE MOLECULES)..

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.66244+02	H2	.31844+00	H2O	.96757-01	C*	.00000	CLH	.99440-01
AL	.41177-02	ALN	.41753-06	CH3CL3K	.00000	CO	.17827-00	C2H2	.31299-09
C	.31162-07	C2	.16515-11	C3	.53108-15	C4	.21174-21	C5	.23125-25
CAL	.57655-09	ALCL	.32058-01	ALCL0	.61418-02	ALCL2	.77738-02	ALCL3	.95705-04
ALH	.38606-03	CLL	.14413-04	CLLN	.19762-07	CLL20	.35038-11	AL20	.18492-02
AL202	.13972-04	CLL02	.28195-02	CLLN	.19762-07	CLL20	.35038-11	CLL4	.18492-02
CH	.16502-07	CHCL3	.28403-14	CHN	.46268-05	CHN0	.25955-06	CH0	.21769-04
CH2	.57256-04	CH2CL2	.90902-12	CH20	.42266-06	CH3	.27665-07	CH3CL	.10615-09
CH4	.38123-08	CN	.35097-06	C2H4	.91729-13	C2H40	.25097-16	C2H2	.20210-11
CO2	.94123-12	C4H2SI	.00000	C4H2	.61212-21	CL	.25115-01	CLH0	.12975-04
CLH3SI	.00000	CLN0	.12044-06	CL0	.18052-04	CL02	.31630-09	CLSI	.00000
CL2H2SI	.00000	CL20	.15714-09	CL2SI	.00000	CL3H4C1	.00000	CL4SI	.00000
H	.11054+00	HN	.38137-04	HO	.18184-01	HSI	.00000	H2N	.16675-04
H2O2	.44268-06	H3N	.64423-05	H4H2	.56497-12	H4SI	.00000	N	.39880-04
NO	.13772-07	N02	.12161-06	NSI	.00000	N20	.14360-06	I203	.25112-14
N204	.18551-19	N205	.34535-23	O	.37092-02	OSI	.00000	O2SI	.00000
O3	.15521-09	SI	.00000	SI2	.00000	SI3	.00000	CLC0	.61645-05
CLN02	.82745-12	H40	.22406-05	HN02	.16411-07	HN03	.45079-12	ALH0	.30063-02
H02	.17225-05	N03	.18353-12	CLL2	.50754-10	CLL3	.15528-13	H2N2	.90840-09
CN2	.71735-10	C20	.18641-08	C2H	.19863-09	CS1	.00000	CS12	.00000
C2N	.13594-10	C2SI	.00000	NSI2	.00000	C2CL4	.19282-21	C2CL6	.17071-30
AL02	.36435-03	C2CL2	.10809+13	C2HCL	.37568-11	CHCL	.10042-08	CL3SI	.00000
CL2	.19006-04	N2	.86440-01	O2	.44450-03	CND	.64254-07	N3	.38342-09
C2H3	.44419-12	C2H6	.12457-16	C3H	.47754-14	C3H2	.55444-15	C3H3	.60615-16
C3H4	.17612-17	C3H5	.49637-17	C4H	.62057-18	C4H2	.57383-19	ALCLO*	.00000
CS1*	.00000	CLH4N*	.00000	CLH4N0*	.00000	ALCLH*	.00000	ALN*	.00000
AL205SI*	.00000	C3AL4*	.00000	H4SI3*	.00000	AL*	.00000	AL203*	.13472+00
O2SI*	.00000	SI*	.00000	AL60135*	.00000				

Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASNET) PROR. 2 0090000000
UPDATE OF DIFFUSION FACTORS

SPECIES	DIFFUSION FACTOR
CO2	1.29160
H2	.36930
H2O	.77490
CO	1.01700
CPH2	1.17460
C	.69180
C2	1.02930
CH	.74920
CH4	.93570
CN	1.02670
H	.30160
N	.74930
NO	.99810
O	.73970
N2	1.02620
O2	1.00000

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DNH/DLIT	DLNH/DLNP	CAPMA
.35736+00	.10551+02	-.39322+01	.90604+01	.94911+00

PROPERTY ROUTINE OUTPUT IN LH-MASS, FT, SEC, RTU, AND DEG-K

TEMP	VISC	COND	UHAR	PR	SC
.14000+04	.23573+04	.22113+04	.65800+04	.24968+00	.72409+00
MU1	MU2	POL.WT	MTIL	PTIL	HTIL
.76380+00	.18628+02	.32735+02	.13115+04	.66736+00	.50277+03

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER

1	2	3	4	5	6	7	8	9	10
.32878+01	.67853+01	.75171+01	.35974+00	.27332+00	.19134+00	.00000	.00000	.00000	.00000
.96237+01	.11806+00	.13071+00	.29634+00	.45249+01	.28731+00	.00000	.00000	.00000	.00000

SOLUTION TIMES

ITERATIONS = 3 TIME = .443 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72300+00
TEMP = 1400.0000 DEG K. PRESS = 26.66495 ATP

	GAS	CONDENSED	COMPOSITE
ENTHALPY - RTU/LHM	-.25724+03	-.67346+04	-.29774+04
ENTROPY - RTU/LHM DEG K	.24231+01	.42230+00	.15835+01
DENSITY - LHM/FT3	.38543+00		.66409+00
MOLECULAR WEIGHT	14.9440	101.9600	32.7352

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.66244+02	H2	.31444+00	H2O	.96797+01	C	.00000	CPH2	.99490+01
AL	.41177+02	ALH	.41753+06	CH4CL3S	.00000	CO	.17427+00	CLH	.31299+09
C	.31162+07	C2	.16415+11	C3	.53108+15	C4	.21172+21	C5	.23196+25
CAL	.57645+09	ALCL	.52059+01	ALCL0	.61418+02	ALCL2	.77738+02	ALCL4	.95705+04
ALH	.38646+03	ALH02	.26145+02	ALO	.24040+02	AL2CL6	.32038+11	AL20	.14925+02
AL202	.13972+04	CCL	.14413+08	CCLH	.14762+07	CCL20	.45073+09	CCL4	.18820+17
CH	.16502+07	CHCL3	.28403+14	CH4	.44268+05	CH40	.25955+06	CH0	.21769+04
CH2	.57256+08	CH2CL2	.90402+12	CH20	.42266+06	CH3	.27463+07	CH3CL	.10615+09
CH4	.38123+08	CH	.35057+06	C2H4	.91729+13	C2H40	.23097+16	C2H2	.20210+11
C302	.94123+12	CH4PST	.00000	C4H2	.41212+21	CL	.23113+01	CLH0	.12976+04
CLH3SI	.00000	CLN0	.12094+04	CL0	.12052+04	CL02	.31639+09	LLSI	.00000
CLH2ST	.00000	CL20	.15714+09	CL2SI	.00000	CL3HST	.00000	CL4ST	.00000
H	.11044+00	HN	.26137+04	H0	.14184+01	HSI	.00000	H2N	.16678+04
H202	.48268+06	H3N	.44423+05	H4H2	.76497+12	H4SI	.00000	H	.39802+04
NO	.15772+03	N02	.12161+04	SI	.00000	N20	.14364+06	20S	.23112+14
N204	.18551+14	N205	.34435+23	O	.37092+02	OSI	.00000	O2SI	.00000
O3	.15591+09	SI	.00000	SI2	.00000	SI3	.00000	CCLO	.61653+05
CLN02	.82745+12	HNO	.22406+05	H402	.14511+07	H403	.45079+12	ALH0	.30043+02
H02	.17225+05	N03	.18353+12	CCL2	.40754+10	CCL3	.15528+13	H2N2	.90810+09
CN2	.71735+10	C20	.14461+08	C2H	.14463+09	CSI	.00000	CS12	.00000
C2H	.13594+10	C2SI	.00000	CS12	.00000	C2CL4	.19282+21	C2CL6	.10207+30
AL02	.36435+03	C2CL2	.10409+13	C2HCL	.37564+11	CHCL	.10042+04	CL3ST	.00000
CL2	.19006+04	N2	.46990+01	O2	.44950+03	CL0	.64254+07	N3	.38342+09
CLH3	.44419+12	C2H4	.12457+16	C3H	.97734+14	C3H2	.55444+15	CSH3	.60643+16
C3H4	.17612+17	C3H5	.49639+17	C4H	.42057+18	C4H2	.47383+19	ALCL04	.00000
CSI	.00000	CLH4N	.00000	CLH4N04	.00000	ALCL14	.00000	ALN4	.00000
AL205SI	.00000	C3AL4	.00000	HSI3	.00000	AL	.00000	AL203	.13472+00
O2SI	.00000	SI	.00000	AL6013S	.00000				

Sample Problem 2 Output (Continued)

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CP-PROZEM  .37638+00

PROPERTY ROUTINE OUTPUT IN LB-PASS,FT,SEC,HTU,AND DFG-H
TEMP      VISC      COND      DPAR      PR      SC
.81688+04 .28888+04 .25662+04 .89088+04 .39318+00 .72437+00
MU      MU      MOL.WT      HTIL      CPTIL      HTILO
.03997+00 .20538+02 .25888+02 -.11818+04 .64087+00 -.15830+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .647)
      1      6      7      8      13      17      18      106
.00045+01 .10165+00 .11071+00 .24012+00 .98337+01 .40033+00 .40674+05 .00000
.96235+01 .11809+00 .13073+00 .24633+00 .49295+01 .24731+00 .46902+05 .00000

SOLUTION TIMES
ITERATIONS = 29      TIME = 4.449 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS SIC/PG
MASS TRANSFER COEFFICIENT ROUGH = .46300+00
RHO V WALL/RHOE UE CM = .44639+04 HFKINE = .44639+04

STATE ADJACENT TO THE SURFACE . . .
TEMP = 2160.0000 DEG R = 1200.0000 DEG K      PRESS = 26.66895 ATM

      GAS      COMPENSED      COMPOSITE
ENTHALPY - RTU/LBM      -.15525+04      .00000      -.15525+04
ENTROPY - RTU/LBM DEG R      .20017+01      .00000      .00000
DENSITY - LBM/FT3      .43759+00      .00000      .43759+00
MOLECULAR WEIGHT      25.8842      .0000      25.8842

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOF UE CM) . . .
1= .39581+04 2= .27801+05 3= .21308+10 4= .21079+23 5= .16877+26
6= .66781+26 7= .60427+32 8= .50836+34

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .32088+01 2= .32088+01 3= .10816+02 4= .32088+01 5= .10816+02
6= .35572+02 7= .42073+04 8= .55184+06

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = RPRIME CONDENSED ) . . .

      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
      CO2      .40874+01      H2      .42502+00      H2O      .15115+00      CO      .00000      CLM      .10230+01
      AL      .27935+14      ALN      .20846+21      CH3CL3S      .21831+09      CO      .15525+04      C2M2      .47424+08
      C      .12600+24      C2      .13441+20      C3      .47686+27      C4      .11707+34      C5      .52747+35
      CAL      .78428+24      ALCL      .57363+06      ALCLC      .15427+05      ALCL2      .97485+03      ALCL3      .88782+01
      ALM      .35048+13      ALM02      .74113+06      AL      .10322+14      AL2CL6      .22790+02      AL2O      .77191+11
      AL2O2      .28495+12      CCL      .21445+23      CCLV      .11774+11      CCl2O      .62767+14      CCL4      .98809+27
      CM      .38662+21      CMCL3      .42540+19      CM4      .46410+05      CM4U      .12279+06      CM4      .66837+09
      CM2      .28693+15      CH2CL2      .12754+12      CM2O      .18406+05      CM3      .38078+07      CM3CL      .11247+06
      CM4      .22542+01      CM      .43416+15      CM4U      .56033+06      CM4UO      .58880+14      CM2      .46047+13
      C3O2      .26131+12      CM2S1      .21327+15      CM4U2      .12867+21      CL      .53377+09      CLM0      .62041+13
      CLM3S1      .13848+05      CLN0      .14844+19      CLU      .92421+19      CL02      .47399+31      CLS1      .31085+14
      CL2M2S1      .47949+07      CL2O      .23441+27      CL2S1      .11430+07      CL3M2      .39019+07      CL4S1      .56891+06
      H      .24800+07      H1      .40799+14      H0      .67477+10      HSI      .53950+16      H2N      .40544+09
      H2O2      .16346+16      H3N      .44847+03      H4U2      .14564+14      H4S1      .72323+10      I      .24938+18
      NO      .14021+12      NO2      .23467+22      FSI      .11081+16      V2O      .14621+16      H2O3      .00000
      N2O4      .00000      N2O5      .00000      O      .42029+17      OSI      .25232+05      O2S1      .42141+09
      O3      .53704+36      SI      .98640+18      S12      .14701+26      S18      .31254+32      CCLN      .22529+10
      CLN02      .50891+31      HNO      .15797+15      H4O2      .62473+20      H4O3      .22184+30      ALMO      .15982+06
      H02      .11399+20      NO3      .58541+37      CCL2      .97581+21      CCL3      .75063+24      H2M2      .86176+15
      CM2      .37940+20      C2O      .12163+16      CM4      .12495+15      CSI      .11571+27      CS12      .29665+24
      C2N      .18942+19      C2S1      .66610+23      S12      .21422+21      C2CL4      .11728+29      C2CL6      .00000
      AL02      .38095+15      C2CL2      .38320+20      CMCL      .12442+13      CMCL      .11958+18      CL3S1      .93370+07
      CL2      .32313+12      H2      .10206+00      U2      .76456+18      CM0      .33204+15      H3      .12775+21
      CMH3      .50928+12      C2H6      .27511+05      CM4      .95214+18      CM2      .14913+16      CMH3      .19846+13
      CMH4      .77345+11      C3H5      .58512+09      CM4      .10440+21      CM42      .23952+17

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Sample Problem 2 Output (Concluded)

GRAPHITE SURFACE KINETICS (GASNET) PRON. 2 5002000000

CP-PROZEN = .3033+00

PROPERTY ROUTINE OUTPUT IN LR-MASS,FT,SEC,RTU,AND DEG-R
 TEMP VISC COND DHAR DP SC
 .25200+04 .29694-24 .29244-04 .11494+03 .34617+00 .72471+00
 MU1 MU2 MOL.WT HTIL CPTEL HTILO
 .02010+00 .20169+02 .24940+02 -.75174+03 .70007+00 -.10046+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASER = .647)
 1 6 7 8 13 17 19 104
 .07825-01 .10298+00 .11222+00 .24211+00 .98046-01 .34607+00 .15452-04 .104
 .96221-01 .11032+00 .11064+00 .29824+00 .49246-01 .24720+00 .35444-04 .00000

SOLUTION TIMES
 ITERATIONS = 11 TIME = 3.675 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS SIC/PG
 MASS TRANSFER COEFFICIENT ROULK = .46300+00
 RHO V WALL/RHOE UE CM = .33747-03 RHPHPL = .33747-03

STATE ADJACENT TO THE SURFACE . . .
 TEMP = 2520.0000 DEG R ± 1400.0000 HLG K PRESS = 26.66895 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LHM	-.11133+04	.00000	-.11133+04
ENTROPY - RTU/LHM DEG R	.20449+01	.00000	.00000
DENSITY - LRP/FT3	.36134+00		.36134+00
MOLECULAR WEIGHT	24.9401	.0000	24.9401

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM) . . .
 1 = .53826-05 2 = .14741-04 3 = .54105+00 4 = .76104-14 5 = .27709-21
 6 = .66291-21 7 = .50441-26 8 = .55636-28

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES

1 = .16744+02 2 = .14744+02 3 = .20164+03 4 = .16744+02 5 = .21144+03
 6 = .07324+04 7 = .14939+02 8 = .37005+00

CHEMICAL STATE ADJACENT TO THE SURFACE

(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
 (MOLE FR FOR CONDENSED = WHRIF CONDENSED) . . .

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.26494-01	H2	.44422+00	H2O	.13404+00	CO	.00000	CLH	.14444-01
AL	.67444-11	ALA	.23031-17	CH3CLAS	.64415-11	CO	.16533+00	CPH2	.46001-08
C	.71227-21	C2	.94744-24	C3	.37354-24	CH	.20434-31	C5	.17944-32
CAL	.61041-24	ALCI	.33044-04	ALLUO	.44475-04	ALC12	.72441-02	ALCL4	.62370-01
ALH	.32045-10	ALH02	.21947-04	ALU	.24444-11	ALPCL4	.40464-04	AL20	.17444-07
AL202	.40241-04	UCL	.30451-20	CLLH	.44461-11	CLL20	.54444-13	CLL4	.51245-25
CH	.37341-14	CHCL3	.32716-18	CH4	.61437-05	CHL0	.16705-06	CH0	.71245-08
CH2	.13542-13	CH2CL2	.14431-12	CH20	.14100-05	CH3	.44150-07	CH3CL	.31441-07
CH4	.13046-02	CH	.41420-13	CPH4	.44772-07	CPH40	.24137-14	CPH2	.18349-12
CS02	.50614-12	CHH2SI	.72444-20	CH02	.41444-21	CL	.17607-07	CLH0	.27349-11
CLH3SI	.74722-04	CLH0	.34414-17	CLU	.64414-14	CL02	.11459-26	CLSI	.44140-12
CLH2SI	.29144-07	CL20	.40444-24	CL2SI	.43274-07	CL3H4	.14744-07	CL4SI	.77219-07
H	.62442-04	H0	.24724-12	H0	.37417-14	H4SI	.14444-13	H2H	.42444-08
H202	.21420-14	H4H	.21444-04	H4H2	.24414-14	H4SI	.17645-09	H	.25922-15
N0	.16646-10	N02	.36302-19	SI	.37474-14	SI	.17002-14	N204	.32049-34
N204	.00000	N204	.00000	O	.44271-14	O	.31434-04	O2SI	.44944-08
O3	.12666-30	SI	.10747-14	SI2	.24424-22	SI3	.13743-27	CLL0	.24444-09
CLH02	.33434-27	H4H	.19742-13	H4H2	.14434-17	H4H3	.44422-27	ALH0	.74411-05
H02	.14327-17	H4H	.40143-32	CLL2	.64414-14	CLL3	.40442-22	H2H2	.17045-13
CH2	.66443-14	C20	.67402-15	C2H	.43174-14	CS1	.17052-23	CS12	.34522-21
C2H	.21770-17	C2SI	.20114-20	SI2	.17772-14	CPH14	.73178-24	CPCL4	.00000
AL02	.62443-12	CPCL2	.44425-19	CPHCL	.47444-13	CHLL	.17645-16	CL3SI	.40011-07
CL2	.98244-11	C2	.44745-01	CP	.74645-13	CH0	.17645-13	SI	.54247-19
C2H3	.90474-12	C2H4	.20440-07	CSH	.14412-16	CHH2	.44414-16	CHH4	.12412-13
C3H4	.70245-12	C3H5	.27040-10	CH	.16474-20	CHH2	.24144-17		

Sample Problem 3

In this problem, all options which require the input of thermophysical properties are utilized. The surface material option of carbon/carbon 901 is used. The edge thermodynamic state (2805.81°K and 12.778 atm) is input directly. Diffusion factors for 16 selected species are input. Preexponential factors, activation energies, and temperature exponents are input for each of the eight possible kinetically controlled reactions, and inhibiting coefficients are input only for the three oxidation reactions. Finally, two frozen-edge temperatures and two surface temperatures are input to be used in lieu of the corresponding built-in temperature arrays.

Listing of Input

	0037223400	2805.61	12.778	0.0	0.0	0.246	0.	PRGM. 5
1.	1000.							
2.	1000.							
3.	1000.							
4.								
5.	1200.							
6.	1400.							
7.								
8.	5							
9.	1 HYDROGEN	1.006	3.6752					
10.	6 CARBON	12.011	1.6865		1.0			
11.	7 NITROGEN	14.007	1.2430					
12.	8 OXYGEN	16.000	3.6376					
13.	9 FLUORINE	19.000	0.022683					
14.	16							
15.	C	0.691800H		0.749200CH		0.935700H		1.02670
16.	H2	1.017000C02		1.291400C02H2		1.17460H		0.30180
17.	CO	0.18930H2O		0.77490H		0.74930H0		0.99810
18.	H2	1.026200		0.7397002		1.000000C2		1.02530
19.	1 6 2	8 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
20.	-940539+5	366362+5	130735+2	733664-3-754525+6	798849+2	500.	2500.1	-0.C02
21.	-940539+5	365610+5	142661+2	269831-3-233974+5	798583+2	2500.	6000.1	-0.C02
22.	2 1 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
23.	-996 0+0	212685+5	626264+1	934668-3	610915+5	484856+2	500.	2500.1
24.	-996 0+0	212227+5	800304+1	362 19-3-186878+7	484694+2	2500.	6000.1	-0.H2
25.	2 1 1	8 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
26.	-577479+5	303898+5	847457+1	183253-2-305370+6	684879+2	500.	2500.1	-0.H2O
27.	-577479+5	302496+5	132 A+2	231126-3-481992+7	684385+2	2500.	6000.1	-0.H2O
28.	1 6 1	8 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
29.	-264169+5	224202+5	779944+1	441449-3-262 21+6	653523+2	500.	2500.1	-0.C0
30.	-264169+5	223744+5	866947+1	665971-4-155174+6	653761+2	2500.	6000.1	-0.C0
31.	1106	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
32.	0 0+0	144476+5	550350+1	240 14-3-559635+6	121418+2	500.	2500.2	-0.C*
33.	0 0+0	144197+5	526345+1	216128-3	131326+7	121316+2	2500.	6000.2
34.	1 17 1	1 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
35.	-220629+5	219473+5	705542+1	710907-3-136296+6	623935+2	500.	2500.1	-0.CLH
36.	-220629+5	218861+5	866363+1	182815-3-964314+6	623719+2	2500.	6000.1	-0.CLH
37.	1 9 1	1 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
38.	-651399+5	211218+5	641313+1	828856-3	240795+5	587192+2	500.	2500.1
39.	-651399+5	210703+5	855858+1	137134-3-259239+7	587 11+2	2500.	6000.1	-0.FH
40.	1 13 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0
41.	779999+5	134755+5	491880+1	303529-4	233929+5	508505+2	500.	2500.1
42.	779999+5	134527+5						

153

154

157

158

160

Sample Problem 3 Output

GRAPHITE SURFACE KINETICS (GASKET) PROG. 3

0130000*00

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00800	.0367511	.0000000
6	CARBON	12.01100	.0166646	.0000000
7	NITROGEN	14.00700	.0124297	.0000000
8	OXYGEN	16.00000	.0363751	.0000000
9	FLUORINE	19.00000	.0002268	.0000000
106	GRAPHITE	12.01100	.0000000	.0632570

ELEMENTS	HYDROGEN	CARBON	NITROGEN	OXYGEN	FLUORINE
	GRAPHITE				

BASE SPECIES	H2	CO2	N2	H2O	FH
	C*				

UPDATE OF DIFFUSION FACTORS

SPECIES	DIFFUSION FACTOR
CO2	1.29140
H2	.38930
H2O	.77490
N2	1.02620
CO	1.01700
C	.69180
CH	.74920
CH4	.93570
CN	1.02670
C2H2	1.17460
H	.30160
N	.74930
NO	.99810
O	.73970
O2	1.00000
C2	1.02530

Sample Problem 3 Output (Continued)

GRAPHITE SURFACE KINETICS (GASNET) PROC. 3

5002700000

6 6

CD=PROZEN = .40642+00

PROPERTY ROUTINE OUTPUT IN LH=MASS,FT,SEC,HTU,AREA,IF=H
 TEMP VISC COND DENS TR SC
 .00200+00 .32202+04 .21946+04 .20799+03 .59990+00 .72560+00
 MU1 MU2 POL,WT HTL CPVTL PTLA
 .91000+00 .24522+02 .74222+02 -.22304+04 .65100+00 -.22777+04

ELEMENTAL X AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (BAREN = .667)
 1 6 7 8 9 10A
 .34707-01 .20209+00 .16974+00 .30842+00 .42026+04 .00000
 .00037-01 .10074+00 .16924+00 .32775+00 .46036+02 .00000

SOLUTION TIMES
 ITERATIONS = 9 TIME = 2.00A SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
 MASS TRANSFER COEFFICIENT HOCUP = .24400+00
 AND V WALL/RMCE UE CM = .36549+00 RPHIME = .36509+05

STATE ADJACENT TO THE SURFACE . . .
 TEMP = 2920.0000 DEG R = 1400.0000 DEG K PRESS = 12.7700 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LBM	-.23210+04	.00000	-.23210+04
ENTROPY - BTU/LBM DEG R	.22778+01	.00000	.00000
DENSITY - LBM/FT3	.17234+00		.17234+00
MOLECULAR WEIGHT	24.0277	.0000	24.0277

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RMCE UE CM) . . .
 1a .20622-11 2a .20394-10 3a .62277-15 4a .14100-10 5a .52247-21
 6a .12444-20 7a .11020-25 8a .10443-27

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
 1a .20444+03 2a .20444+03 3a .41413+05 4a .20444+03 5a .41413+05
 6a .39606+07 7a .34961+02 8a .33290+00

CHEMICAL STATE ADJACENT TO THE SURFACE

(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
 (MOLE FR FOR CONDENSED = RPHIME CONDENSED) . . .

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
COS	.20660+00	M2	.13763+00	N2O	.20701+00	C0	.00000	FM	.54917-02
N2	.15006+00	CO	.21270+00	C	.12225-21	H0	.20168-07	N03	.27003-29
CH	.24604-19	CH4	.34500-06	CHNO	.62813+07	CH0	.31555-08	CH2	.34602-15
CH2O	.32602-04	CH3	.43417-09	CH4	.49644-05	CN	.60089-14	CNO	.19360-13
CH2 NCN	.02424-19	C2H	.23449-16	C2H2	.46792-11	C2H4	.12399-10	C2HNO	.50602-17
C2H	.26030-19	C2H2	.18655-14	C2O	.42104-14	C3O2	.26190-13	C4H	.62090-28
C2H2	.41220-22	C4H2	.20810-25	H	.50230-06	H0	.36064-12	HNO	.90543-13
HNO2 TR	.60216-14	HNO3	.20508-24	H02	.51714-16	H2H	.11257-08	H2N2	.38256-14
H2O2	.30374-13	H3N	.21726-04	H4N2	.10715-15	V	.42360-15	N0	.19767-09
N02	.20066-17	N2O	.17162-13	N2O3	.14489-31	O	.68069-13	O2	.60927-13
C2H6	.96498-12	C2H3	.73364-15	C3H	.62367-20	C3H2	.11281-19	C3H3	.05090-10
C3H4	.17992-16	C3H5	.26672-15	F2	.29367-24	CHF	.50361-17	CHFO	.14526-08
CHF3	.13191-18	CH2F2	.49591-15	CH3F	.63194-11	C2F2	.60764-28	C2F3H	.94375-20
C2F4	.95265-34	C2HF	.65967-14	F	.26389-12	CHC	.35534-16	FC	.10407-20
FWO	.10522-18	FWO2	.74180-28	FWO3	.00000	FO	.60793-22	FO2	.16645-27
FWN	.20079-28	FWN2 TR	.76466-34	FO	.32145-14	F3H	.34429-38	F3NO	.00000
CF	.77779-19	CFN	.79470-15	CF0	.14415-12	CF2	.33902-18	CF2O	.12085-11
CF3	.34321-23	CF4	.41522-23	C2	.13842-26	C1	.43170-27	C4	.19044-35
C5	.14004-37								

Sample Problem 3 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROG. 3

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DLNM/DLMT	DLHM/DLHP	GAMMA
.46249+00	.65564+00	-.99470-01	.44135-02	.11752+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, BTU, AND DEG-R

TEMP	VISC	CONU	UHAR	PR	SC
.50505+04	.51724-04	.39360-04	.76050-03	.60777+00	.72573+00
MU1	MU2	MOL.WT	HTIL	CPTIL	HTIL*
.90353+00	.24443+02	.23866+02	-.76863+03	.54365+00	-.90189+03

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)

1	6	7	8	9	106
.37025-01	.20256+00	.17410+00	.38200+00	.43097-02	.00000
.49537-01	.18874+00	.16429+00	.58775+00	.46436-02	.00000

SOLUTION TIMES

ITERATIONS = 38

TIME = 13.699 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .00000
 TEMP = 5050.4579 DEG R. = 2805.4100 DEG K. PRESS = 12.77800 ATM

ENTHALPY - BTU/LHM	GAS	CONDENSED	COMPOSITE
	-.10389+04	.00000	-.10389+04
ENTROPY - BTU/LHM DEG R	.26582+01	.00000	.26582+01
DENSITY - LBM/FT3	.82678-01		.82678-01
MOLECULAR WEIGHT	23.8660	.0000	23.8660

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
C02	.12957+00	H2	.10109+00	H2O	.32744+00	C*	.00000	FW	.54117-02
N2	.14795+00	CO	.27292+00	C	.77738-11	H0	.67376-02	N03	.39440-13
CH	.61978-11	CH*	.22775-06	CH10	.11414-06	CH0	.24462-05	CH2	.83245-11
CH20	.20104-06	CH3	.23200-09	CH4	.13789-09	CH	.17571-08	CH0	.39465-08
CN2	.18493-12	C2H	.81423-13	C2H2	.69146-12	C2H4	.22745-15	C2H40	.10719-14
C2H	.48730-14	C2H2	.88703-14	C20	.94466-11	C302	.53113-13	C4H	.29314-23
CHH2	.72762-24	CH42	.17134-25	H	.73962-02	H0	.66530-06	H40	.38493-06
HNO2	.11660-07	H*03	.34432-12	H02	.53589-06	H2N	.84655-06	H2N2	.22739-10
H202	.30976-06	H3*	.12701-05	H4H2	.46335-14	N	.39010-06	N0	.74492-03
N02	.70996-07	H20	.58228-07	H203	.37731-15	O	.31381-03	O2	.41419-03
C2H6	.21207-19	C2H5	.26796-15	C3H	.62186-18	C3H2	.29627-19	C3H3	.58945-20
C3H4	.27923-21	C3H5	.48241-21	F2	.01304-14	CHF	.24473-12	CHF0	.24447-08
CHF3	.12704-18	CH2F2	.72442-16	CH3F	.54603-13	C2F2	.33636-22	C2F3H	.28234-26
C2F4	.39976-30	C2HF	.13616-16	F	.17095-05	FH0	.11542-08	FN	.87972-11
FNO	.87005-10	FNO2	.94423-15	FNO3	.20093-21	F0	.42544-10	F02	.32441-12
F2N	.57401-17	F2H2	.11121-21	F20	.23175-18	F3H	.95160-25	F3N0	.17392-29
CF	.16741-11	CF*	.17162-11	CF	.24658-08	CF2	.61495-14	CF20	.75542-11
CF3	.72827-19	CF4	.42456-22	C2	.34436-16	C3	.55451-20	C4	.88845-28
C5	.24395-32								

Sample Problem 3 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASNET) PROR. 3      0000000000

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLNM/DLNT      DLNM/DLNP      G6HFA
.38462+00      .19183+01      -.27575+00      .44135+02      .10709+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, RTU, AND DEG-R
TEMP      VISC      COND      DHAN      PR      SC
.18000+04      .26207-04      .16470-04      .15753-03      .61201+00      .72573+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.90353+00      .24443+02      .23866+02      -.24210+04      .44749+00      -.24385+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GANEY = .667)
      1      6      7      8      9      106
.37025-01      .20256+00      .17410+00      .58200+00      .43097-02      .00000
.49537-01      .18874+00      .16929+00      .58775+00      .46836+02      .00000

SOLUTION TIMES
ITERATIONS = 38      TIME = .252 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .00000
TEMP = 1800.0000 DEG K. = 1000.0000 DEG K.      PRESS = 12.77400 ATM

ENTHALPY - RTU/LBM      GAS      CONDENSED      COMPOSITE
-.24353+04      .00000      -.24353+04
ENTROPY - BTU/LBM DEG K      .22222+01      .00000      .22222+01
DENSITY - LBM/FT3      .25186+00      .0000      .25186+00
MOLECULAR WEIGHT      25.8660      .0000      25.8660

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .12957+00      H2      .10109+00      H2O      .15274+00      C4      .00000      FH      .54117-02
N2      .14795+00      CO      .27242+00      C      .77738-11      H0      .07376-02      F0      .39443-13
CH      .61978-11      CH4      .262775-06      CH3O      .11414-06      CH0      .24462-05      CH2      .63245-11
CH2O      .20108-06      CH3      .25200-09      CH4      .13784-04      CH      .17571-08      CH0      .39465-08
CN2      .18443-12      C2H      .01523-13      C2H2      .69146-12      C2H4      .22785-15      C2H4O      .10715-18
C2N      .48730-14      C2N2      .69703-14      C2O      .94466-11      C3O2      .51115-13      C4H      .29314-23
C4H2      .72782-24      C4H2      .17314-25      H      .74462-02      H4      .44530-06      H2O      .38495-06
HN02      .11660-07      HN03      .24432-12      H02      .55449-06      H2H      .22789-10
H2O2      .30976-06      H3O      .12701-05      H4H2      .64335-14      V      .39010-06      H2H2      .74442-03
N02      .70996-07      N2O      .58224-07      H2O3      .77731-15      O      .31351-03      O2      .41419-03
C2H6      .21207-19      C2H3      .25746-15      C3H      .62186-14      C3+2      .29627-19      C3H3      .58945-20
C3H4      .27923-21      C3H5      .48241-21      F2      .41304-14      CHF      .24473-12      CHF0      .28647-08
CHF3      .12704-18      CH2F2      .72442-16      CH3F      .94603-13      C2F2      .35638-22      C2F3H      .24234-26
C2F4      .39976-30      C2HF      .13-16-16      F      .17095-05      FH0      .11542-08      F4      .87972-11
FNO      .87085-10      FNC2      .44423-15      FNO3      .20043-21      FO      .42544-10      FO2      .32441-12
F2N      .57401-17      F2H2      .11121-21      F2O      .23175-14      F3H      .39160-25      F3H0      .17392-29
CF      .16741-11      CF4      .17162-11      F0      .24459-08      CF2      .41495-14      CF2O      .75542-11
CF3      .72827-19      CF4      .42446-22      C2      .34436-14      C3      .54451-20      C4      .64445-28
CS      .24395-32

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Sample Problem 3 Output (Concluded)

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CO-FROZEN = .5430E+00

PROPERTY ROUTINE OUTPUT IN LG-PASS,RT-SEC,RTUARD,LEG-N
TEMP      VISC      CORR      DENS      EN      SE
.2160E+04 .2695E-04 .1940E-04 .1654E-03 .5705E+00 .725E+00
MU1      MU2      MOL WT      HTL      HTIL      HTIL*
.9236E+00 .2450E+02 .2416E+02 .2412E+04 .4777E+00 .2454E+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASEY = .667)
      1      2      3      4      5      6      7      8      9      10
.3368E-01 .2030E+00 .1660E+00 .5411E+00 .4156E-02 .000000 .000000
.4953E-01 .1847E+00 .1692E+00 .5477E+00 .4663E-02 .000000 .000000

SOLUTION TIMES
ITERATIONS = 9          TIME = 2.474 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
MASS TRANSFER COEFFICIENT HMOX = .2460E+00
RHO V WALL/RHCE DE CM = .744E-12  FPRIME = .744E-12

STATE ADJACENT TO THE SURFACE . . .
TEMP = 2160.0000 DEG R = 1200.0000 DEG K  PRESS = 12.77E+00 ATM

      GAS      CONDENSED      COMPOSITE
ENTHALPY = BTU/LBM      -2.2405E+04      .00000      -2.2405E+04
ENTROPY = BTU/LBM DEG R      .2183E+01      .00000      .2183E+01
DENSITY = LBM/FT3      .2040E+00      .00000      .2040E+00
MOLECULAR WEIGHT      25.1859      .0000      25.1859

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHO DE CM) . . .
1= .3414E-14  2= .5493E-13  3= .6285E-14  4= .5508E-23  5= .3492E-25
6= .1293E-25  7= .1147E-31  8= .9612E-34

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .2814E+02  2= .2814E+02  3= .7919E+03  4= .2814E+02  5= .1125E+02
6= .4163E+02  7= .3692E-04  8= .3093E-06

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = GRIFF CONDENSED) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .2394E+00      H2      .1522E+00      H2O      .2654E+00      CO*      .00000      CO*      .00000
N2      .1510E+00      CO      .1860E+00      C      .5078E-25      H2O      .2481E-09      H2O      .2481E-09
CH      .3904E-22      CHN      .3944E-06      CH2O      .5119E-07      CH2O      .5119E-07      CH2O      .5119E-07
CH2O      .3756E-04      CH4      .5220E-09      C4H      .1E-23E-03      C4H      .1E-23E-03      C4H      .1E-23E-03
C2H      .6565E-21      C2H      .1449E-17      C2H2      .2320E-10      C2H2      .2320E-10      C2H2      .2320E-10
C2N      .4544E-21      C2H2      .1152E-14      C2H2      .1649E-17      C2H2      .1649E-17      C2H2      .1649E-17
C4H2      .1604E-21      C4H2      .3554E-25      H      .2144E-07      H      .2144E-07      H      .2144E-07
HN02 TR      .1092E-18      HN03      .1907E-24      H02      .2369E-19      H2H      .1223E-09      H2H      .1223E-09
H2O2      .1410E-14      H3E      .560E-04      H4H2      .6347E-16      V      .4447E-14      V      .4447E-14
N2O      .1012E-20      N2O      .1205E-15      H2O3      .3747E-17      O      .4301E-16      O      .4301E-16
C2H6      .3959E-09      C2H3      .1072E-14      C2H3      .1512E-20      C3H2      .8502E-20      C3H2      .8502E-20
C3H4      .7606E-15      C3H5      .2364E-13      F2      .1E-12E-27      CH4      .1101E-14      CH4      .1101E-14
CHF3      .1440E-14      CH2F2      .1E-07E-14      F2H3F      .4454E-10      C2F2      .7428E-30      C2F2      .7428E-30
C2F4      .6994E-35      C2HF      .1144E-14      F      .1457E-14      FNO      .1129E-13      FNO      .1129E-13
FNO      .1171E-21      FNO2      .3470E-32      FNO3      .5527E-26      F2O      .5527E-26      F2O      .5527E-26
F2N      .5552E-32      F2N2 TR      .7761E-34      F2O      .6000E-00      F3I      .00000      F3I      .00000
CF      .2784E-21      CF4      .6374E-14      CF4      .6374E-14      CF2      .1201E-19      CF2      .1201E-19
CF3      .1355E-24      CF4      .2222E-24      CF2      .4544E-10      C4      .1E-19E-29      C4      .1E-19E-29
C5      .00000

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